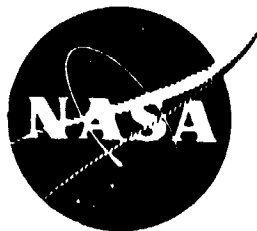


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NASA CR-135140

QUIET CLEAN SHORT-HAUL EXPERIMENTAL ENGINE (QCSEE)

Whirl Test of Cam/Harmonic Pitch Change Actuation System

by

Aircraft Systems Department, Propulsion Project Group

Hamilton Standard
Division of United Technologies Corporation

Under Subcontract to General Electric Company
(P.O. 200-4XX-14G38570)

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CAM/HARMONIC PITCH CHANGE ACTUATION SYSTEM
Contractor Report, 10 Nov. 1975 - 16 Feb.
1976 (Hamilton Standard, Windsor Locks,

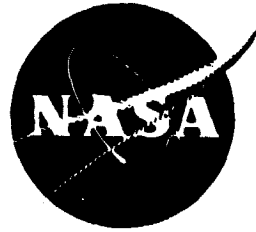
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Prepared For

National Aeronautics and Space Administration

NASA Lewis Research Center
Contract NAS3-18021



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16. Abstract <p>A variable pitch fan actuation system, which incorporates a remote nacelle mounted blade angle regulator, was tested. The regulator drives a rotating fan mounted mechanical actuator through a flexible shaft and differential gear train. The actuator incorporates a high-ratio harmonic drive attached to a multi-track spherical cam which changes blade pitch through individual cam follower arms attached to each blade trunnion.</p> <p>Testing of the actuator on a whirl rig, is reported. The tests were conducted to verify that the unit satisfied the design requirements and was structurally adequate for use in an engine test.</p>					
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1.0

SUMMARY

The Hamilton Standard blade pitch change actuation system for the Quiet Clean Short Haul Experimental Engine (QCSEE) was tested on a whirl rig, at Hamilton Standard, between November 10, 1975 and February 16, 1976.

The objectives of the test were to verify that the unit satisfied the design requirements and was structurally adequate for use in an engine test.

The testing included evaluation of the travel limit switch, blade angle position accuracy, performance, frequency response, and endurance.

During tests of the travel limit switch it was found that the no-back output shaft was under-designed. Analysis of the shaft revealed that it could not be adequately strengthened within the space available. In order to reduce the load on the no-back, a snubber was installed in the actuator. When run with the snubber, no further distress was noted on the output shaft.

The testing showed that:

- Blade overtravel after actuation of the travel limit switch at maximum pitch change rate and zero fan speed was within the calculated value of 6.5-7.0 degrees.
- Blade angle can be positioned within 0.25 degrees when moving from open to close at zero fan speed and within 1.5 degrees at high fan speeds.
- There is approximately 1 degree of hysteresis in the system when reversing the direction of blade angle change at zero fan speed.
- The minimum attainable blade angle change was 0.17 degrees toward open and 0.26 degrees toward close.
- The maximum pitch change rate attained during a blade angle change was 135 degrees/second.
- Frequency response without the snubber indicated reasonable correlation with predictions at frequencies up to 1 Hertz where the magnitude ratio was lower and the phase shift was higher than at frequencies above 1 Hertz.

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- **Frequency response with the snubber again indicated reasonable correlation with predictions at frequencies up to 1 Hertz with excitation magnitudes of ± 8 ma, however with ± 4 ma excitation the magnitude ratio was down and there was considerable phase shift.**
- **The actuation system successfully completed 500 simulated mission endurance cycles at pitch change rates up to 75 degrees/second and 50 cycles at pitch change rates up to 135 degrees/second.**

2.0

INTRODUCTION

During the proposal effort for the Quiet Clean Shorthaul Experimental Engine (QCSEE), a design study of ten prospective fan pitch change systems was conducted. The results of this study were reported in HSPC 74A14 QCSEE Variable Pitch Fan System Proposal. On the basis of this effort, four systems were selected for further study.

The detail study of the four systems was conducted under General Electric Purchase Order 200-4XX-14G31376. The results of the study were presented in SP 08A74 QCSEE Variable Pitch Fan Pitch Change System. The study showed that a system incorporating a remotely mounted Beta Regulator, driving a harmonic drive/cam actuator through a flexible drive shaft, was the most attractive. This type of system was designed, manufactured, and tested under NASA Contract NAS 3-18021. The results of the design effort were reported in NASA CR-134852 which also includes a summary of the preliminary design studies done on the other systems.

A second actuator was also developed by the General Electric Company. Details of the design of the General Electric actuator are presented in NASA CR-134873 "QCSEE Ball Spline Pitch Change Mechanism Design Report".

This report describes the whirl rig testing conducted on the system. The object of the test was to determine the operating characteristics of the actuator, verify that it satisfies the design requirements, and assure its structural adequacy for use in an engine test.

3.0

SYSTEM DESCRIPTION

The variable pitch actuator system is shown in Figure 1. An electrical input command signal from the engine digital control to the electro-hydraulic servo valve (EHV) directs high pressure oil to motors in the beta regulator. This provides rotary mechanical input to the actuator differential gear train through a flexible drive shaft. Rotary motion is then transmitted through a no-back, harmonic drive, rotating cam, and cam follower arms to the blade trunnions. Since there is a fixed mechanical relationship between hydraulic motor rotation and blade angle, two linear variable differential transformers (LVDT) driven by motor output provide redundant blade angle feedback signals to the digital control to close the control loop and null the input signal when the blades reach the commanded position.

The overall gear ratio from the blades to the drive shaft is 1005:1 with most of the ratio (201:1) provided by a harmonic drive. This permits the low-torque power transmission elements between the beta regulator and the harmonic drive to be designed for low weight and improved blade angle accuracy.

The mechanical pitch change power and blade angle feedback functions are provided by the beta regulator module which is remotely mounted in a readily accessible area of the engine cowling. A simplified schematic of the beta regulator is shown in Figure 2. A blade angle change command from the engine control to the EHV mounted in the accessory section, causes movement of the servo valve to direct supply oil to either the open or close pitch ports of the hydraulic motor. The motor output drives the flexible shaft to change blade angle and drives two LVDT's through a worm gear and screw to provide an electrically redundant blade position feedback. Electrical limit switches are provided to cut off the command signal to the EHV if a blade angle is commanded beyond the maximum operating range. Pressure relief valves across the motor ports limit motor pressure to 3000 psi during rapid accelerations of the actuator system.

The rotary output of the beta regulator is transmitted to the actuator differential gear train through a flexible drive shaft passing through the engine reduction gearing. The shaft core is encased in a flexible teflon lined casing supported in a rigid conduit mounted on the engine reduction gear support. Continuous engine lubrication oil flow is directed through the casing from the beta regulator to lubricate the core and the actuator components.

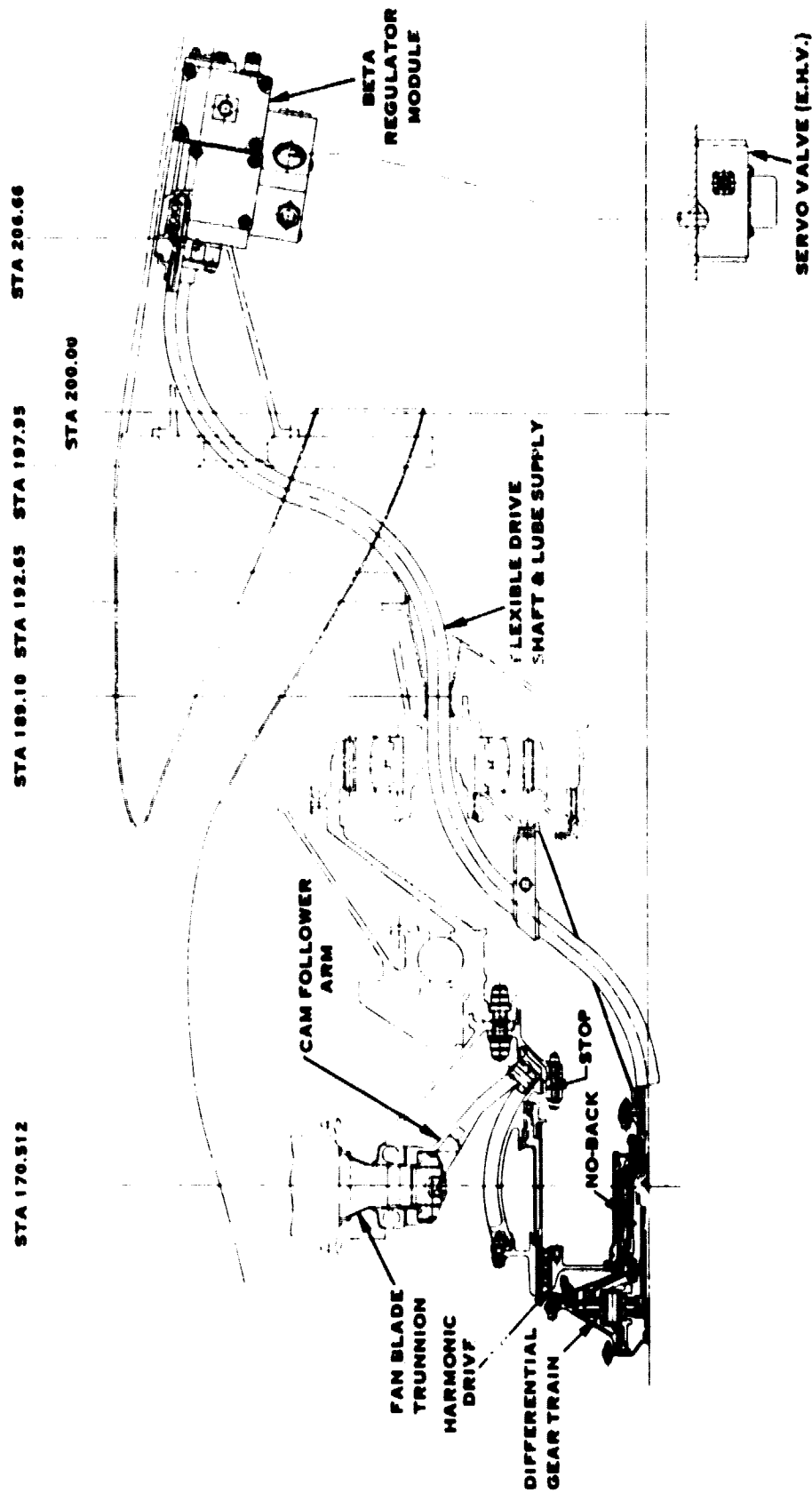


FIGURE 1. QCSEE VARIABLE PITCH ACTUATOR SYSTEM

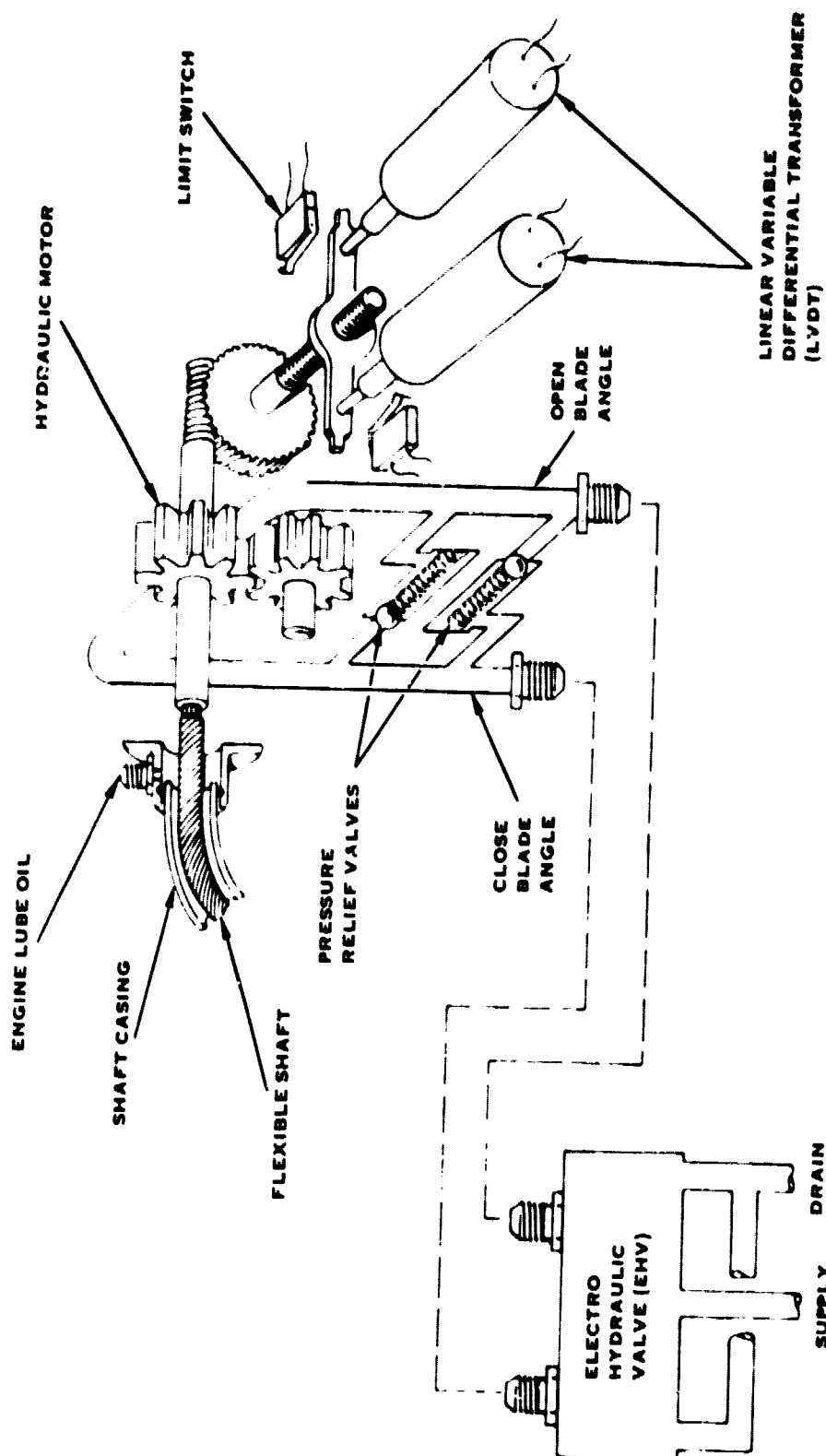


FIGURE 2. BETA REGULATOR SCHEMATIC

3.0 (Continued)

A planetary differential gear train is utilized to cross the rotating boundary of the fan. The differential gearing is a conventional 5:1 ratio phase difference type with a grounded sun gear, an input sun gear driven by the flexible shaft, three pairs of planet gears on a bearing supported cage, a reference speed ring gear fixed to the fan disk and an output ring gear driving the no-back input. With no pitch change input, the output ring gear rotates at fan speed. Rotation of the input sun gear during pitch change causes the output ring gear to either advance or recede with respect to the fan speed. This change in output is the input to the no-back. The gears and bearings are lubricated by oil directed outward centrifugally from the sun gear shafts.

A bi-directional spring clutch or "no-back" is provided between the differential gearing and the harmonic drive to maintain the set blade angle position in the absence of a pitch change command. This device consists of a self-energizing steel spring which is in contact with the inner surface of a fixed housing, the input and output shafts and the necessary couplings and bearings. When holding a fixed blade angle, the blade loads are transmitted to ground (housing) through the spring. When the input acts against opposing blade loads (raising the load), the spring slides in the housing and does not react to any blade loads. When the input acts against aiding blade loads (lowering the load), the input releases the spring at the commanded pitch rate and the blade load energy is dissipated in frictional heat between the spring and housing. Due to the short duty cycle and the thermal mass of the parts, the total heat rise is low in the no-back. Lubrication oil flows continually through the no-back and is supplied centrifugally from the sun gear shafts.

No-back housing torque is reacted by a disk-type torque limiter brake. The no-back is a high-gain locking device capable of locking more than a million in-lbs of torque at high friction coefficients, and the torque limiter limits maximum no-back torque to ground to acceptable structural limits during rapid pitch change decelerations. The brake disks are lubricated by oil supplied centrifugally from the differential gearing.

The harmonic drive provides the primary gear reduction for the mechanical actuator and increases the input torque to the level required to change pitch. Four basic elements are incorporated in this high-ratio (201:1) mechanical transmission rated at 50,000 in-lbs output. They are: a three-lobed harmonic-shaped wave generator input plug which provides the harmonic the harmonic lobe shape to the flexible spline, a triplex split inner race ball bearing set for high radial stiffness, a flexible spline (flex spline) to convert from

3.0 (Continued)

the harmonic lobe shape to a grounded circular shape with minimum frictional losses and a stiff circular output spline which drives the blade pitch cam.

The thin-race ball bearings are pressed on the three-lobed wave generator plug and assume the three-lobe harmonic shape. Spline teeth on the outside diameter of the flex spline mesh with spline teeth on the inside diameter of the circular spline at the three lobe locations. Circular splines on the other end of the flex spline ground it to the fan disk. Due to a 3-tooth difference in number of teeth between the circular spline and flex spline ($603-600=3$), one revolution of the wave generator input rotates the circular spline output $3/603$ or $1/201$ of a revolution.

Lubrication oil for the harmonic bearings and splines is supplied centrifugally from the differential gearing and no-back.

The cam and follower arms convert output rotation of the harmonic drive to fan blade angle change. Titanium follower arms, splined and clamped to the blade trunnions, engage individual cam slots in the spherical cam surface through cam rollers to synchronize the blades and sum the blade torques. The radial axis defined by the roller and cam track centerlines always intersects the fan axis of rotation at the same point similar to the apex point of a bevel gear mesh.

Cam support is provided by a preloaded duplex bearing set mounted on a support ring attached to the fan disk mounting flange for accurate balance control. Lubrication oil from the harmonic drive lubes the bearing set and is returned centrifugally to the engine scavenge area. A single dynamic oil seal with centrifugal venting precludes a dynamic pressure head.

Fixed mechanical stop lugs between the cam and cam support ring restrict the blades to 7° overtravel at each end of the maximum operating range.

4.0

RIG DESCRIPTION

Figure 3 is a drawing showing the arrangement of the whirl rig and the actuator.

The whirl rig used for the test was a modification of an existing rig. The rig utilizes a 186.4 kilowatts (250 horsepower) electric motor to drive the fan through an eddy current clutch and a speed increasing gearbox. The connecting shaft between the gearbox and the actuator has a flange which dimensionally duplicates the actuator/disk mounting surface in the engine. The flange also provides a path for the removal of the lubrication fluid.

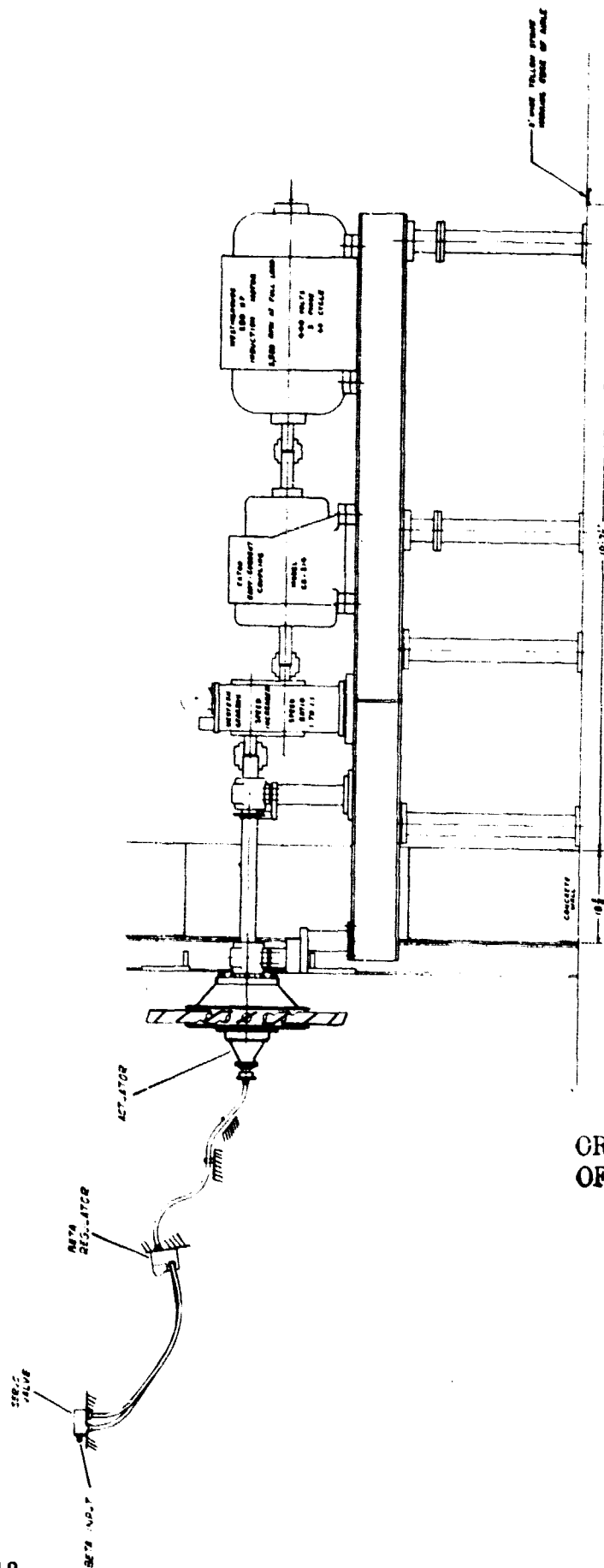
A disk together with trunnions, stub blades (counterweights), and other retention hardware was provided for the test by General Electric. The stub blades are designed to apply the same centrifugal load to the blade retention and the actuator as the actual blade, and to approximate the twisting moment of the actual blade. Figure 4 is a curve of twisting moment versus blade angle for the actual and the stub blade. Stub blades were used for the test as they do not produce thrust and therefore can be driven by a relatively small motor.

Initial attempts to run the rig revealed the need to provide a shroud to enclose the stub blades and their retention to reduce the windage losses and consequently the power required to drive the assembly and the noise level in the vicinity of the test rig.

In the engine, the Beta Regulator is mounted behind the actuator and the flex shaft is routed through the engine gearbox to the actuator. To duplicate this arrangement on the whirl rig would require a hollow connecting shaft between the speed increaser gear box and the actuator, a hollow shaft through the gear box, and a quill shaft between the flex cable and the pitch change input at the actuator. This approach was investigated and discarded as it added another spring rate to the pitch change input system (the quill shaft), as well as being expensive and time consuming to obtain a hollow shaft gearbox.

Instead, a set of test hardware which provided a front input to the actuator for the flex cable was designed and manufactured. This hardware does not affect the spring rate of the input system. Figure 5 is an assembly drawing of the front input hardware.

In an engine installation, the lubricating and pitch change fluids are supplied by an engine driven pump. For the whirl test, a Viking pump rated at 18.9 liters/min (5 gpm) at 68.9 newtons/cm² (100 psi) was used to supply the



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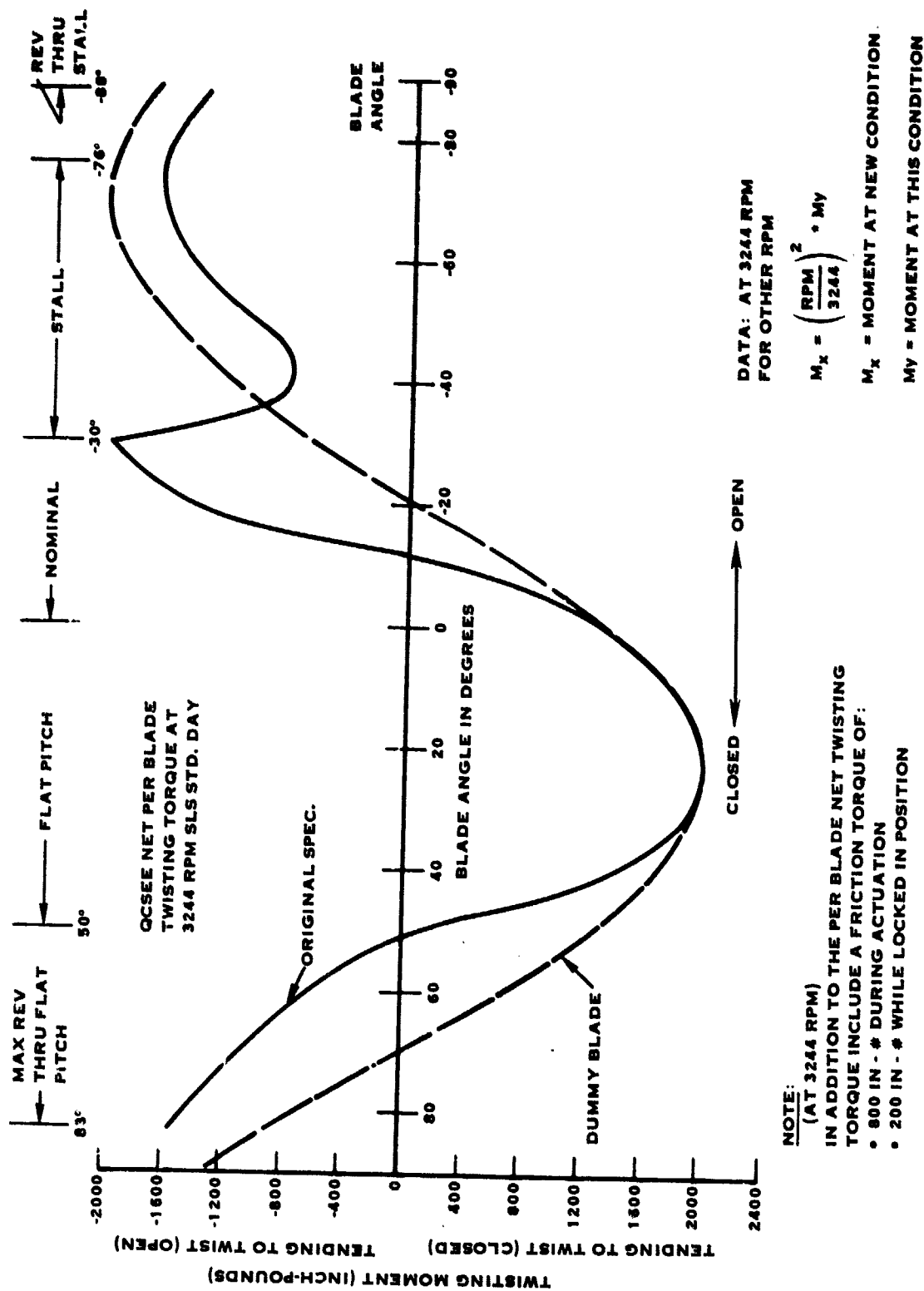


FIGURE 4. MAX NET TWISTING MOMENT

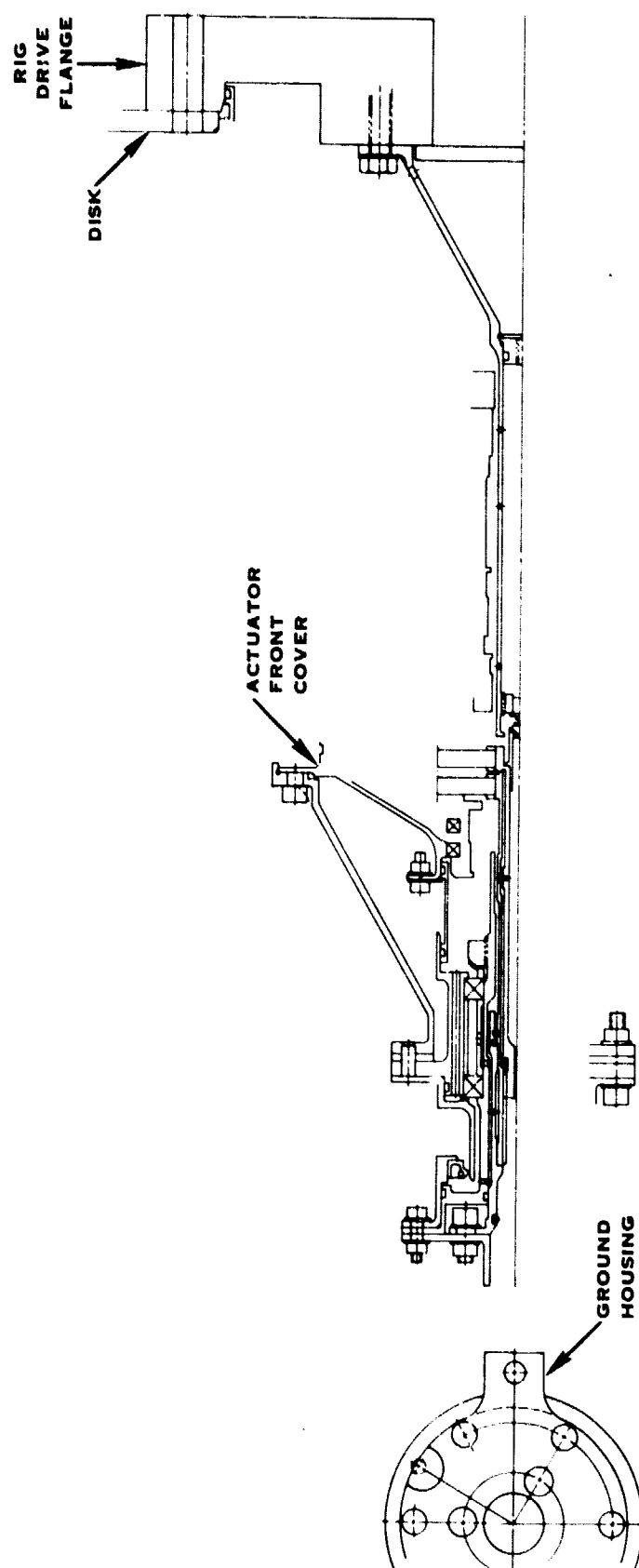


FIGURE 5. ASSEMBLY, FRONT INPUT HARDWARE

lubricating fluid. Initially, it was planned to use one Denison pump rated at 132.5 liters/min (35 gpm) at 3447.4 newtons/cm² (5000 psi) to supply change fluid for the majority of the testing, and to use a Denison pump rated at 94.6 liters/min in parallel with it for testing requiring high flow (maximum pitch change rates). Operating the two pumps proved to be quite difficult, so the second pump was replaced by an accumulator.

The instrumentation provided for the test is listed in Table I. The flex shaft speed was measured by machining a six tooth wheel on the feedback shaft in the beta regulator, and installing a magnetic pickup in the beta regulator housing.

The flex shaft torque was measured by strain gaging and calibrating the ground sun gear in the actuator.

Actual blade angle was measured using photo diode sensors to measure the relative position of the actuator cam and the disk. The output of the sensors was read by a phase meter.

Figure 6 is a photograph of the whirl rig installation.

A closed loop variable gain control system, modified from an existing unit, was used to operate the actuator.

The rig was operated in accordance with Operating Procedure 222PT-37. A copy of this procedure is included in Appendix A.

TABLE I
INSTRUMENTATION LIST

Measurement	Range	Accuracy
EHV Supply Pressure	0 - 4000 psig	± 40 psi
EHV Current Signal	± 100 ma	± 2.25% of reading
Flow to EHV	0 - 45 gpm	± 2.83% of full scale
ΔP Across-Motor	0 - 3500 psig	± 2.25% of full scale
Temperatures	0 - 300°F	± 2°F
Blade Angle Command	+20 to -120°	± 2% of full scale
LVDT Feedback Voltage	± 5 V dc	± 2% of full scale
Flex Shaft Speed	0 - 24,000 rpm	± 2.83% of full scale
Flex Shaft Torque	0 - 200 in lb	± 2.83% of full scale
Lube Oil Flow	0 - 1 qt/min	± 2% of reading
Lube Oil Pressure	0 - 100 psig	± 1 psi
Fan Speed	0 - 3700 rpm	± 2% of full scale
Vibration - Horizontal	0 - 30 mils	± 5% of reading
Vibration - Vertical	0 - 30 mils	± 5% of reading
Fan Blade Angle	+20 to -120°	± 0.2°

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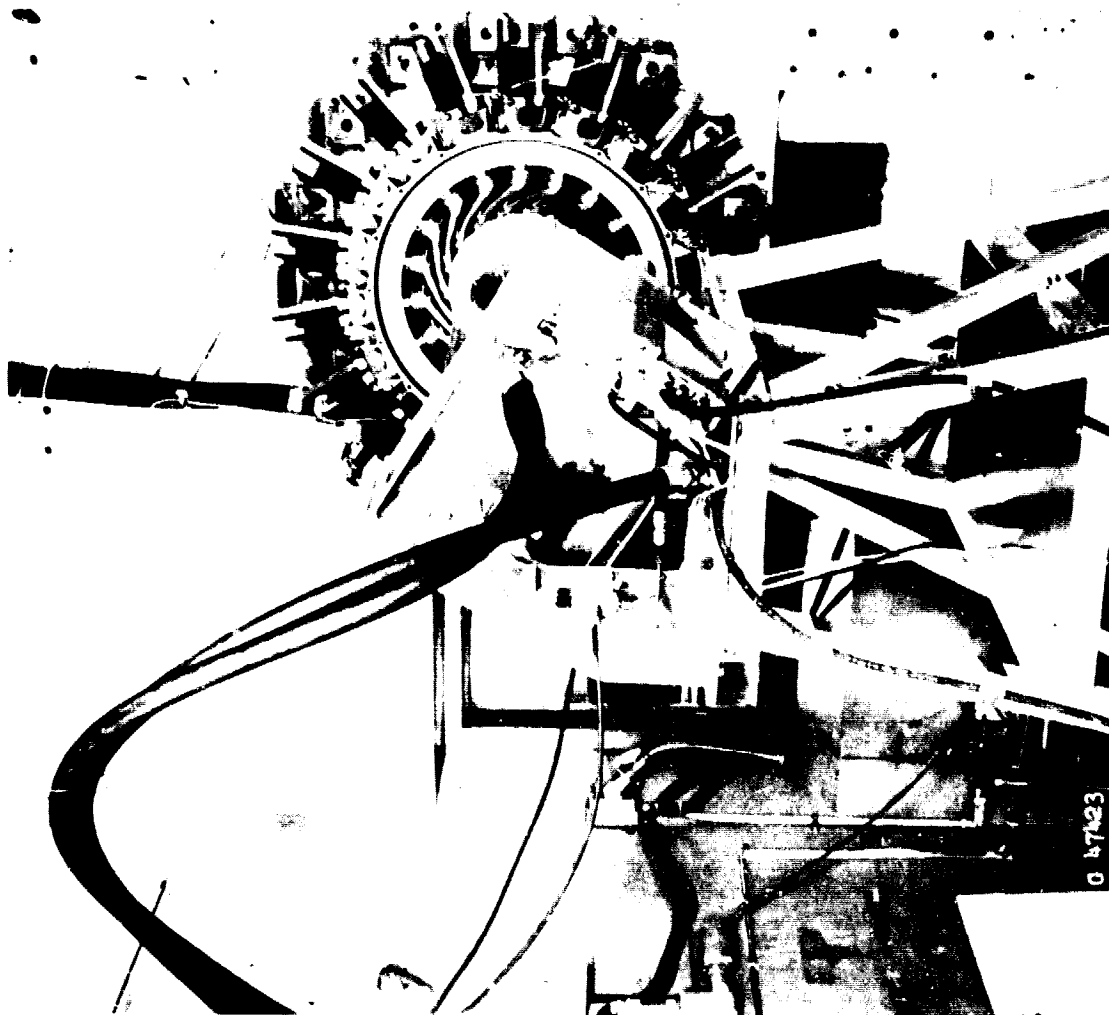
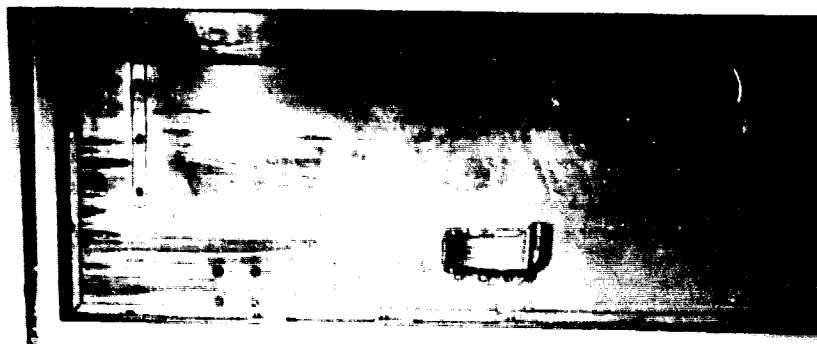


FIGURE 6. ACTUATOR IN WHIRL RIG

5.0

TEST PROCEDURE

The test was conducted essentially in accordance with Plan of Test 222PT-31 Rev. A. A copy of this plan is included in Appendix B. Variations from the Plan of Test are described below at the appropriate point in the test procedure description.

The test points in the plan are defined in terms of fan blade angle to be compatible with the specification. However, the stub blades supplied by General Electric were offset 25° relative to the blade angle in order to properly locate the peak twisting moment loads on the actuation system and a portion of the test data was recorded in terms of counterweight angles. The data is marked blade angle or counterweight angle, as appropriate, and the relationship between the two is that blade angle plus 25° equals counterweight angle. For the test, the counterweights were reindexed 2 spline teeth (18.5 degrees) from the design condition. This was done at the direction of General Electric to obtain more reverse blade angle.

The lubrication flow check was conducted with the flex shaft disconnected from the actuator. The flow from the shaft was measured at varying inlet pressures. Inlet pressure was measured at the pump.

The test was later repeated measuring the pressure at the inlet to the regulator and measuring the flow at the inlet to the flex shaft.

The LVDT null and calibration test was accomplished by changing blade angle with the manual pitch change input and measuring the counterweight angle. The blades were moved from "close" to "open" only.

The travel limit switch tests were accomplished by setting the controller to give a step command of approximately 30-40 degrees of blade angle which would actuate the travel limit switch. The pitch change rate was varied by regulating servo valve supply pressure and flow. The amount of overtravel was determined by physical measurement of the angle at which the counterweights stopped, compared with the angle at which the switch actuated. The testing was conducted at 0 fan rpm.

During early testing it was found that operation at the maximum pitch change rate overstressed the no-back output shaft. In order to continue testing, the maximum pitch change rate was limited to 75 degrees/second.

Initial running revealed a rig resonance at approximately 2500 fan rpm. To avoid this resonance, all testing specified at 2500 rpm was conducted at 2700 rpm.

5.0

(Continued)

The position accuracy test was conducted by setting blade angle with the controller and measuring actual blade angle. Because of the instrumentation accuracies in this test (controller setting, actual blade angle readout) an alternate static positioning accuracy test was also run. In this test, the blade angle feedback (LVDT's) were positioned with the manual input and the actual blade angle change was measured by a dial indicator and converted to angle change.

The test to determine the pressure and flow required to start and sustain actuator motion was conducted by commanding the desired change with no pressure to the servo valve, and then increasing the pressure to the valve until the blade angle change was complete.

The test to determine the minimum blade angle change around 0° was conducted by slowly changing the controller input until a change in LVDT feedback voltage was observed. The actual counterweight position was measured to determine that the blades had moved.

Frequency response testing was conducted with a two channel transfer function analyzer with automatic gain and sweep control and direct plot output. For the static testing, blade angle was measured by a proximity pickup set up on one of the stub blades.

The endurance test was conducted in accordance with Table II. The forward thrust test points were set manually, the modulating thrust points were run using an oscillator input to the controller, and the reverse/unreverse transients were step inputs to the controller. Initial cycles were conducted at approximately six per hour to preclude overheating the no-back. Since experience showed no evidence of heating on the no-back spring, the remaining cycles were conducted at a rate of ten to twelve per hour.

Following testing in accordance with Plan of Test 222PT-31 Rev. A, the actuator was modified by the addition of a snubber. Testing in accordance with Plan of Test 222PT-38 was then accomplished. A copy of this plan is included in Appendix B.

TABLE II
QCSEE ACTUATOR

Speed (rpm)	Blade Angle	DC Command Pot Setting	Feedback Gain	Step Command Set	Cond.
2700 (#3)	12°	309	325	9.81	ON
2700	-3°	205	↑ <		

*Plug in Function Gen. - Amp - Min
Freq - Range 0.1
Dial 1.9

Don't Forget to go to 2700 Prior to Unreverse.

≈ 10 min/cycle

5.0 (Continued)

These tests were conducted in the same manner as the tests of Plan of Test 222PT-31 Rev. A with the exception of the frequency response test. This test was conducted with a single channel transfer function analyzer. This unit did not have automatic gain and sweep control, or direct plot capability. The following test points were run rather than those listed in the plan of test.

Frequency (cps)	Servo Valve Current (ma)
0.5	$\pm 4 \pm 8$
1.0	$\pm 4 \pm 8$
2.0	$\pm 4 \pm 8 \pm 12$
3.0	$\pm 4 \pm 8 \pm 16$

6.0

TEST RESULTSStructural

During the test the following structural problems were noted with the hardware.

During the initial tests of the travel limit switches, after six actuations at pitch change rates up to 82 degrees/second, it was found that the no-back output shaft had fractured at the webs between the three windows. Figure 7 is a photograph of the shaft. The fracture of the shaft was attributed to the shaft being under-designed in this area for the expected load of 271.1 newton meters (2400 inch pounds). The shaft was repaired by electron beam welding, and "beefed" up in the area where it had fractured. In addition a new shaft was fabricated incorporating additional strengthening. The welded shaft (763494-1/222X575) was approximately twice as strong and the new shaft (763494-1 Chg. B) was four times as strong as the design which fractured. Figure 8 is a comparison of the three configurations.

Testing was resumed with the welded output shaft. Performance tests, including some running at high pitch change rates, and a total of 46 flight cycles were completed. The unit was disassembled for a routine inspection, and the welded output shaft was found to be fractured in two of the three webs.

Analysis of this incident revealed that the original design of the shaft did not take into account the torque generated by inertia of the no-back drum and brake hardware which must be accelerated up to speed when the actuator starts slowing down.

At pitch change rates of 135 degrees per second, this inertia raises the load on the shaft to 536.6 newton meters (4750 inch pounds). Further analysis revealed that even with the inertia reduced as much as feasible in the existing design, the output shaft could not be strengthened sufficiently within the space available. Consequently, testing with the new shaft was limited to a pitch change rate of 75 degrees per second.

After completion of 500 flight cycles, the new shaft (763494-1 Chg. B) was found to be cracked in the web area. Investigation of this incident including a static torque test of the system, revealed that the spring rate of the system was 5648.7 newton meters per radian (50,000 inch pounds per radian) rather than the calculated 2824.4 newton meters per radian (25000 inch pounds per radian). The higher spring rate raises the expected 271.1 newton meter load on the shaft at 75°/second pitch change rate, to 451.9 newton meters (4000 inch pounds).

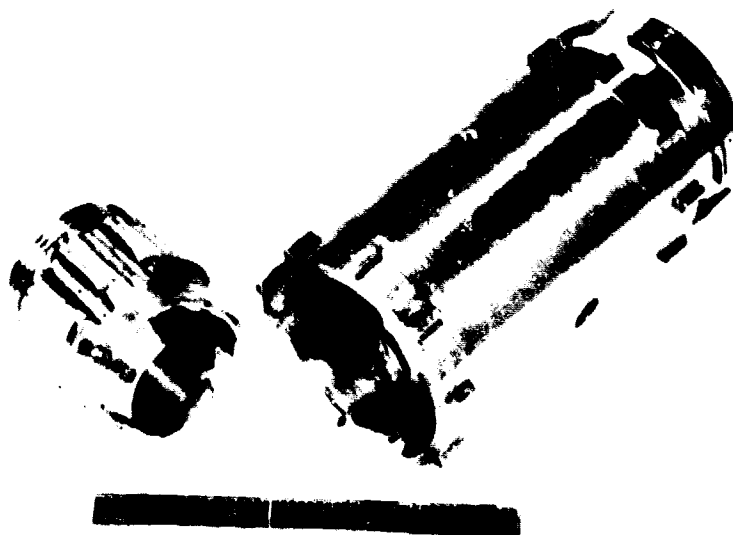


FIGURE 7. 763494-1 OUTPUT SHAFT

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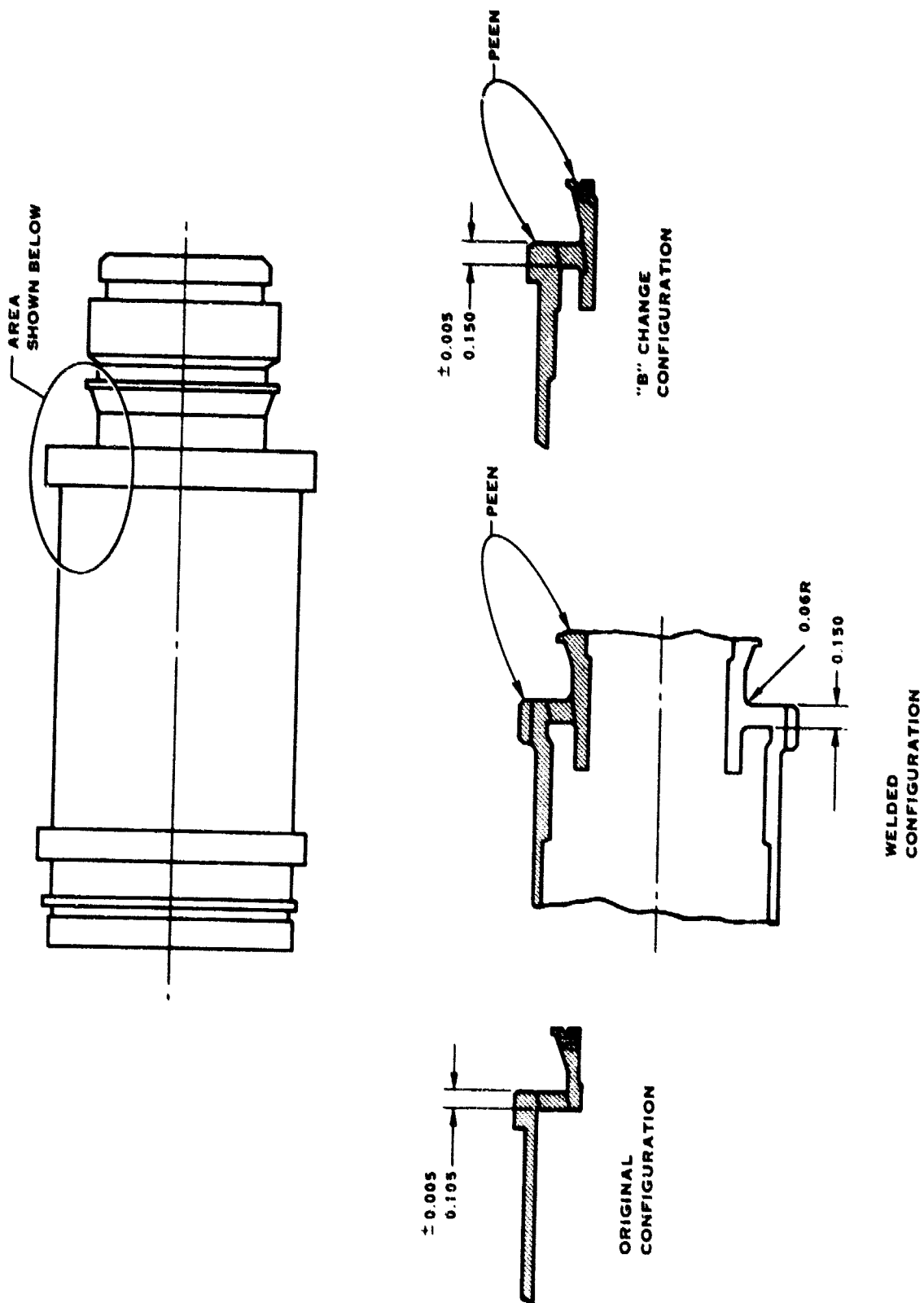


FIGURE 8. OUTPUT SHAFT COMPARISON

6.0 (Continued)

The difference between the calculated and actual system spring rates is the result of the coefficient of friction assumed between the no-back spring and the no-back drum. In the calculations, a lower than actual coefficient was used. This results in more engaged spring coils to absorb a given torque resulting in a greater spring deflection, and therefore a lower no-back spring rate.

To restore the actuators maximum pitch change rate capability, a snubber was designed and fabricated to reduce the spring rate of the system to 677.8 newton meters per radian (6000 inch pounds per radian), which reduced the output shaft load to 271.1 newton meters at the maximum pitch change rate of 135°/second.

Incorporation of the snubber results in the following life predictions for the output shaft and the snubber:

Maximum Flex Shaft Speed (rpm)	17,500	21,000
Snubber Fatigue Life (cycles)		
at room temperature	> 1,000	750
at 93.3°C (200°F)	1,000	500
Output Shaft Fatigue Life (cycles)		
at room temperature	5×10^4	1.5×10^4
at 93.3°C (200°F)	2.1×10^5	1×10^5

At the same time that the snubber was installed in the actuator, the no-back spring was replaced with a new part. This was done as a precautionary measure as the original spring had been subjected to higher than design loads during operation without a snubber.

Prior to, and following the testing of Plan of Test 222PT-38, the spring rate of the snubber was measured. The initial measurement revealed the actual spring rate to agree closely with the calculated rate (684.4 newton meters per radian [6067 inch pounds per radian] vs. 698.2 newton meters per radian [6180 inch pounds per radian]). The after testing check revealed no change in spring rate or other deterioration of the snubber.

6.0 (Continued)

During the initial spring rate check of the snubber, its deflection versus load was calibrated. A means of indicating relative motion during actuator operation was added to the snubber, and the deflection checked at various pitch change rates up to maximum. These measurements indicated that the snubber limited the load on the output shaft to the design value of 293.7 newton meters (2600 in lbs).

It was observed during the test that the wear pattern on the cam tracks was high in the track on one side, and low on the other. Inspection of the cam revealed that the sides of the tracks were not parallel to a radius through the center of the track. Subsequent running over the full range of speeds and loads has shown that this small abnormality in the pattern does not represent a significant problem and no corrective action was taken.

As a result of an assembly error, the rear support housing was fractured in the 'O' seal groove area that mates to the engine. This fracture extended about 3 inches circumferentially at the aft edge of the seal groove. The housing was repaired by removing the damaged area, electron beam welding a new ring onto the back of the housing, and remachining.

During the lubrication flow check it was found that oil leaked through the outer casing of the flex shaft at the junction with the end fittings. This was found to be a result of a drawing error which did not call for the teflon lining in the casing to be swaged between the casing and the end fittings. The second flex cable leaked slightly at the junction of one end fitting and the casing. This was attributed to a poor joint at the swage of the casing to the end fitting. For rig running, the conduit was sealed at the actuator and the drain hole plugged to contain the leakage.

At the completion of testing, the flex shaft core was deformed, apparently as a result of having been over-torqued. The distortion of the core during the over-torque also deformed the casing. Reference Figure 9. The over-torque was attributed to a shutdown during the travel limit switch tests from a pitch change rate of 130 degrees per second with a controller time constant of 10 milliseconds. The controller was modified to a time constant of 25 milliseconds, (system designed for 20-30) and subsequent shaft torques were measured to be within acceptable limits.

During the inspection following the completion of testing per 222PT-31 Rev. A, pitting and scoring were noted on the bevel gears and their pinion. The data received with the bevel gear set from the manufacturer had shown the final grind pattern to be marginal.

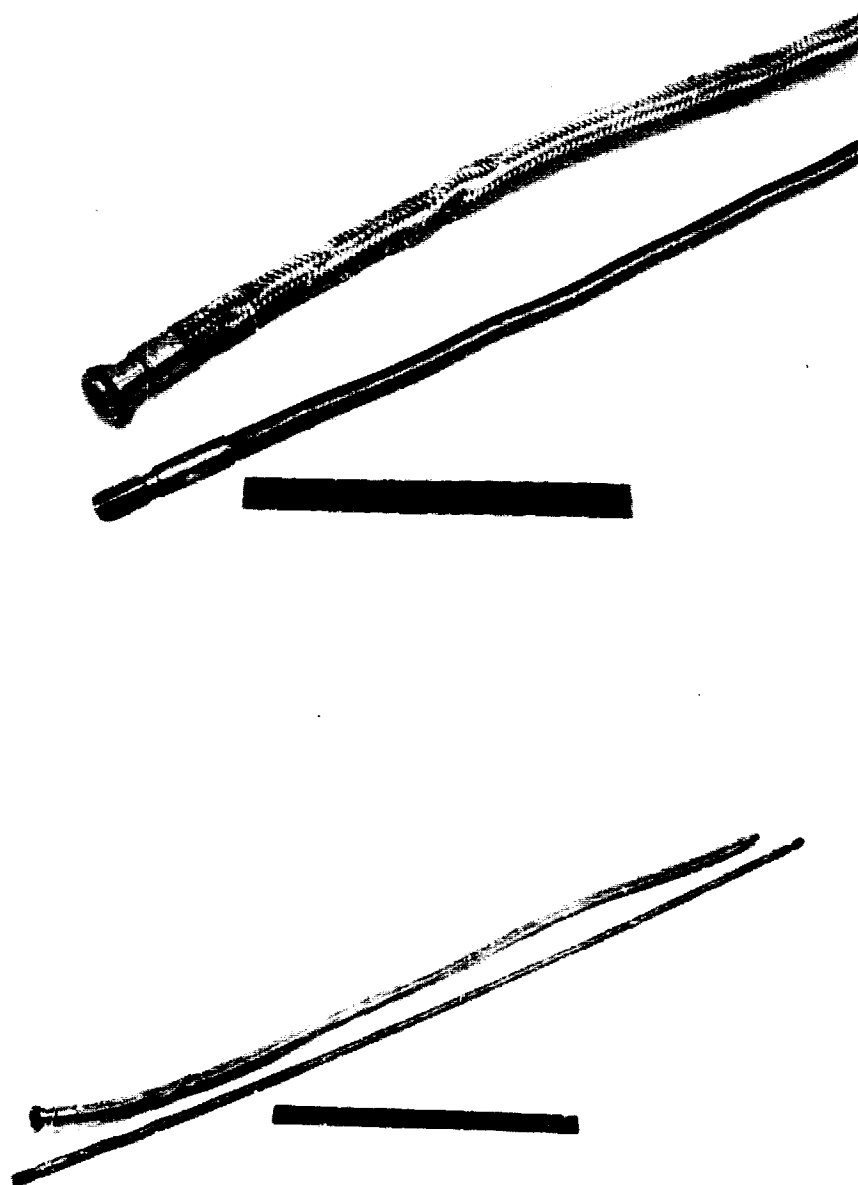


FIGURE 9. 763402-1 FLEXIBLE SHAFT

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6.0 (Continued)

During the course of the test, the gear pattern had been examined several times and always appeared to be high on the tooth. Consequently, the shimming of the pinion and gears was changed several times to bring them closer into mesh. As the parts are brought closer into mesh the backlash is reduced. The lubrication system for the beta regulator was designed to provide a mist to lubricate the gear mesh. As the backlash was reduced, this method of lubrication apparently became marginal. The gear set was replaced, and the regulator reworked to provide an oil jet which sprays directly into the gear mesh. The mesh was shimmed to insure sufficient backlash rather than attempting to center the pattern on the tooth.

During the disassembly of one of the hydraulic motors for inspection, the bearing housing was damaged by a faulty disassembly procedure. This motor was replaced by a new motor. Following the completion of the flight cycles conducted with the snubber, an attempt was made to conduct the frequency response test. With an input to the servo valve of ± 4 ma, no response was obtained from the actuator. The hydraulic motors were disassembled for inspection, and the new motor was found to exhibit heavy wear on the housing bore at the drive gear face. Dimensional inspection revealed no reason for this wear. Another motor was installed in the regulator, and the actuator then responded to current inputs to the servo valve of ± 4 ma.

All other hardware in the actuator and the regulator was in good condition following the tests. The hardware was subjected to magnaflux, zygo, and visual inspection following the completion of testing per Plan of Test 222PT-31 Rev. A, and visual inspection following testing per Plan of Test 222PT-38.

Performance

The lubrication flow check revealed that it took 63.8 newtons per square centimeter (92.5 pounds per square inch) at the lubrication pump to obtain a flow of 0.80 liters per minute (0.85 quarts per minute) out of the flex shaft. Figure 10 is a plot of the data taken during this test. A second check was made to determine the pressure required at the inlet to the regulator to obtain the required flow. This test showed that it took 42 newtons per square centimeter (61 pounds per square inch) to achieve the desired flow. The design value was 48 newtons per square centimeter (70 pounds per square inch). Figure 11 is a plot of the data taken during this test.

The results of the LVDT calibration tests showed the output voltages from the two LVDT's to be in close agreement. Table III is a summary of the data taken during the test where the blades were moved from "close" to "open", and Figures 12 and 13 are plots of output voltage versus blade angle.

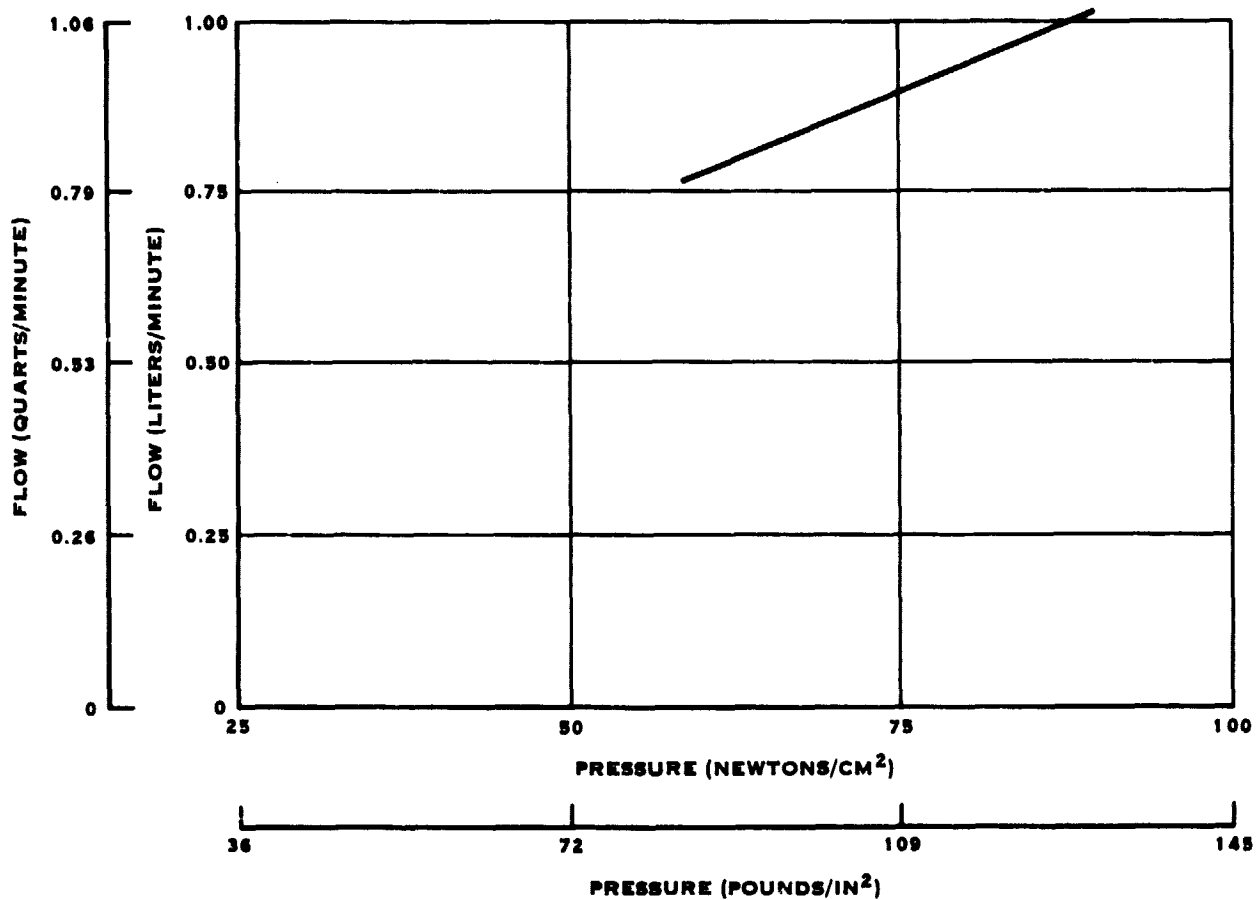


FIGURE 10. LUBRICATION FLOW CHECK FLOW VS. PRESSURE AT PUMP 11-10-75

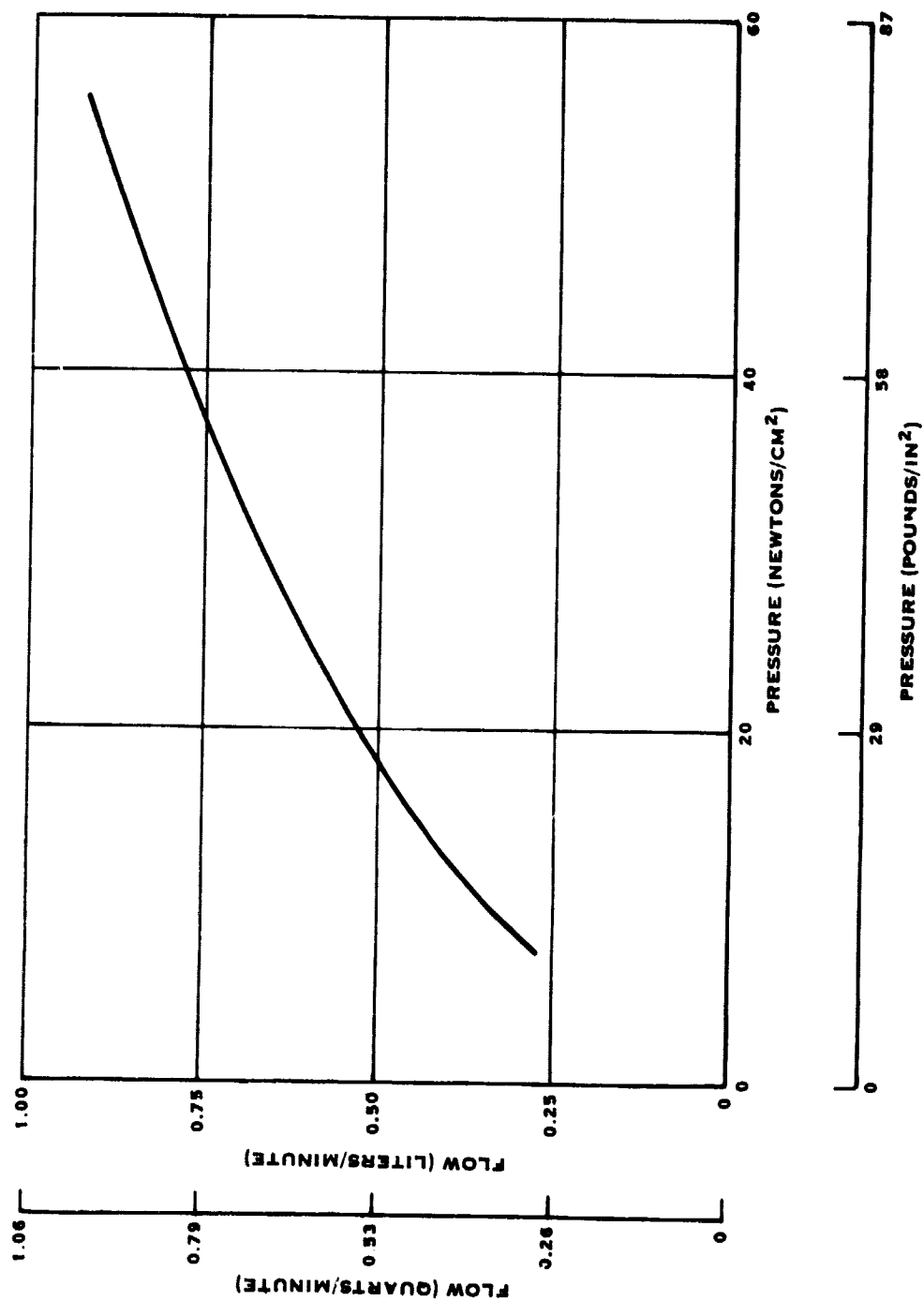


FIGURE 11. LUBRICATION FLOW CHECK - FLOW VS. PRESSURE AT REGULATOR 1-14-76

TABLE III
LVDT CALIBRATION

DATA FROM 11-10-75

Counterweight Angle	Blade Angle	Excitation Voltage	Output Voltage Total		Output Voltage Volts/Volt	
			LVDT1	LVDT2	LVDT1	LVDT2
*42.2	17.2	5.666	2.373	2.371	0.419	0.418
35.0	10.0	5.665	2.107	2.105	0.372	0.372
30.0	5.0	5.667	1.907	1.905	0.337	0.336
25.0	0	5.664	1.715	1.711	0.303	0.302
20.0	- 5.0	5.666	1.513	1.509	0.267	0.266
15.0	-10.0	5.667	1.307	1.305	0.231	0.230
10.0	-15.0	5.665	1.094	1.091	0.193	0.193
5.0	-20.0	5.666	0.893	0.890	0.158	0.157
0	-25.0	5.665	0.706	0.704	0.125	0.124
- 5.0	-30.0	5.665	0.518	0.517	0.091	0.091
-10.0	-35.0	5.666	0.345	0.342	0.061	0.060
-15.0	-40.0	5.665	0.184	0.183	0.032	0.032
-20.0	-45.0	5.664	0.034	0.033	0.006	0.006
-25.0	-50.0	5.665	-0.121	-0.121	-0.021	-0.021
-30.0	-55.0	5.665	-0.265	-0.265	-0.047	-0.047
-35.0	-60.0	5.665	-0.425	-0.425	-0.075	-0.075
-40.0	-65.0	5.665	-0.575	-0.574	-0.102	-0.101
-45.0	-70.0	5.665	-0.725	-0.725	-0.128	-0.128
-50.0	-75.0	5.665	-0.875	-0.873	-0.154	-0.154
-55.0	-80.0	5.665	-1.027	-1.027	-0.181	-0.181
-60.0	-85.0	5.665	-1.190	-1.187	-0.210	-0.210
-65.0	-90.0	5.665	-1.353	-1.351	-0.239	-0.238

TABLE III (Continued)
LVDT CALIBRATION

DATA FROM 11-10-75

Counterweight Angle	Blade Angle	Excitation Voltage	Output Voltage Total		Output Voltage Volts/Volt	
			LVDT1	LVDT2	LVDT1	LVDT2
-70.0	-95.0	5.665	-1.520	-1.514	-0.268	-0.267
-75.0	-100.0	5.665	-1.686	-1.683	-0.298	-0.297
-80.0	-105.0	5.665	-1.850	-1.847	-0.327	-0.326
-85.0	-110.0	5.665	-2.007	-2.003	-0.354	-0.354
-90.0	-115.0	5.665	-2.153	-2.150	-0.380	-0.380
-95.0	-120.0	5.665	-2.290	-2.284	-0.404	-0.403
*-98.7	-123.7	5.665	-2.382	-2.378	-0.420	-0.420

*Mechanical Stop

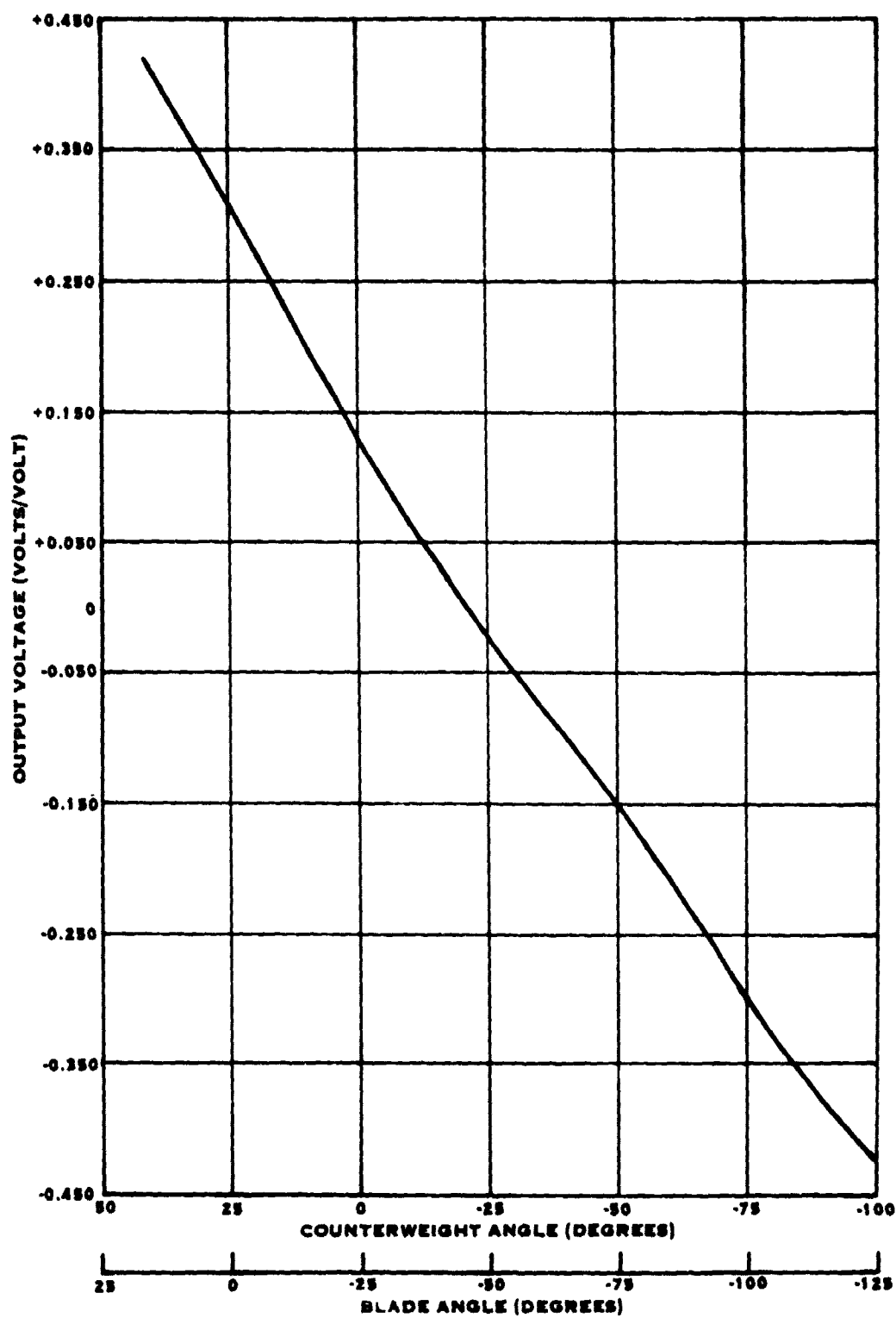


FIGURE 12. OUTPUT VOLTAGE VS. BLADE ANGLE LVDT #1 11-10-75
DATA TAKEN FROM CLOSE TO OPEN

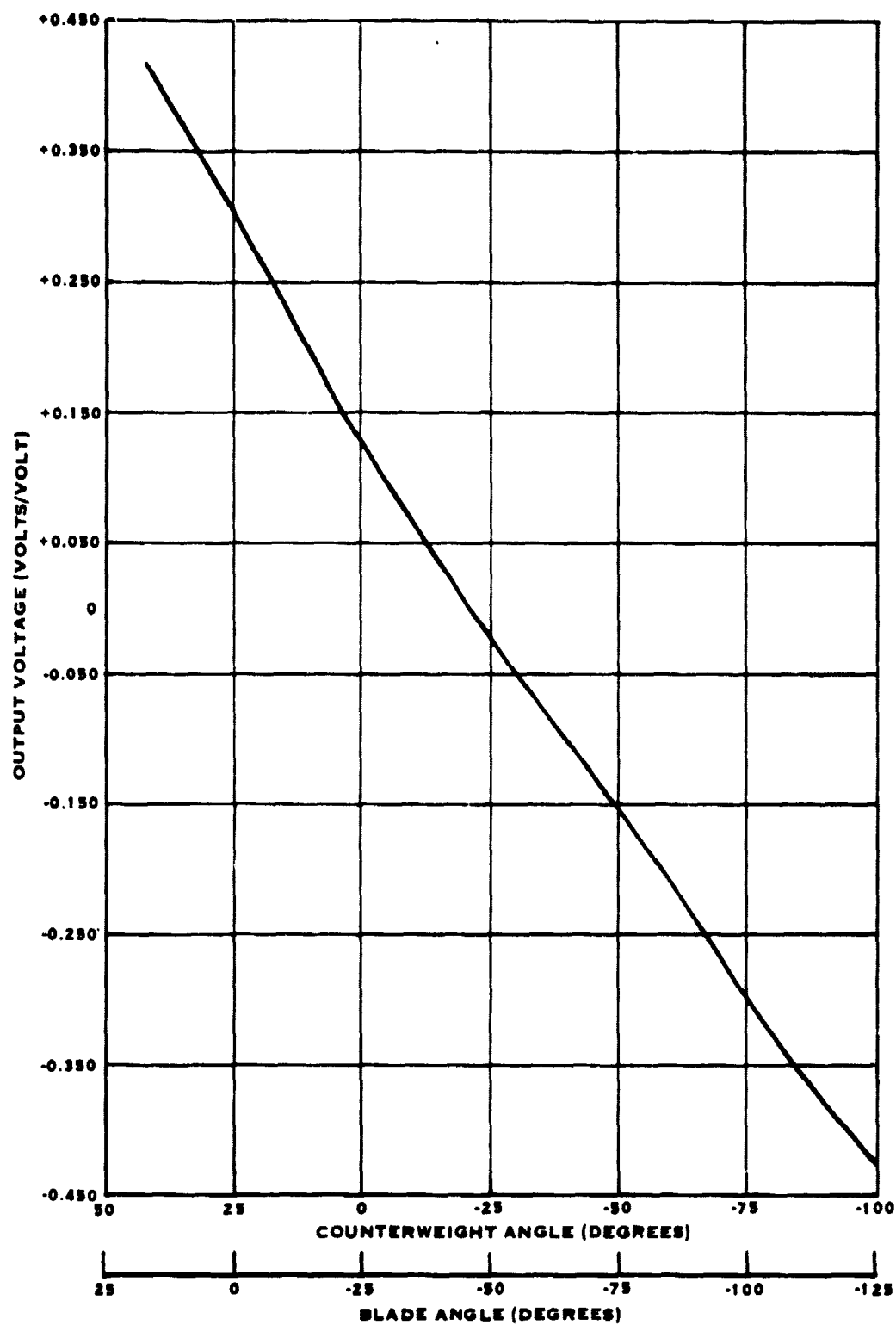


FIGURE 13. OUTPUT VOLTAGE VS. BLADE ANGLE LVDT #2 11-10-75
DATA TAKEN FROM CLOSE TO OPEN

6.0

(Continued)

The data available from the travel limit switch tests indicates that the blade overtravel after a switch actuation at maximum pitch change rate was within the calculated value (6.5° - 7.0°), when the data is adjusted for the higher pitch change rate and the effect of the motor back pressure is taken into account.

Table IV is a summary of the data taken during the tests. The data shows that the overtravel and the flex shaft torque are greater at the open end of travel than at the close end. The reason for this has not been determined. Overtravel and flex shaft torque are a function of the pitch change rate, the servo valve time constant, and the drag torque of the torque limiter brake. The higher the pitch change rate, the greater the overtravel and the higher the shaft torque. The greater the valve time constant, the greater the overtravel and the lower the shaft torque. The higher the drag of the torque limiter, the less the overtravel and the lower the shaft torque. Figure 14 is a curve of calculated overtravels and torques versus valve time constants.

In setting the torque limiter brake drag, variations amounting to 1 n-m (10 in. lb) of flex shaft torque from one direction to the other occurs. This does not account for the differences noted in the test. It is felt that the difference is a result of different dynamics in the no-back operation from one direction to the other. Sanborn traces of a travel limit switch stop at both the open and close ends of travel are included in Appendix C.

The rotating blade angle position accuracy test showed a maximum deviation of 1.5° between the set (LVDT) blade angle and the angle determined by the photo diode system. Tables V, VI, and VII are summaries of the data. The deviation noted is within that expected based on estimates of the mechanical and hydraulic hysteresis, the accuracy of the LVDT calibration, and the accuracy of the photo diode system. The three points which show the photo diode sensor angle to be closer to open than the LVDT angle are considered to be bad data points and should be ignored.

The static blade angle position accuracy test showed that the correlation between the set and resultant blade angles were good. In the close direction over a 4° range from 2° open to 2° close the resultant angle deviated from the set angle by a total of 0.25° . This deviation is within the accuracy of the LVDT calibration.

The test also showed that there is slightly less than 1 degree of hysteresis in the system when reversing the direction of blade angle change. This is somewhat greater than the expected value of 0.79 degrees. The expected value consists of a mechanical error of 0.48 degrees, a feedback backlash

**TABLE IV
TRAVEL LIMIT SWITCH**

DATA FROM 2-13-75

Step Blade Angle Command

Time Constant = 25 milliseconds

Fan Speed = 0 rpm

Blade Angle Travel Prior to Stop - 30 degrees

Actuator with Snubber

<u>Switch Setting</u>		<u>Beta Stop</u> (degrees)	<u>Beta Overtravel</u> (degrees)	<u>Pitch Change Rate</u> (degrees/sec)	<u>Peak Shaft Torque</u>	
<u>Open</u> (degrees)	<u>Close</u> (degrees)				(in-lbs)	(N-m)
-115.1		-119.0	3.9	101.2	260	29.4
		-120.5	5.4	106.5	300	33.9
		-121.1	6.0	116.2	340	38.4
	+10.2	+12.3	2.1	103.2	230	26.0
		+15.5	5.3	123.8	250	28.2
		+15.6	5.4	123.8	250	28.2

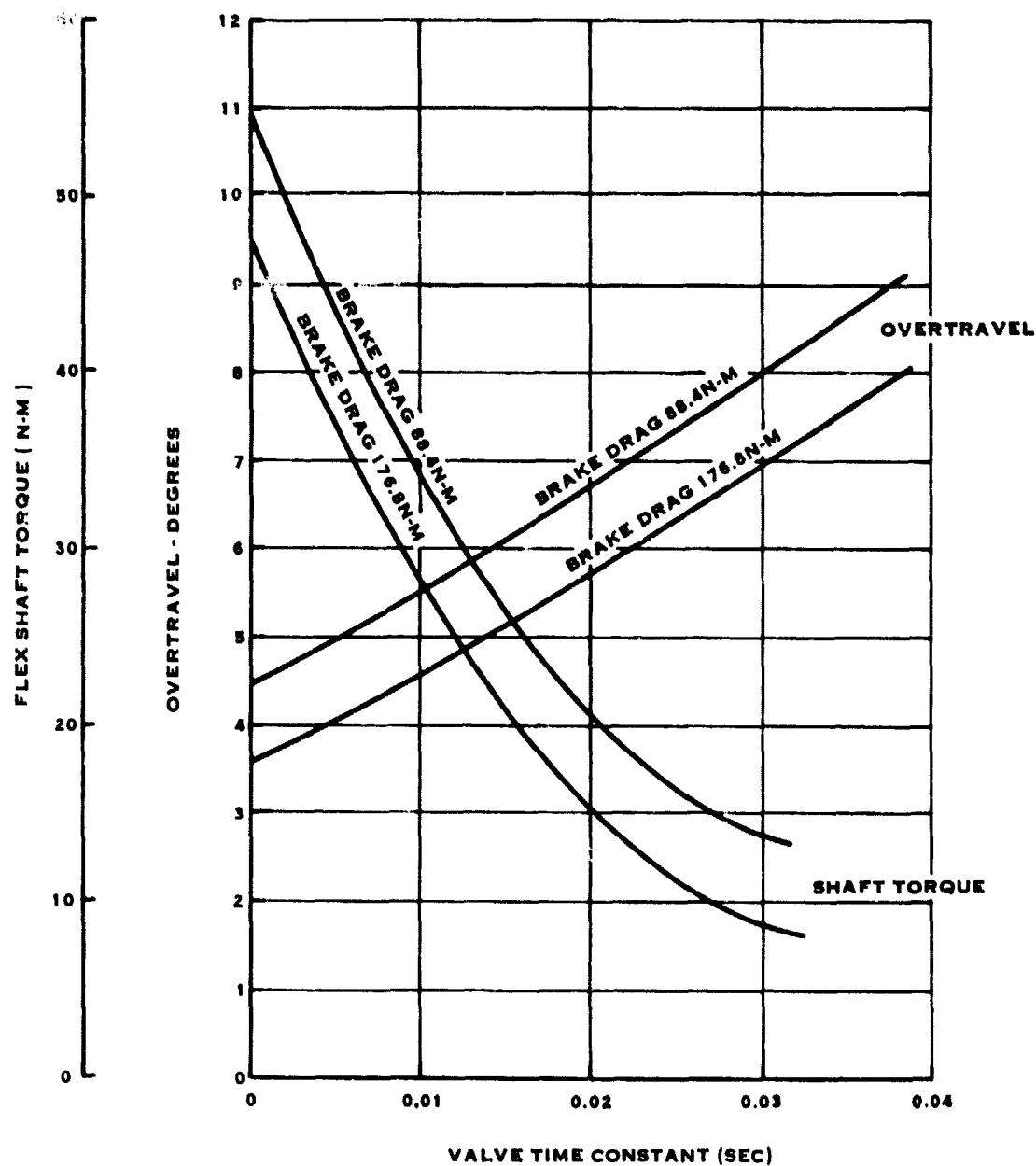


FIGURE 14. CURVE - OVERTRAVEL & SHAFT TORQUE VS VALVE TIME CONSTANT

TABLE V
 ANGLE POSITION ACCURACY
 (ROTATING)
 DATA FROM 12-30-75

	Photo Diode Blade Angle <u>(degrees)</u>	Fan Speed <u>(rpm)</u>
	+ 13.0	2700
	- 2.5	3068
	+ 0.8	3068
	+ 8.0	3068
	+ 4.0	3068
	+ 7.5	3068
	+ 9.5	3068
	+ 7.5	3068
00	-100.5	3068
12.0	+ 13.0	3068

TABLE VI
BLADE ANGLE POSITION ACCURACY
(ROTATING)
DATA FROM 12-30-75

<u>LVDT Blade Angle (degrees)</u>	<u>Photo Diode Blade Angle (degrees)</u>	<u>Fan Speed (rpm)</u>
+12.0	+13.0	2700
- 3.0	- 2.2	2700
0	+ 1.0	2700
+ 7.0	+ 8.5	2700
+ 5.0	+ 6.0	2700
+ 7.0	+ 8.0	2700
+ 9.0	+10.0	2700
+ 7.0	+ 8.0	2700
- 100	-99.5	2700
+12.0	+13.5	2700

TABLE VII
BLADE ANGLE POSITION ACCURACY
(ROTATING)

DATA FROM 12-31-75

<u>LVDT Blade Angle (degrees)</u>	<u>Photo Diode Blade Angle (degrees)</u>	<u>Fan Speed (rpm)</u>
+12.0	+13.0	3068
+ 9.0	+10.5	3068
+ 7.0	+ 8.0	3068
+ 5.0	+ 6.0	3068
0	+ 0.5	3068
- 3.0	- 2.0	3068
- 100	-99.5	3068
- 3.0	- 2.5	3068
0	- 1.0	3068
+ 5.0	+ 5.5	3068
+ 7.0	+ 8.0	3068
+ 9.0	+10.0	3068
+12.0	+13.0	3068

6.0 (Continued)

of 0.07 degrees, a backlash of the trunnion roller to the cam track of 0.14 degrees, and a calibration inaccuracy of 0.10 degrees. The reason for the difference between the measured and expected value is not known, but could be the result of larger than designed mechanical errors or backlash.

Figure 15 is a sketch of the test setup, Table VIII is a summary of the data taken during the test, and Figure 16 is a plot of the data. It should be noted that this is the maximum hysteresis and would only occur at full reverse during normal operation. During forward thrust operation, the actuator is always loaded towards close.

The results of testing to determine the pressure required to start and sustain blade motion are listed in Table IX. In those cases where more than one set of data is given for an excursion, the blades moved a few degrees, stopped, and then moved again as pressure was raised. The data given as "To Sustain" should have been taken when the blades were moving at a constant rate. As most of the excursions were very short, this was not the case. Even in the excursions to and from reverse, the motor flow could not be restricted enough for a constant pitch change rate to be established. The data given for sustaining was taken at a point where the pressure was constant, or almost constant, for a short period of time. The pressures required to start and sustain motion was well within the 3000 psi available for all cases tested. Sanborn traces of this test are included in Appendix C.

Actuator efficiency was determined at the input to the differential gear train where the actual torque on the ground sun gear was measured. Efficiencies were calculated based on data obtained during transient operation of the pitch change actuator. Since these were not steady state pitch change rates, the possibility of errors in the absolute numbers are greater and the results should therefore be used in a manner which reflects this possibility. The efficiencies determined were higher than anticipated, and were in the 70% range. The following tabulation summarizes the measured efficiencies.

Blade Angle (deg)	Direction of Motion	Fan Speed (rpm)	Efficiency (%)
-110	Open	3000	76
-100	Close	3000	73
- 66	Close	2500	71
- 50	Close	2350	75
+ 10	Open	2500	73

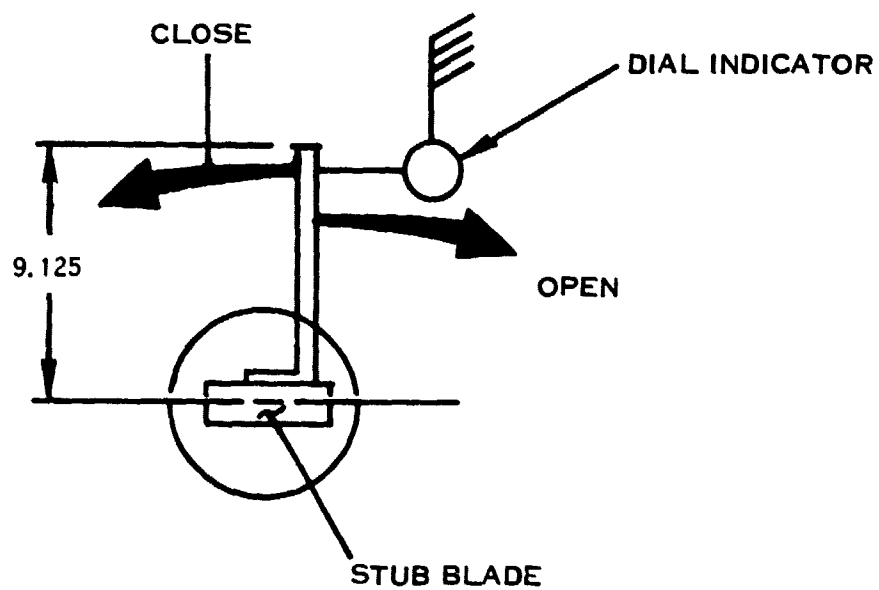


FIGURE 15. TEST SETUP BLADE ANGLE POSITIONING ACCURACY (STATIC)

TABLE VIII
BLADE ANGLE POSITION ACCURACY
STATIC
DATA FROM 2-14-76
BASED ON LVDT #1 CALIBRATION 2-5-76

LVDT Reading (volts)	Set Blade Angle (degrees)	Dial Indicator Reading (inches)	Δ Dial Indicator Reading (inches)	Δ Blade Angle (degrees)	Resultant Blade Angle (degrees)
1.670	-2.000	0.758	0	0	-2.000
1.678	-1.787	0.730	0.028	0.176	-1.824
1.686	-1.574	0.690	0.040	0.250	-1.574
1.693	-1.387	0.666	0.024	0.151	-1.423
1.700	-1.200	0.638	0.028	0.176	-1.247
1.708	-0.987	0.612	0.026	0.163	-1.084
1.715	-0.800	0.582	0.030	0.188	-0.896
1.723	-0.587	0.548	0.034	0.213	-0.683
1.730	-0.400	0.522	0.026	0.163	-0.520
1.738	-0.187	0.486	0.036	0.226	-0.294
1.745	0	0.461	0.025	0.157	-0.137
1.753	+0.213	0.426	0.035	0.220	+0.083
1.760	+0.400	0.400	0.026	0.163	+0.246
1.768	+0.613	0.369	0.031	0.195	+0.441
1.776	+0.826	0.335	0.034	0.213	+0.654
1.784	+1.039	0.306	0.029	0.182	+0.836
1.791	+1.226	0.280	0.026	0.163	+0.999
1.798	+1.413	0.253	0.027	0.170	+1.169

TABLE VIII (Continued)

LVDT Reading (volts)	Set Blade Angle (degrees)	Dial Indicator Reading (inches)	Δ Dial Indicator Reading (inches)	Δ Blade Angle (degrees)	Resultant Blade Angle (degrees)
1.805	+1.600	0.225	0.028	0.176	+1.345
1.813	+1.813	0.189	0.036	0.226	+1.571
1.820	+2.000	0.160	0.029	0.182	+1.753
1.813	+1.813	0.160	0	0	+1.753
1.805	+1.600	0.160	0	0	+1.753
1.798	+1.413	0.160	0	0	+1.753
1.791	+1.226	0.160	0	0	+1.753
1.784	+1.039	0.158	0.002	0.013	+1.740
1.776	+0.826	0.183	0.025	0.157	+1.583
1.768	+0.613	0.213	0.030	0.188	+1.395
1.760	+0.400	0.245	0.032	0.201	+1.194
1.753	+0.213	0.276	0.031	0.195	+0.999
1.745	0	0.306	0.030	0.188	+0.811
1.738	-0.187	0.332	0.026	0.163	+0.648
1.730	-0.400	0.365	0.033	0.207	+0.441
1.723	-0.587	0.390	0.025	0.157	+0.284
1.715	-0.800	0.426	0.036	0.226	+0.058
1.708	-0.987	0.457	0.031	0.195	-0.137
1.700	-1.200	0.488	0.031	0.195	-0.332
1.693	-1.387	0.515	0.027	0.170	-0.502
1.686	-1.574	0.540	0.025	0.157	-0.659
1.678	-1.787	0.573	0.033	0.207	-0.866
1.670	-2.000	0.606	0.033	0.207	-1.073

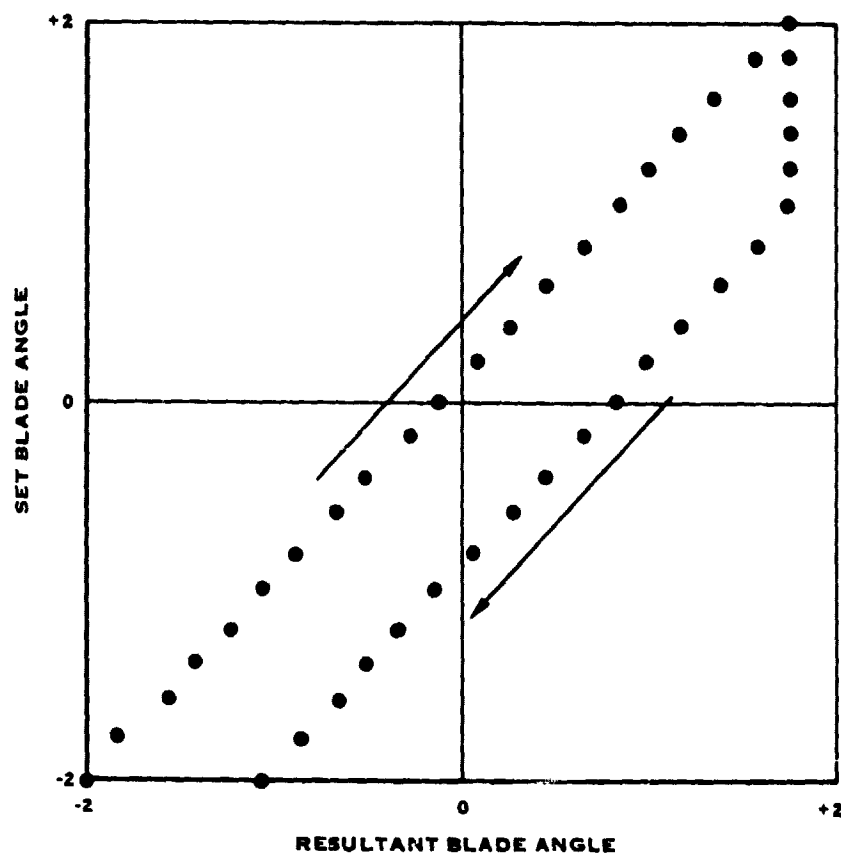


FIGURE 16. BLADE ANGLE POSITION ACCURACY DATA FROM 2-14-76
SET BLADE ANGLE VS. RESULTANT BLADE ANGLE

TABLE IX. PERFORMANCE

Data from 12-31-75

Blade Angle Excursion (degrees)	Fan Speed (rpm)	Pressure to		Torque to		Pitch Change Rate (max) (degrees/ sec)
		Start Motion (psig)	Start Motion (newtons/ cm ²)	Sustain Motion (psig)	Sustain Motion (newtons/ cm ²)	
+12 to -3	2700	950	655.0	1000	689.4	3.75
(+10.5)	2700	1100	758.4	1100	758.4	22.5
-3 to 0	3408	400	275.8	250	172.4	11.25
0 to +7	3068	450	310.2	250	172.4	18.75
+7 to +5	3068	1600	1103.1	1000	689.4	7.5
+5 to +7	3068	400	275.8	200	137.9	3.75
+7 to +9	3068	300	206.8	200	137.9	11.25
+9 to +7	3068	1000	689.4	1000	689.4	5.25
+7 to -100	3068	1500	1034.2	1200	827.3	11.25
-100 to +7	2700	1600	1103.1	400	275.8	75.0
		1000	689.4	1000	689.4	22.5
	2700	1600	1103.1	1000	689.4	67.5

6.0 (Continued)

The average pitch change rate for a blade angle excursion from -3 degrees to -100 degrees at 3315 fan rpm with a EHV supply pressure of 2378.6 ± 34.4 newtons per square centimeter (3450 ± 50 psig) was 116 degrees per second. The maximum rate attained was 135 degrees per second. A Sanborn trace of this test is included in Appendix C. The design objective was 135 degrees per second maximum.

The minimum blade angle change which could be achieved around 0 degrees with a fan speed of 3408 rpm and a EHV supply pressure of 2378.6 ± 34.4 newtons per square centimeter (3450 ± 50 psig) was 0.17 degrees in the open direction and 0.26 degrees in the close direction based on LVDT motion. The design objective was 0.5 degrees.

With the blade angle set at -100 degrees, EHV supply pressure at 0, and the fan speed increased from 0 to 3578 rpm, no blade angle change occurred based on LVDT readout indicating that the no back mechanism did not slip.

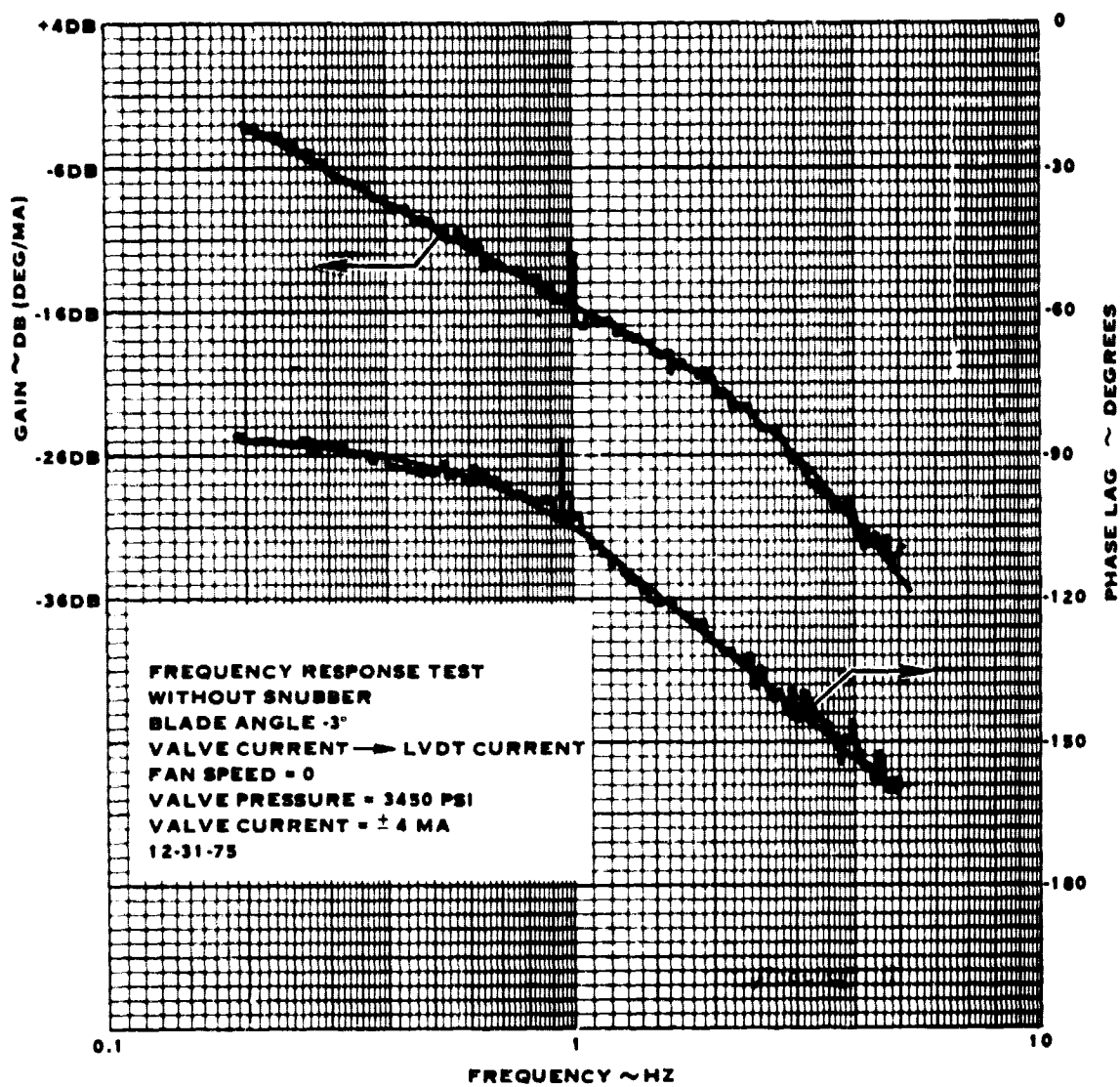
With the blade angle set at 0 degrees, EHV supply pressure at 0, and fan speed increased from 0 to 3408 rpm, no blade angle change occurred based on LVDT readout indicating that the no back mechanism did not slip.

The results of the frequency response testing are presented in Figures 17 through 22. The data in Figures 17 through 20 is for the actuator without a snubber while the data in Figures 21 and 22 is for the actuator with a snubber. In general, the actuator without the snubber indicated reasonable correlation with the predicted performance in the frequency range up to 1 Hertz; magnitude ratio was lower and phase shift was higher than at frequencies above 1 Hertz. The actuator with the snubber indicated reasonable correlation in the frequency range up to 1 Hertz when excitation magnitudes were ± 8 ma. However for ± 4 ma excitation the magnitude ratio was down and there was considerable phase shift.

Possible causes of the deviation between the test results and the design intent are high internal leakage in the hydraulic motors, higher than anticipated friction values, and lags due to the snubber.

A total of 500 endurance cycles at pitch change rates up to 75 degrees/second, were conducted on the actuator prior to installation of the snubber, and an additional 50 cycles at pitch change rates up to 135 degrees/second after snubber installation. Sanborn traces of a typical cycle are included in Appendix C.

Copies of the log sheets generated during the test are included in Appendix D, and a test chronology is included in Appendix E.



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FIGURE 17. QCSEE FREQUENCY RESPONSE

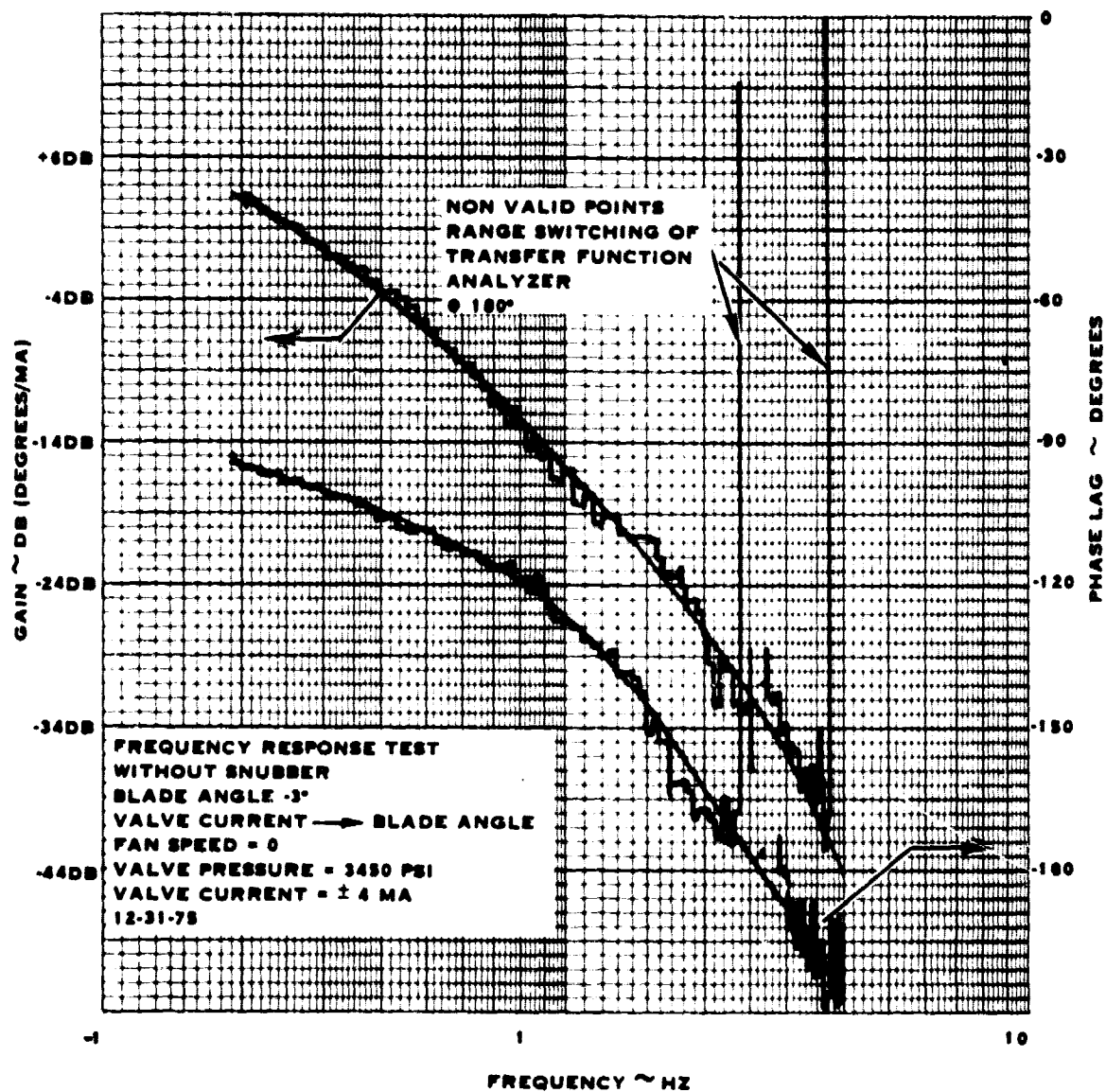


FIGURE 18. QCSEE FREQUENCY RESPONSE

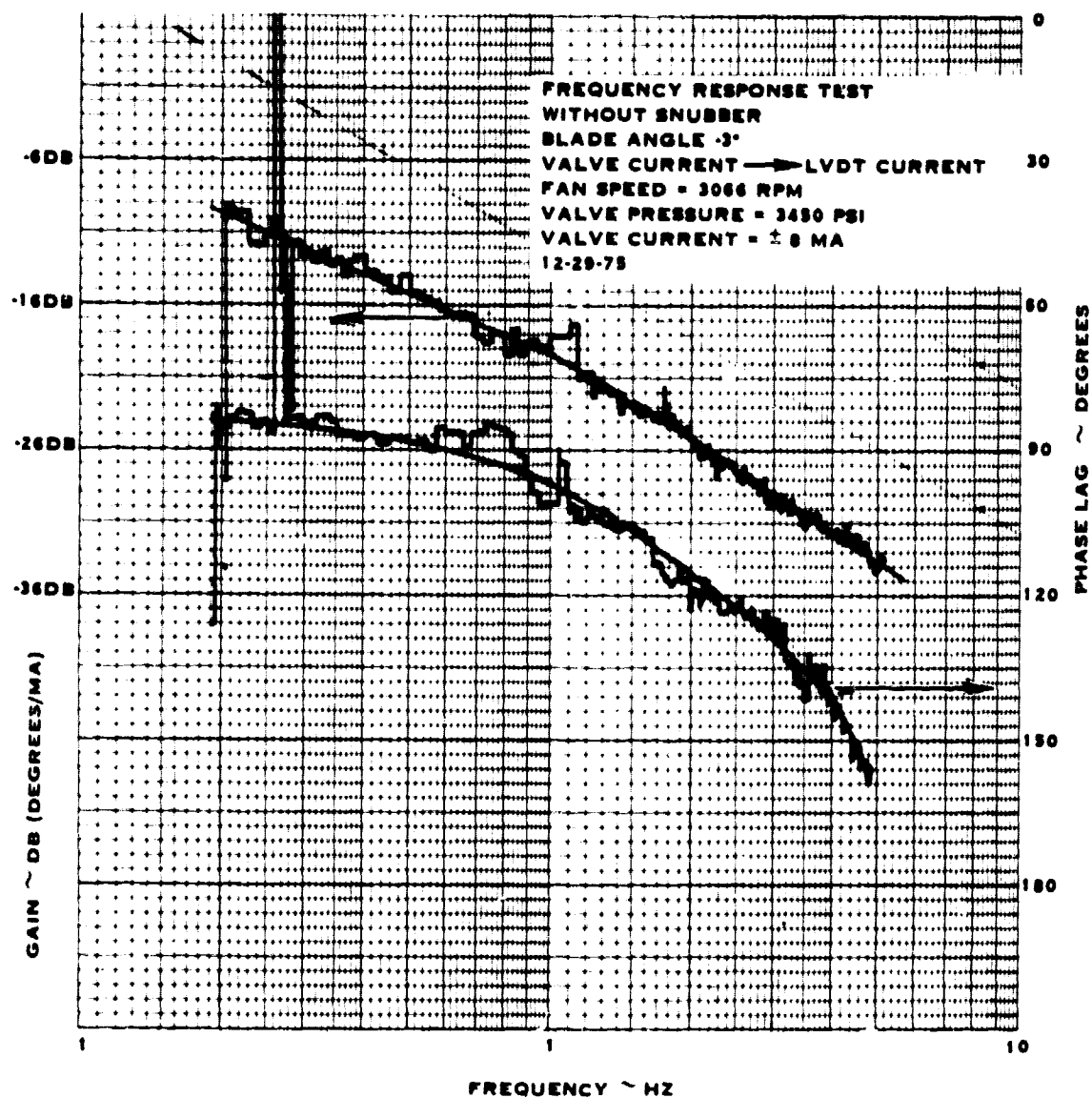


FIGURE 19. QCSEE FREQUENCY RESPONSE

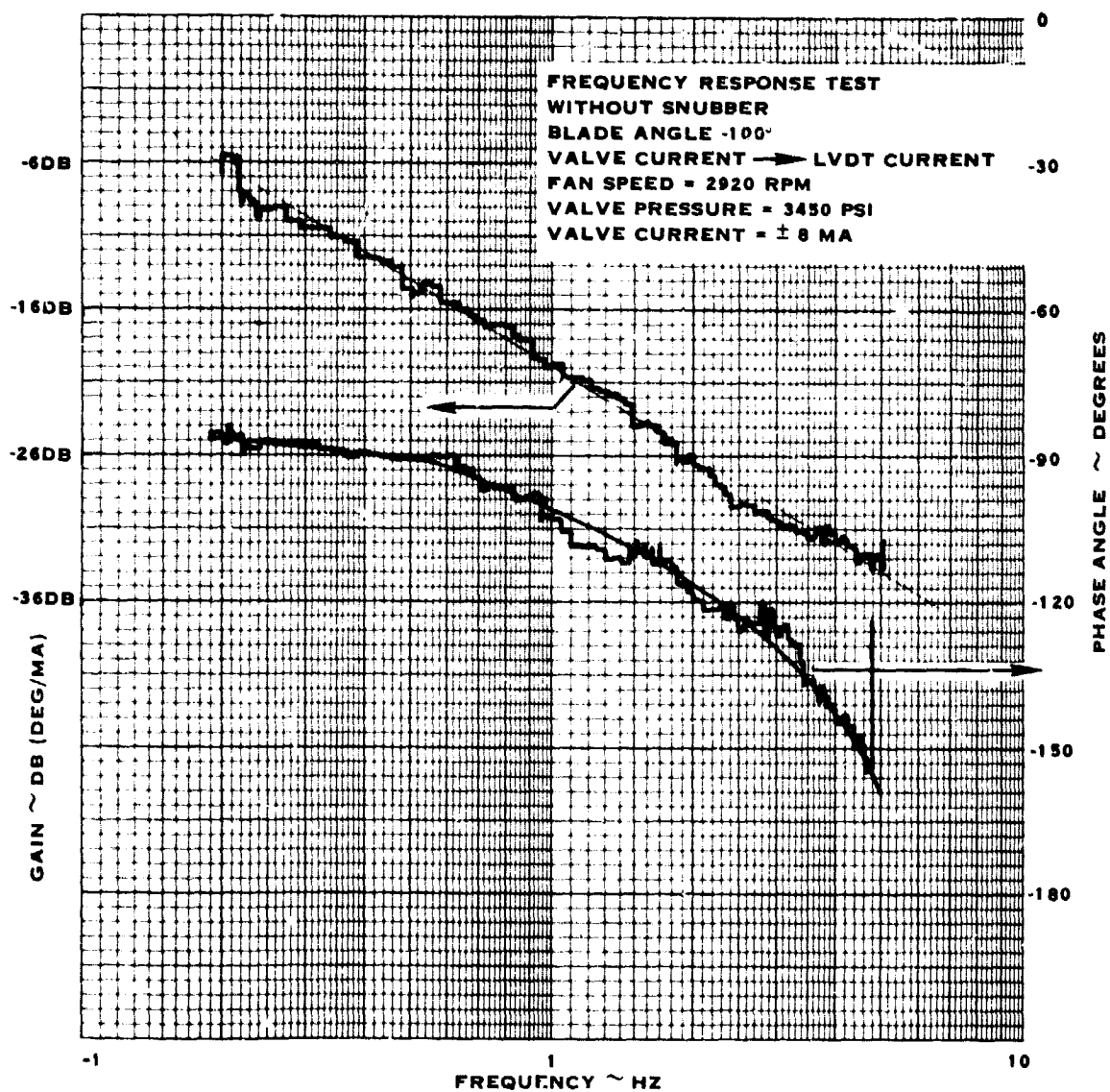


FIGURE 20. QCSEE FREQUENCY RESPONSE

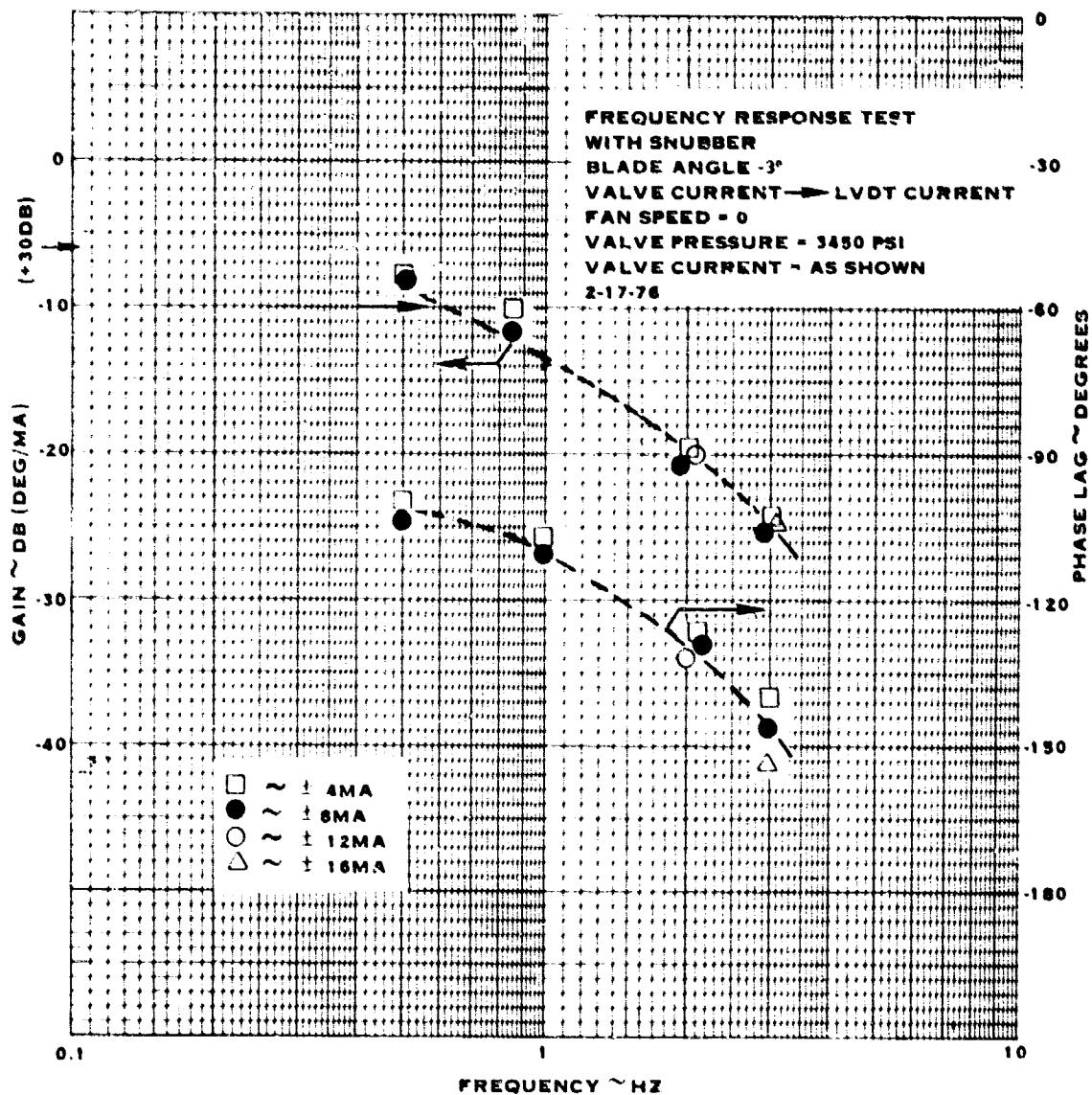


FIGURE 21. QCSEE FREQUENCY RESPONSE

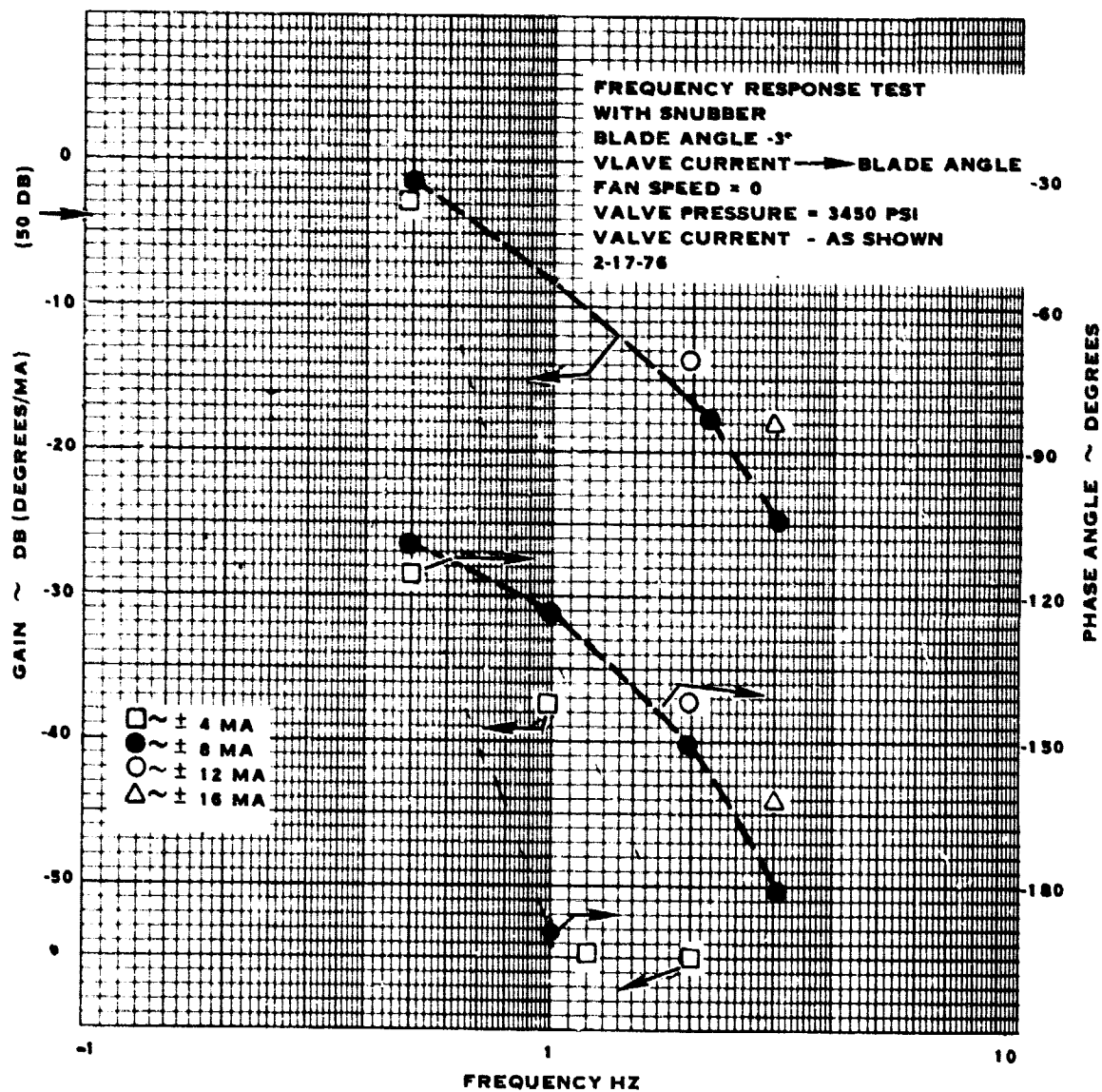


FIGURE 22. QCSEE FREQUENCY RESPONSE

7.0 CONCLUSION

The results of the whirl rig testing shows that the pitch change actuator system, incorporating the snubber, satisfies the design requirements and is structurally adequate for use on the QCSEE being developed for NASA.

The pitch change actuator system was subsequently shipped to General Electric for installation in the engine.

8.0

APPENDICES

222PT-37

OPERATING PROCEDURE

FOR

QCSEE ACTUATOR

WHIRL RIG

November 5, 1975

Prepared by: R) 20.2 - 251

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CONTENTS

- 1.0 GENERAL
- 2.0 RESPONSIBILITIES
- 3.0 RIG OPERATION
 - 3.1 General
 - 3.2 Test Item
 - 3.3 Pre Run Inspection
 - 3.4 Rig Start-up
 - 3.5 Rig Shutdown
 - 3.6 Emergency Shutdown
 - 3.7 After Operation Inspection
 - 3.8 Operating Limits
- 4.0 INSPECTION OF HARDWARE
- 5.0 RIG INSTRUMENTATION
- 6.0 LOG SHEETS
 - 6.1 Frequency
 - 6.2 Content
 - 6.3 Recorded Data

1.0 GENERAL

The purpose of this document is to define a procedure for operating the QCSEE pitch change actuator on the Hamilton Standard whirl test rig (G-7 in the Hydraulics Lab). Copies of this operating procedure will be distributed as follows:

- Test Rig - 2 copies
- Facilities Group - 1 copy
- Engineering - 6 copies (Project and Design)
- Lab Supervision - 2 copies
- Instrumentation - 2 copies

This document takes precedence over test plans as far as rig operating procedure is concerned. The Test Director will resolve all conflicts.

2.0 RESPONSIBILITIES

All persons associated with the QCSEE actuator test program will be required to conform to the operating principles defined in this document. The actual conduct of the test, in accordance with an approved test plan, will be under the control of a Test Director appointed from the Propeller Project Group. Conduct of the test will be the responsibility of this Test Director or his designated representative.

3.0 RIG OPERATION

3.1 General - The rig will be operated, at all times, in accordance with these instructions.

3.2 Test Item - The actuator assembly is defined by drawings 763499 (Beta Regulator) and 763500 (Actuator). Installation and removal of this hardware will be accomplished in accordance with HS 6971 - "Assembly and Test of QCSEE Actuator".

3.3 Pre-Run Inspection - Immediately prior to starting the rig, an inspection must be performed and a "Pre-Run Check List" filled out and signed by both the Rig Operator and the cognizant Engineer conducting the test. A new check list must be filled out if any work is done on instrumentation, rig or test item.

3.4 Rig Start-Up

3.4.1 Check to insure that the following has been accomplished:

- a) Gear box lube system on.
- b) Clutch water on.
- c) Actuator control system on.
- d) Rig speed control set for "manual".
- e) Drive motor on.

Energize clutch control and bring speed up to 500 rpm. If operation is satisfactory, increase speed to 2000 rpm and record a set of data per paragraph 6.0 before proceeding to test plan.

3.5 Rig Shutdown - Normal rig shutdown will be accomplished, with the rig speed control set at the manual position, by reducing rig speed setting to zero and turning off the clutch and drive motor.

3.6 Emergency Shutdown - If an incident or change in readings occur which the Engineer or Operator judge requires an emergency shutdown, the following procedure will be followed:

- a) Turn drive motor power off.
- b) After disc coasts down, turn off gear box lube, actuator lube and actuator hydraulic system.
- c) Immediately write down all observations noted at the time the incident occurred and mark Sanborn record with time and character of incident.

3.7 After Operation Inspection - Immediately following rig shutdown, when it is intended that some changes will be made on the test item, or when the rig will be down for more than 30 minutes, a "Post Run Check List" must be filled out by the Engineer and the Operator.

3.8 Operating Limits - The following are the operating limits which should not be exceeded at any time during operation of this rig:

Fan Speed	3600 rpm max.
EHV Supply Pressure	3800 psi max.
EHV Supply Temperature	250°F max.
Beta Regulator Speed	22,000 rpm max.
Lube Oil Flow	.8 - 1.0 qts/min.
Lube Oil Temperature (Actuator)	250°F max.
Cell Temperature	150°F max.
Vibration	2 mils max.
Clutch Water Temp.	180°F max.
Shaft Torque	125 in-lbs. max.

4.0 INSPECTION OF HARDWARE

Hardware inspection intervals will be established by the Test Director based on results obtained during the test program.

5.0 RIG INSTRUMENTATION

Instrumentation will be provided on the rig to obtain the data defined in Table I. All measurements noted as recording will be continuously recorded at a paper speed of .1 in/sec.

6.0 LOG SHEETS

A log sheet shall be maintained for all running of the actuator or its components on this rig.

6.1 Frequency - Entries shall be made on this log sheet in accordance with the following schedule:

- a) For each start.
- b) Each new functional test condition being evaluated or at 15 minute intervals.
- c) For the first endurance cycle of the run and for every fifth endurance cycle thereafter. Readings to be taken at the start and completion of each cycle.
- d) Prior to shutdown.
- e) As requested by Test Director.

6.2 Content - The log sheets will include the following information:

- a)* Date and time of entry.
- b) Name of test - G.E. QCSEE Actuator - Functional (or Endurance) Test.
- c) Rig Speed
- d) Blade Angle (from control readout)
- e)* Lube oil flow
- f)* Lube oil temperature
- g)* Lube oil pressure
- h)* EHV Supply Pressure
- i)* EHV Supply Temperature
- j) Cell temperature
- k)* Vibration - horizontal and vertical
- l) Clutch temperature
- m) G.B. oil pressure
- n) Test plan paragraph
- o)* Cycle number
- p) Operator and Engineer's name

* Record only these for 6.1(c).

6.3 Recorded Data - Data noted as recording on Table I will be recorded continuously at a record speed of 0.1 in/sec. unless a faster speed is required for the particular test being conducted. All records will be suitably marked with test plan paragraph number or cycle number and date and time for identification and to permit correlation with the rig log sheets.

TABLE 1

<u>Measurement</u>	<u>Range</u>	<u>Type</u>
EHV Supply Pressure	0-4000 psig	Visual
EHV Current Signal	± 100 ma	Recording
Flow to EHV	0-45 gal/min	Recording
4 P Across Motor (1)	0-3500 psig	Recording
Fluid Temperature	0-300°F	Visual
Blade Angle Command	+20° to -120°	Visual and Recording
LVDT Feedback Voltage (1)	± 5 V dc	Recording
Flex Shaft Speed	0-24,000 rpm	Recording
Flex Shaft Torque	0-200 in.lb.	Recording
Lube Oil Flow	0-1 qt/min.	Visual
Lube Oil Pressure	0-100 psig	Visual
Lube Oil Temperature	0-300°F	Visual
Fan Speed	0-3700 rpm	Visual and Recording
Cell Temperature	0-300°F	Visual
Vibration - Horizontal		Visual
Vibration - Vertical		Visual
Fan Blade Angle	+20° to -120°	Visual

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POST RUN CHECK LIST
QCSEE ACTUATOR - G-7 RIC

Date: _____
Rig Time: _____
Flight Cycles: _____

Item	Condition	Initial	
		Operator	Engineer
1 All hardware appears structurally sound.			
2 No evidence of oil leakage.			
3 Arm, disc and cam area clean, dry and free of foreign objects.			
4 All visible bolts, nuts, mounts, etc. appear secure.			
5 All pumps shut off.			
6 Disc and actuator covered up if unit will be shut down for any period of time and is not being worked on.			
7 All data recorded and records properly marked.			

REMARKS -

HSER 7002

11/4/75

FRE RUN CHECK LIST

QCSEE ACTUATOR - G-7 RIC

Date: _____

Rig Time: _____

Flight Cycles: _____

Item	Condition	Initial	
		Operator	Engineer
1 Disc uncovered.			
2 Instrumentation connected and operating.			
3 Arm, disc and cam area clean, dry and free of foreign objects.			
4 All visible bolts, nuts, mounts, etc. appear secure.			
5 Stop switches correctly set and Beta Regulator indexed to actuator (feedback and actual blade angle agree).			
6 Hydraulic pumps on, bypass closed and correct pressure at servo valve (per test plan).			
7 Actuator lube pump on and set for _____ psi at Beta Regulator.			
8 All personnel and loose material out of cell and cell doors secured.			

REMARKS -

APPENDIX B

TEST PLANS

Hamilton Standard

WINDSOR LOCKS, CONNECTICUT • U.S.A.

DIVISION OF UNITED AIRCRAFT CORPORATION

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A

HSER 7002

PAGE 1 OF 12

No. 222PT-31 Rev. ADATE: 10/28/75**PLAN OF TEST**ITEM: 763500 Actuator (QCSEE)PREPARED BY: D. LeishmanCONTRACT: GE 200-4XX-14G-38570APPROVED BY: [Signature]

TEST PERIOD: _____

1. WHAT IS ITEM BEING TESTED?
2. WHY IS TEST BEING RUN? WHAT WILL RESULTS SHOW OR BE USED FOR?
3. DESCRIBE TEST SETUP INCLUDING INSTRUMENTATION, ATTACH SKETCH OF INSTALLATION.
4. ITEMIZE RUNS TO BE MADE GIVING LENGTH OF EACH AND READINGS TO BE TAKEN.
5. SPECIAL INSTRUCTIONS: SAFETY PRECAUTIONS FOR OPERATORS AND HANDLING EQUIPMENT. OBSERVATIONS BY SIGHT, FEEL, OR HEARING. LIST POINTS OF OBSERVATION WHICH MIGHT CONTRIBUTE TO ANALYSIS OF (A) PERFORMANCE OF UNITS. (B) INCIPIENT TROUBLE BEFORE IT OCCURS, AND (C) CAUSE OF FAILURE.
6. HOW WILL DATA BE USED OR FINALLY PRESENTED? GIVE SAMPLE PLOT, CURVE, OR TABULATION AS IT WILL BE FINALLY PRESENTED.

NUMBER ENTRY AS LISTED ABOVE AND DESCRIBE BELOW

1.0	The item being tested is the pitch change actuator for the QCSEE assembled for reverse through stall operation.
2.0	The test is being run to determine the operating characteristics of the actuator, verify that it satisfies the design requirements, and assure its structural adequacy for use in an engine test.
3.0	The actuator, together with a disc and stub blades supplied by GE will be mounted in G-7 Whirl Rig which has been modified to accept the unit. Reference Figure 1. A closed loop variable gain control system with a capability to vary gain between 570 and 2700 ma/volt/volt excitation will be utilized for the test. The instrumentation to be used during the test is listed in Table 1. Figure 2 is a drawing showing the hardware necessary to convert the actuator to a front flex shaft input, and Figure 3 is a lubrication schematic of the actuator.
4.0	The following tests will be conducted. All blade angles are in GE terms. Figure 4 is a plot of blade angle vs. counterweight angle.

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TABLE 1

<u>Measurement</u>	<u>Range</u>	<u>Type</u>
EHV Supply Pressure	0-4000 psig	Visual
EHV Current Signal	<u>+100</u> ma	Recording
Flow to EHV	0-45 gal/min	Recording
4 P Across Motor (1)	0-3500 psig	Recording
Fluid Temperature	0-300°F	Visual
Blade Angle Command	+20° to -120°	Visual and Recording
LVDT Feedback Voltage (1)	<u>+5</u> V dc	Recording
Flex Shaft Speed	0-24,000 rpm	Recording
Flex Shaft Torque	0-200 in.lb.	Recording
Lube Oil Flow	0-1 qt/min.	Visual
Lube Oil Pressure	0-100 psig	Visual
Lube Oil Temperature	0-300°F	Visual
Fan Speed	0-3700 rpm	Visual and Recording
Cell Temperature	0-300°F	Visual
Vibration - Horizontal		Visual
Vibration - Vertical		Visual
Fan Blade Angle	+20° to -120°	Visual

- 4.1 Lubrication Flow Check
 - 4.1.1 With the flex drive shaft disconnected from the actuator, determine the pressure setting necessary at the beta regulator to obtain a flow of .85 qts/min through the shaft at a shaft speed of 0 rpm.
- 4.2 LVDT Null & Calibration (fan speed = 0 rpm)
 - 4.2.1 Using the manual input to the Beta Regulator, determine the LVDT output and blade angle at the mechanical stops of the actuator. Reset the LVDT null so that the output varies an equal amount on either side of null as the blade moves through the full range of travel.
 - 4.2.2 Using the manual input to the Beta Regulator, calibrate actual blade angle versus LVDT output voltage every 5° over the full range of travel in both increasing and decreasing pitch directions. During this calibration, set the travel limit switch cams to actuate at -8° and -96° blade angle.
- 4.3 Travel Limit Switch
 - 4.3.1 With the travel limit switch cams set for -8° and -96°, and a fan speed of 0 rpm, determine the actual blade angle at which the blades stop when the travel limiting switch is actuated at flex shaft speeds of approximately 6000 rpm, 12,000 rpm and 21,000 rpm. Regulate EHV supply pressure to control rate.
 - 4.3.2 With the travel limit switch cams set for -8° and -96°, and a fan speed of 2500 rpm, determine the actual blade angle at which the blades stop when the travel limit switch is actuated at flex shaft speeds of approximately 6000 rpm, 12,000 rpm and 21,000 rpm.
 - 4.3.3 Reset the travel limit switch cams for +12.5° and -116° or to a modified value if testing does not confirm the calculated values of travel required to stop the system (6.5 -7°).
- 4.4 Blade Angle Position Accuracy
 - 4.4.1 With the EHV inlet pressure set at 2000 +100 psig and a fan speed of 2500 rpm, cycle the actuator in accordance with Table 2. At each condition, record actual vs. LVDT blade angle.

Table 2

Step (Reference Table 5)	Blade Angle
1	+12°
3	-3°
5	0°
6	+7°
7	+5°
8	+7°
9	+9°
10	+7°
12	-100°
15	+12°

- 4.4.2 With the EHV inlet pressure set at 3450 \pm 100 psig, and fan speed as shown, cycle the actuator in accordance with Table 2a. At each condition, record actual vs. LVDT blade angle.

Table 2a

Step (Reference Table 5)	Blade Angle	Fan Speed
1	+12°	2500
3	-3°	3068
5	0°	3068
6	+7°	3068
7	+5°	3068
8	+7°	3068
9	+9°	3068
10	+7°	3068
12	-100°	3068
15	+12°	2500

4.5 Performance

- 4.5.1 Determine the pressure required to start actuator motion in both increasing and decreasing pitch directions for the conditions specified in Table 3.

Table 3

Fan Speed	Starting Blade Angle
2500 rpm	+12° (increasing only)
3068 rpm	+5°
3068 rpm	+7°
3068 rpm	+9°
3408 rpm	0°
3408 rpm	-3°
2500 rpm	-100° (decreasing only)

- 4.5.2 Determine the pressure required to sustain actuator motion for the blade angle excursions specified in Table 4.

Table 4

Fan Speed	Blade Angle Excursion
2500 rpm	+12° to -3°
3408 rpm	-3° to +0°
3068 rpm	0° to +7°
3068 rpm	+7° to +5°
3068 rpm	+5° to +7°
3068 rpm	+7° to +9°
3068 rpm	+9° to +7°
3068 rpm	+7° to -100°
2500 rpm	-100° to +12°

- 4.5.3 Determine the average pitch change rate for a blade angle excursion from -3° to -100° at a fan speed of 3315 rpm. EHV supply pressure to be set at 3450 \pm 50 psig. (rate based on LVDT feedback voltage)

- 4.5.4 With the blade angle set at 0°, fan speed of 3408 rpm, and EHV supply pressure 3450 +50 psig, demonstrate the minimum blade angle change which can be obtained around 0°.
- 4.5.5 With the blade angle set at -100°, EHV supply pressure at 0 psig, increase fan speed to 3578 rpm and record any blade angle change.
- 4.5.6 With the blade angle set at 0°, EHV supply pressure at 0 psig, increase fan speed to 3408 rpm and record any blade angle change.
- 4.6 Frequency Response
 - 4.6.1 At a blade angle of -3° and with a fan speed of 0 rpm, determine B_f/ EHV and LVDT/ EHV. Static frequency response and phase angle shall be determined for EHV current peak to peak amplitudes not to exceed +40 ma or that current input which causes a B_f variation of +1.9 to +2.1 degrees at frequencies of 0.5, 1.0, 1.5, 2.0, 3.0, and 4.0 Hz.
 - 4.6.2 Rotating frequency response tests will be conducted to determine Δ LVDT/ Δ EHV.

Two base point conditions will be used:

- 1. Fan speed = 3066 rpm.
B_f = 3° open.
- 2. Fan speed = 2920 rpm.
B_f = 100° open.

Frequency response and phase angle for base point conditions 1 and 2 shall be determined for EHV current peak to peak amplitudes not to exceed +40 ma or that current input which causes a LVDT variation of +.0135 to +.0165 volts/volt at frequencies of 0.5, 1.0, 1.5, 2.0, 3.0, and 4.0 Hz.

- 4.7 Endurance Test
 - 4.7.1 Prior to and at completion of the endurance test, the unit will be disassembled and the hardware will be examined to identify any potential problem areas.
 - 4.7.2 The endurance test will consist of 500 cycles of the actuator in accordance with Table 5. During testing, the EHV supply pressure will be maintained at 3450 +50 psig. The cycles may be run faster than the normal anticipated engine duty cycle in order to shorten the required test time. The cycle frequency will be established during the functional test program. The limiting factor will be the ability of the unit to dissipate the heat generated in the no-back and the clutch. The blade angle must be allowed to stabilize at each point prior to going on to the next point except during modulating operation. (Steps 7-11 of Table 5)

5.0 Special Instructions

Prior to and following operation, the check list shown in Figure 5 must be completed. Note any unusual noises or vibrations, or any changes in noise

TABLE 51 cycle

<u>Step</u>	<u>Fan Speed</u>	<u>Blade Angle</u>
1	2500 rpm	+12°
2	2500	-3°
3	3408	-3°
4	3408	0°
5	3068	0°
6	3068	+7°
7	3068	+5°
8	3068	+7°
9	3068	+9°
10	3068	+7°
11	Repeat steps 7 thru 10 twenty times	
12	3068	-100°
13	3408	-100°
14	2500	-100°
15	2500	+12°

5.0 Continued

or vibration. During the static and performance testing, a log sheet shall be kept which contains the parameters denoted as visual in Table 1 for each test point. Functional test data denoted as recording shall be taken at each test point at a speed commensurate with the test being run.

During the endurance test, a log sheet shall be kept which contains the parameters denoted as visual in Table 1 for the first and each fifth cycle thereafter. Endurance test data denoted as recording shall be taken continuously at a speed of .1 in/sec.

In order to provide a complete time/rpm history for the fan rotor components, data denoted as recording shall be taken at a speed of .1 in/sec at all times when the fan is rotating except when higher recording speeds are needed for a specific test point.

- 6.0 A component test report will be prepared following the completion of the whirl rig tests. Discussions and data presented in the report will cover all tests conducted during the whirl rig test program. All test data will be available for review and use by GE and NASA representatives.

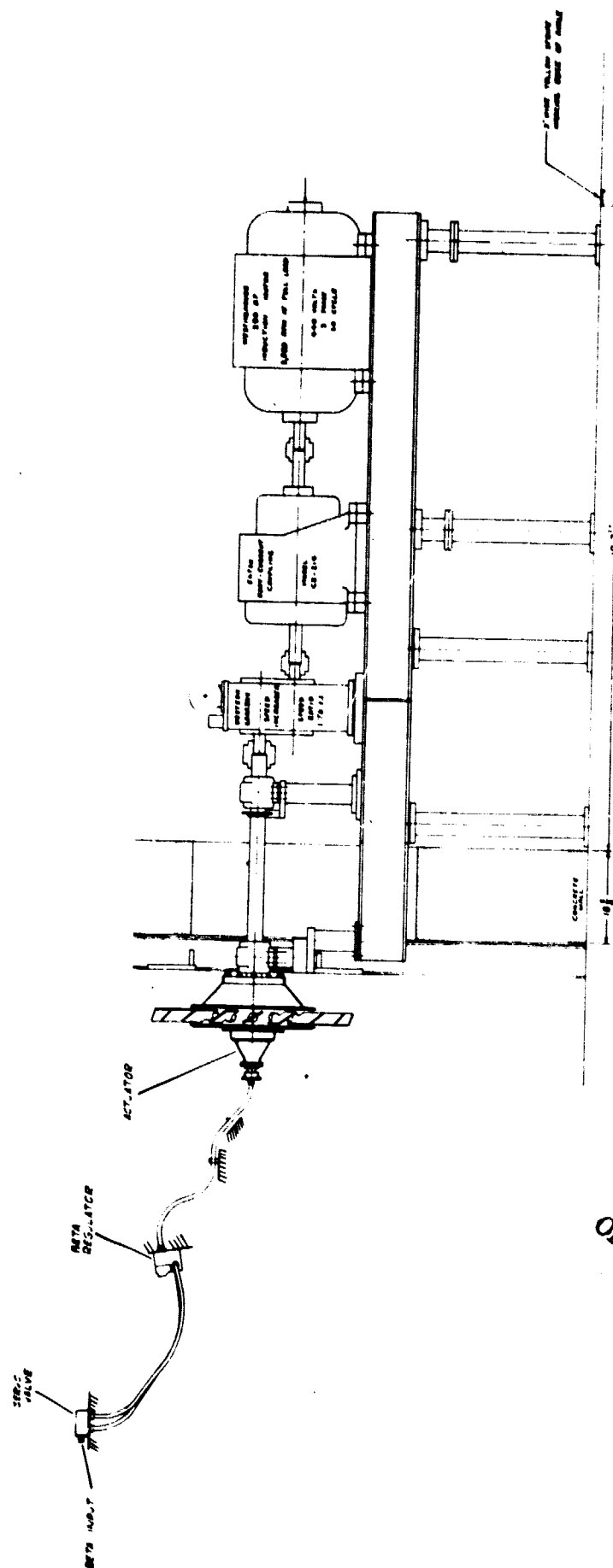


FIGURE 1. WHIRL RIG ARRANGEMENT

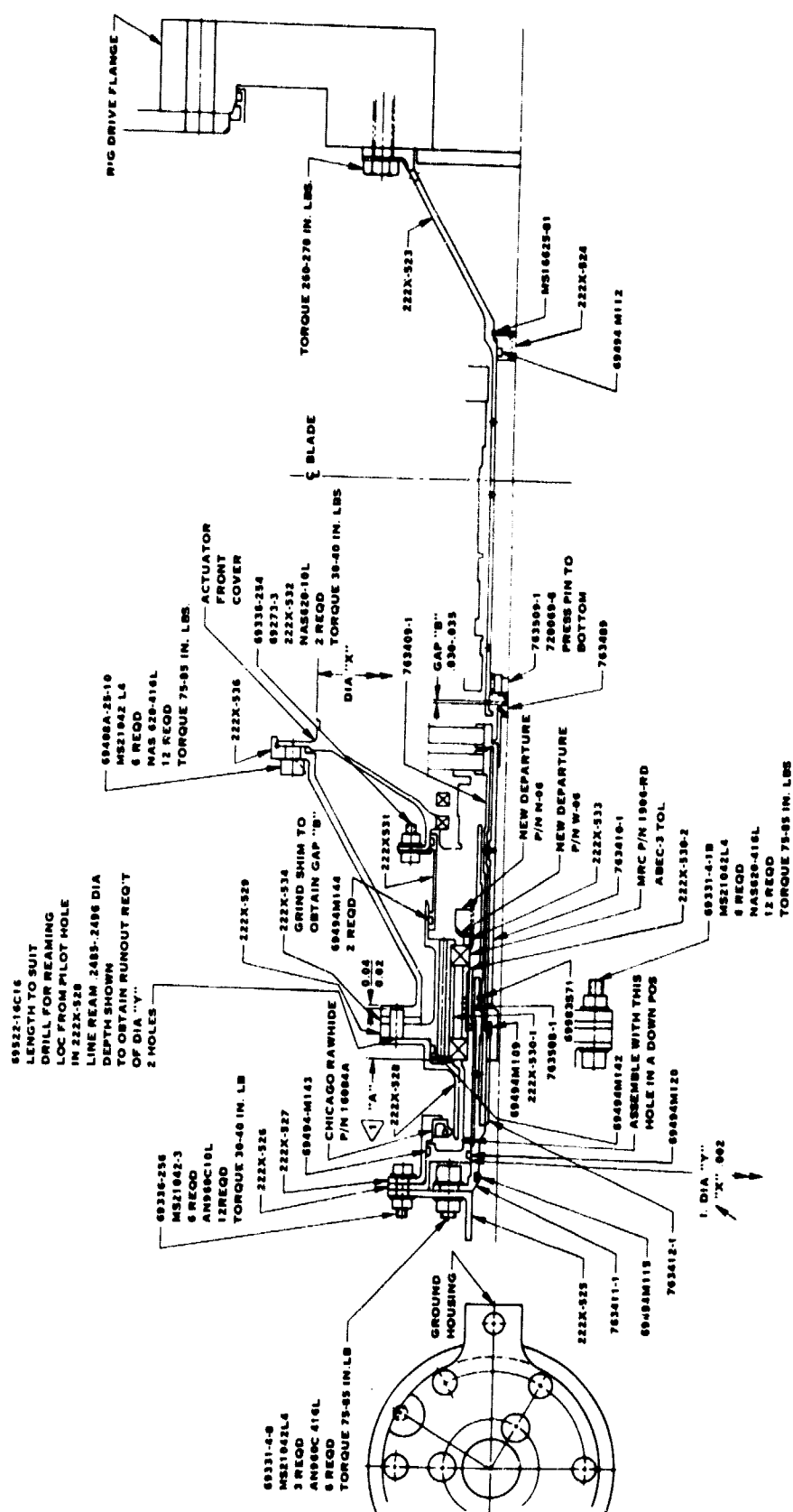


FIGURE 2. ASSEMBLY, FRONT INPUT HARDWARE

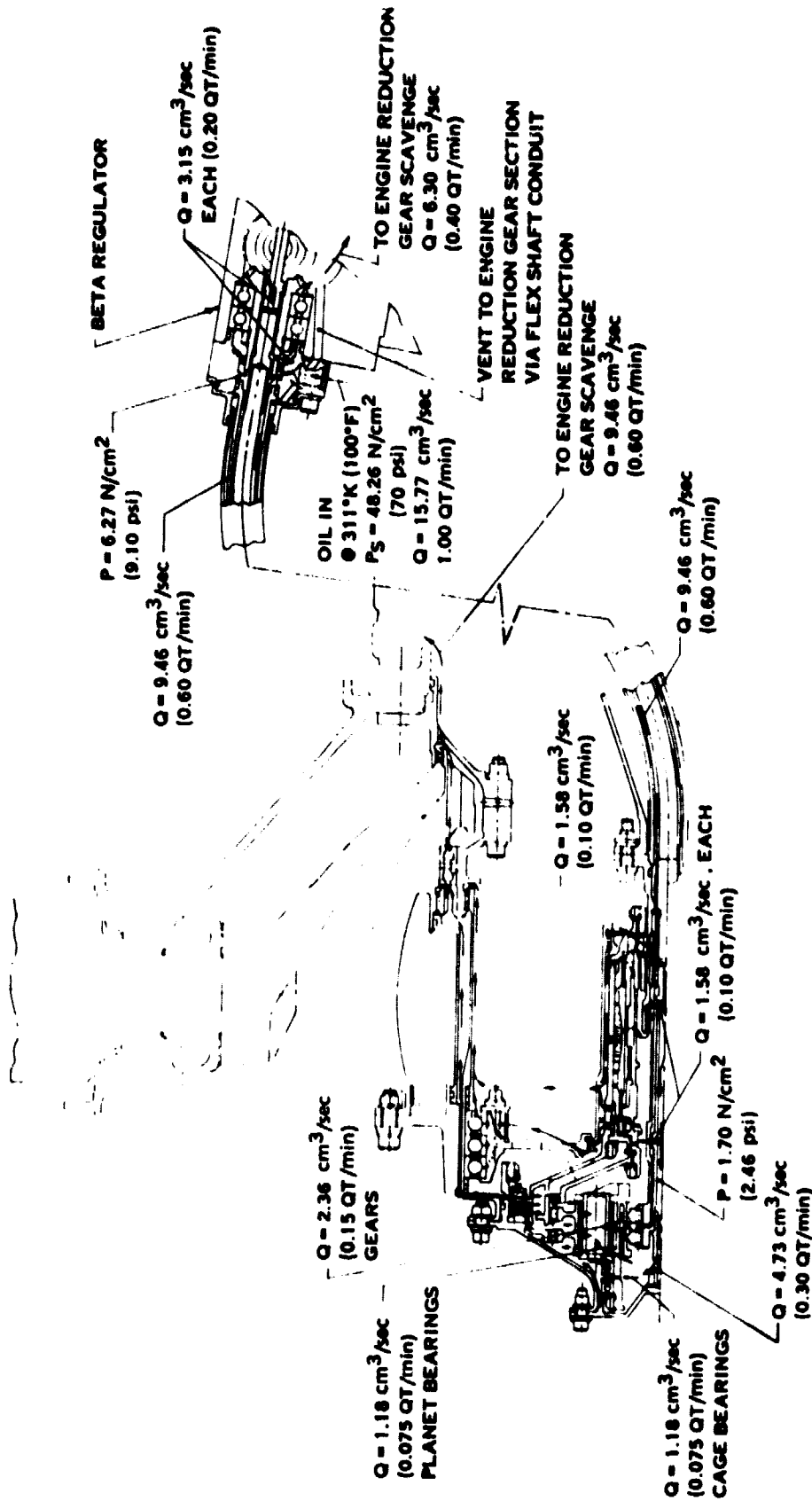


FIGURE 3. LUBRICATION SCHEMATIC

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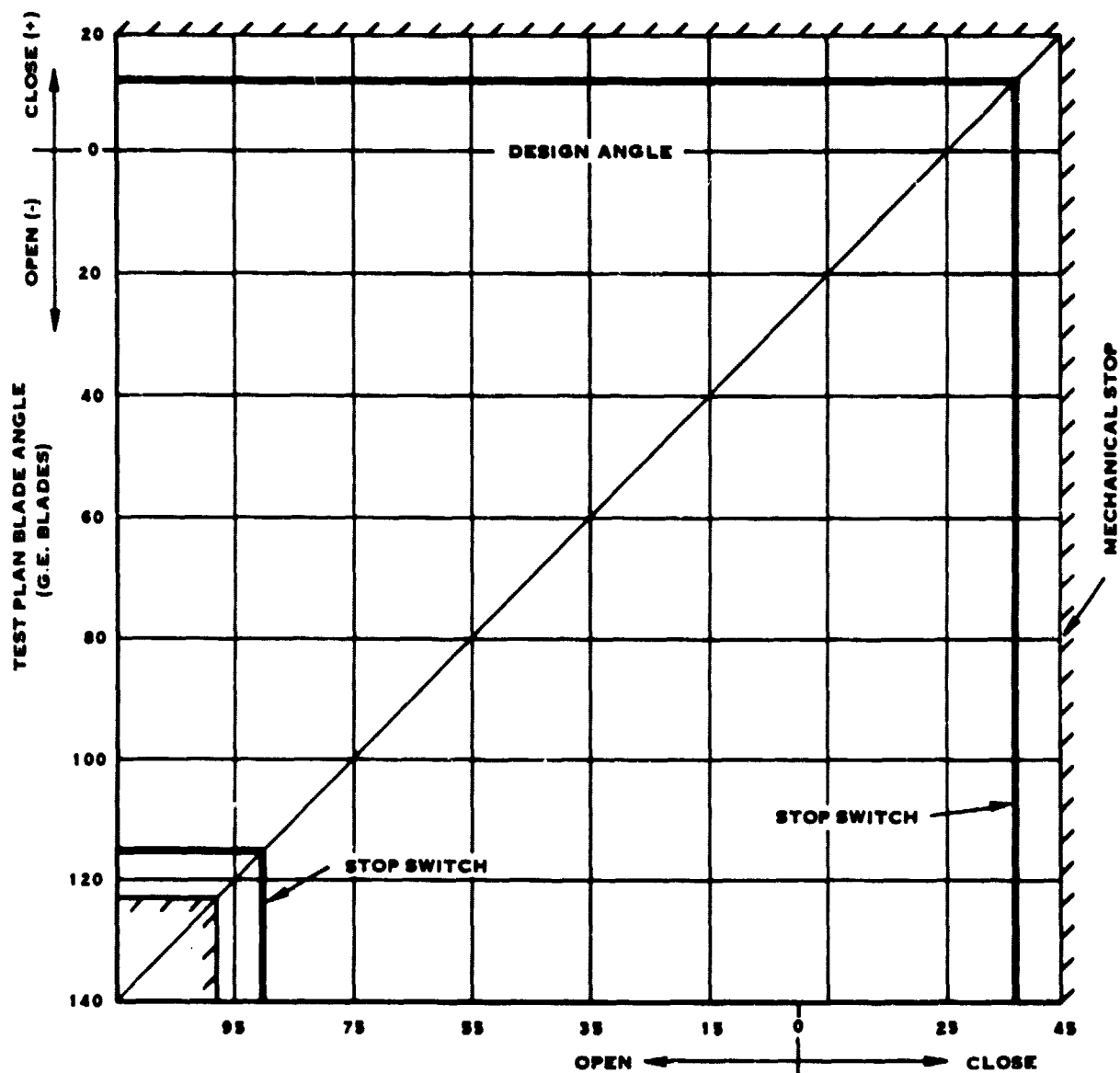


FIGURE 4. QCSEE PITCH CHANGE ACTUATOR TEST PLAN BLADE ANGLE VS. COUNTERWEIGHT ANGLE (TEST PLAN 222 Pt-31 REV. A)

QCSEE ACTUATOR
WHIRL RIG CHECK LIST

Pre Operation

1. Actuator assembled per HS6971
2. System is correctly rigged and indexed
3. Feedback blade angle agrees with actual angle
4. Instrumentation secured
5. Cell cleaned
6. Hydraulic supply pump on
7. Lubrication supply pump on
8. Scavenge pump on

Post Operation

1. Check for leaks
2. Check feedback vs. actual blade angle
3. All required data recorded

FIGURE 5

HAMILTON STANDARD

HSER 7002

Test No. 222PT-38

PLAN OF TEST

Date: 1-30-76Job: 763500 Actuator with Soft Quill ShaftPrepared by: D. E. SmithProject & Order GE 200-4XX-14G-38570

4.0 The following tests will be conducted.

4.1 System Losses

The torque to move the blades will be measured at the beta regulator manual drive when the installation is complete, after each reassembly and following completion of the 50 flight cycles. Torque will be measured in both directions of motion at $+10^\circ$, 0° and -100° of blade angle.

4.2 Blade Angle Calibration

The LVDT's will be calibrated against the position of the counterweights, for both directions of motion. Calibration will be in approximately 2° increments between $+12$ and -10° and 10° increments from -10° to -100° .

4.3 Stop Switches

Stop switches shall be set 6.5° - 7° from the mechanical stops. Stop angle and switch setting will be recorded.

4.4 Max Rate Testing (Ref. 4.5.3 of 222PT-31A)

After checking system operation over entire range and adjusting control settings, perform a reverse transient at 3315 fan rpm and 3450 psi EHV supply pressure. Pump stroke should be adjusted for $10,000 \pm 500$ rpm flex shaft speed. Reduce rig speed to 2700 rpm and unreverse at $10,000 \pm 500$ rpm. Repeat test to obtain two (2) cycles and remove and examine no back and snubber. Determine wind up which snubber experienced.

Reassemble no back and install in rig. Repeat test at $17,500 \pm 500$ flex shaft rpm. Remove and examine no back and snubber and record snubber wind up.

4.5 Endurance Test

Conduct fifty (50) cycles of endurance testing in accordance with paragraph 4.7.2 of 222PT-31A. Max flex shaft speed will be adjusted to achieve 17500 ± 500 rpm during reverse transient portion of run. Following the endurance test, the no back and snubber hardware will be examined.

Test No. 222PT-38

HAMILTON STANDARD

Page 3 of 3

Date: 1-30-76

HSER 7002

Job: 763500 Actuator with Soft Quill Shaft

Prepared by: D. E. Smith

Project & Order GE 200-4XX-14G-38570

4.6 Limit Switch Overtravel

The amount of blade travel required to stop, after tripping the travel limit switches, will be determined at both ends of the operating range. Test will be run statically. For each end of travel, the stopping distance will be determined for flex shaft speeds of 10,000, 12,000, 15,000 and 17,500 rpm (± 500 rpm). The control time constant will be set for .02 seconds initially. If necessary to increase this time constant, the new value shall be recorded on the log sheet.

4.7 Frequency Response

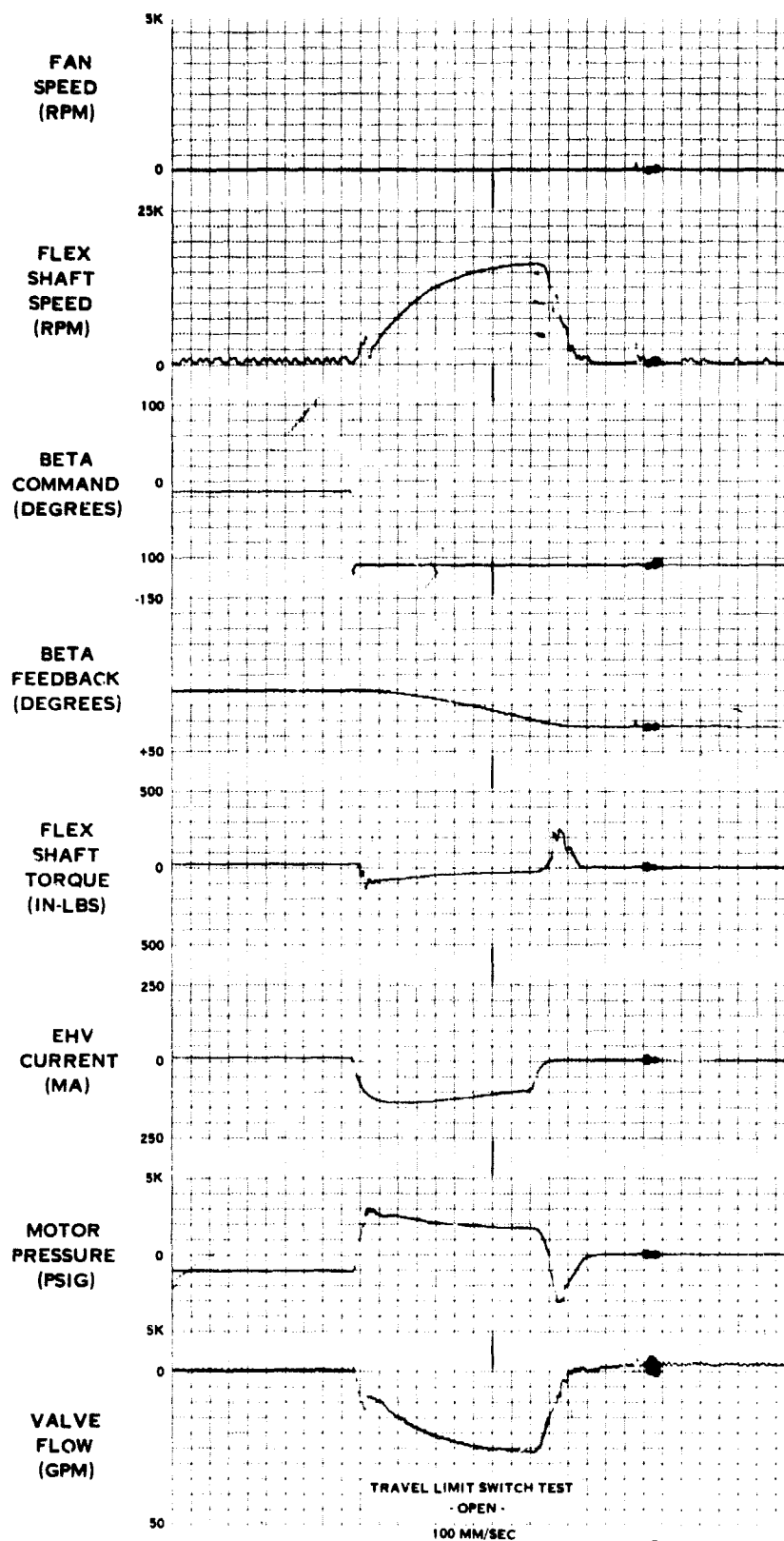
The static frequency response shall be measured as described in 4.6.1 of 222PT-31A.

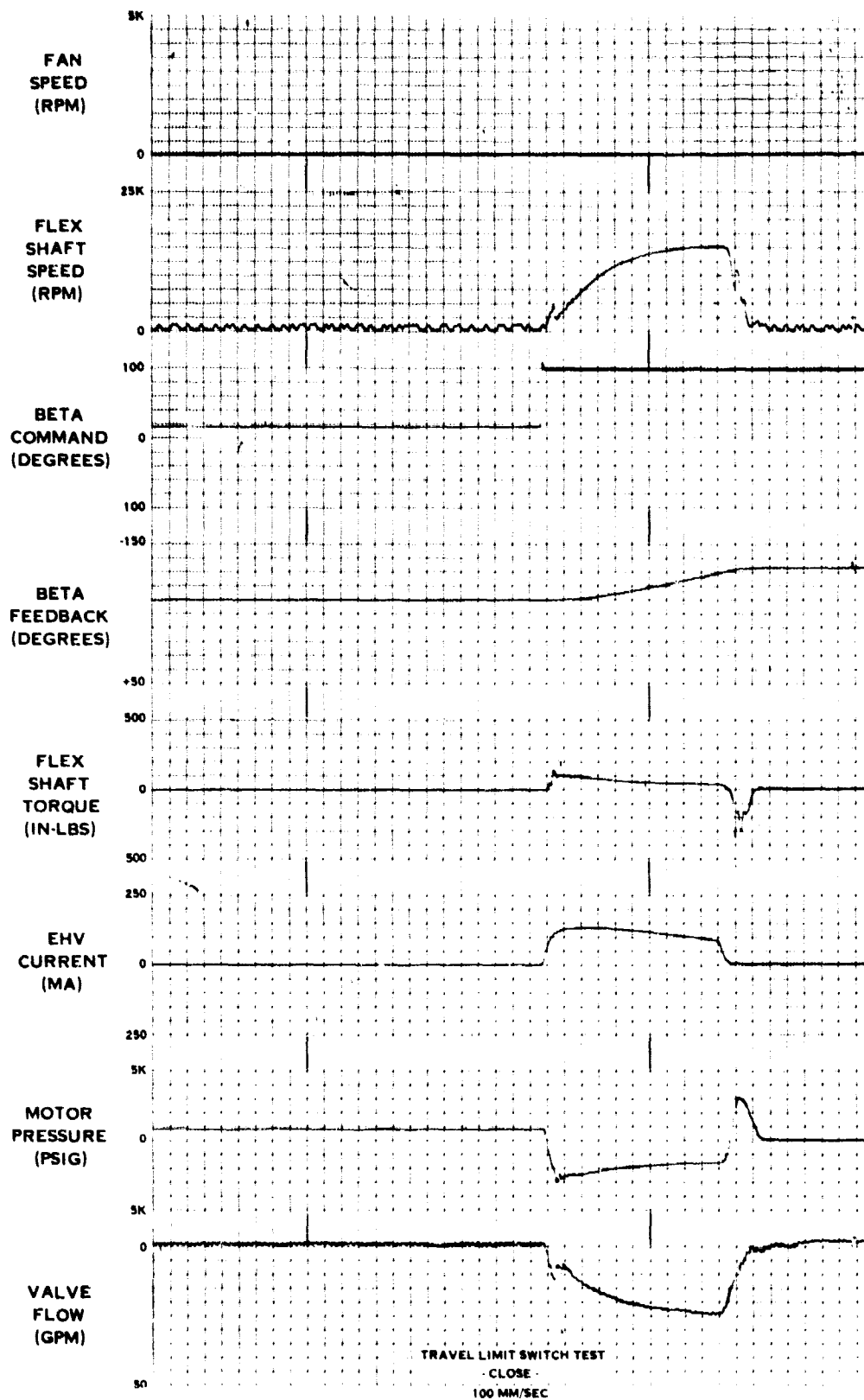
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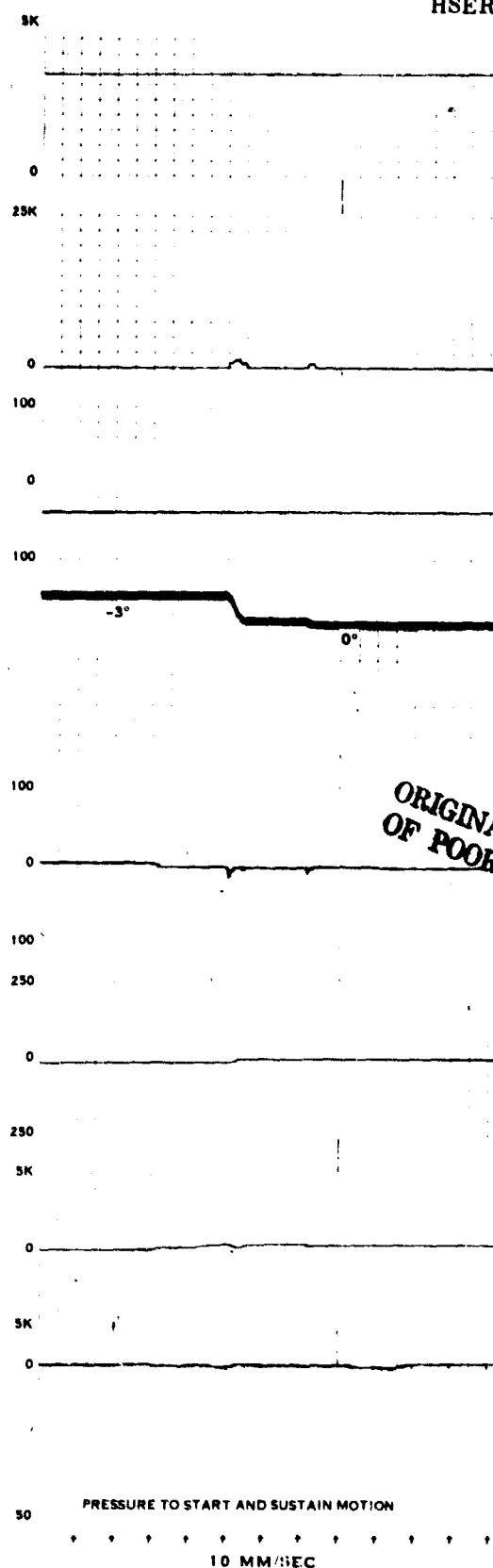
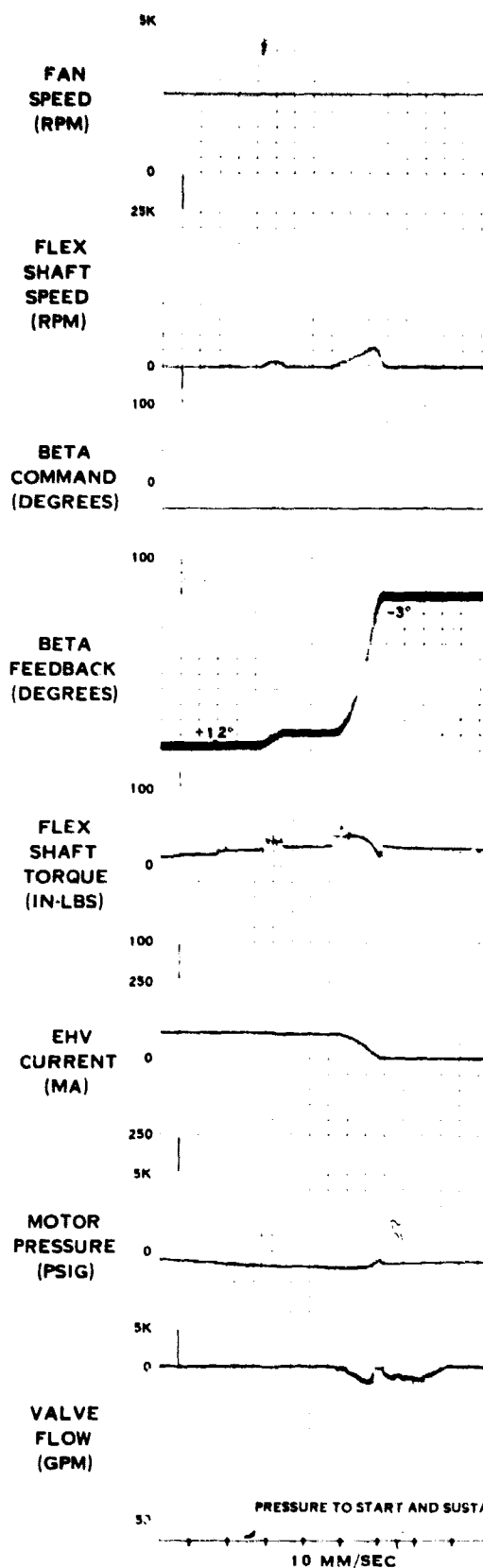
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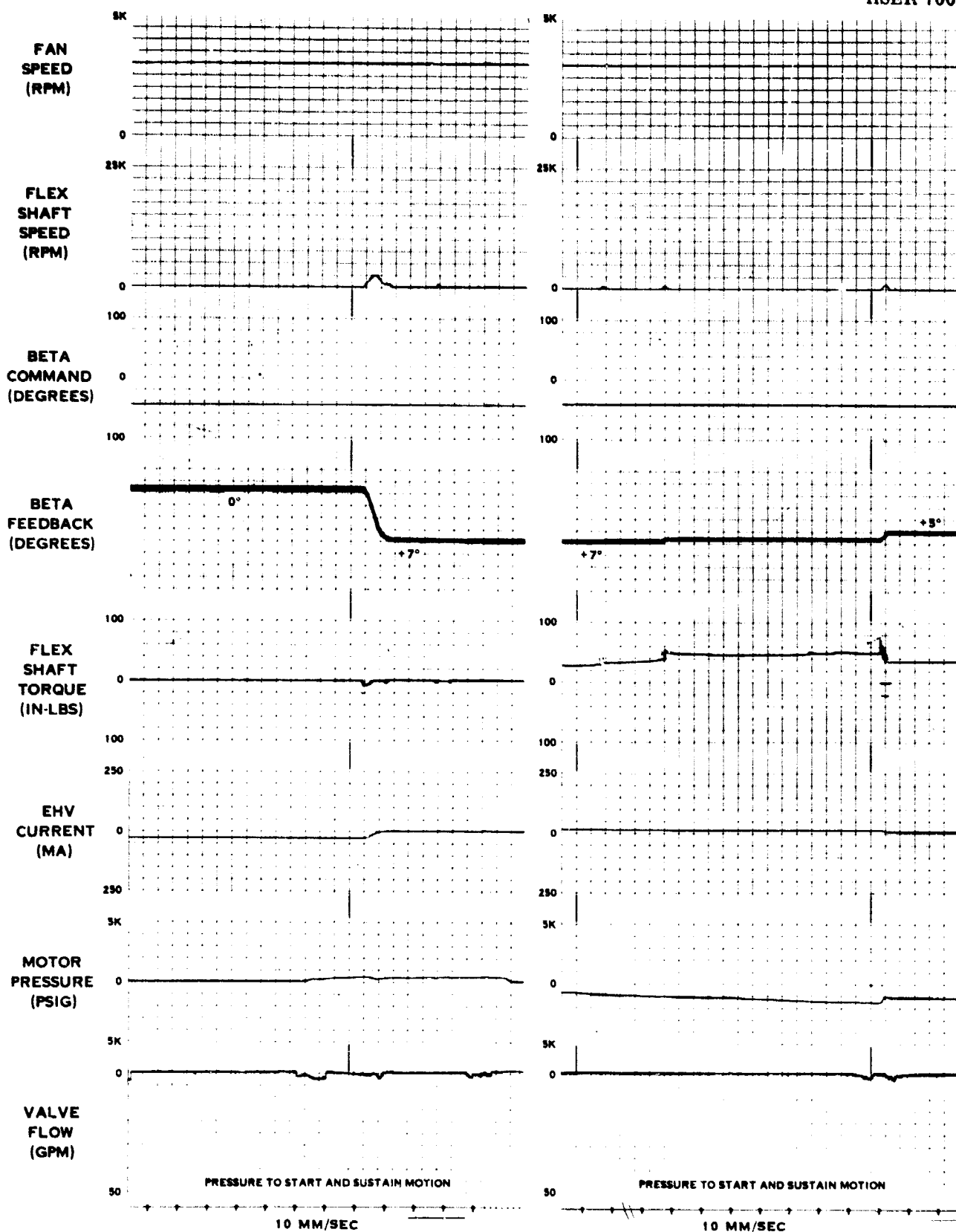
APPENDIX C

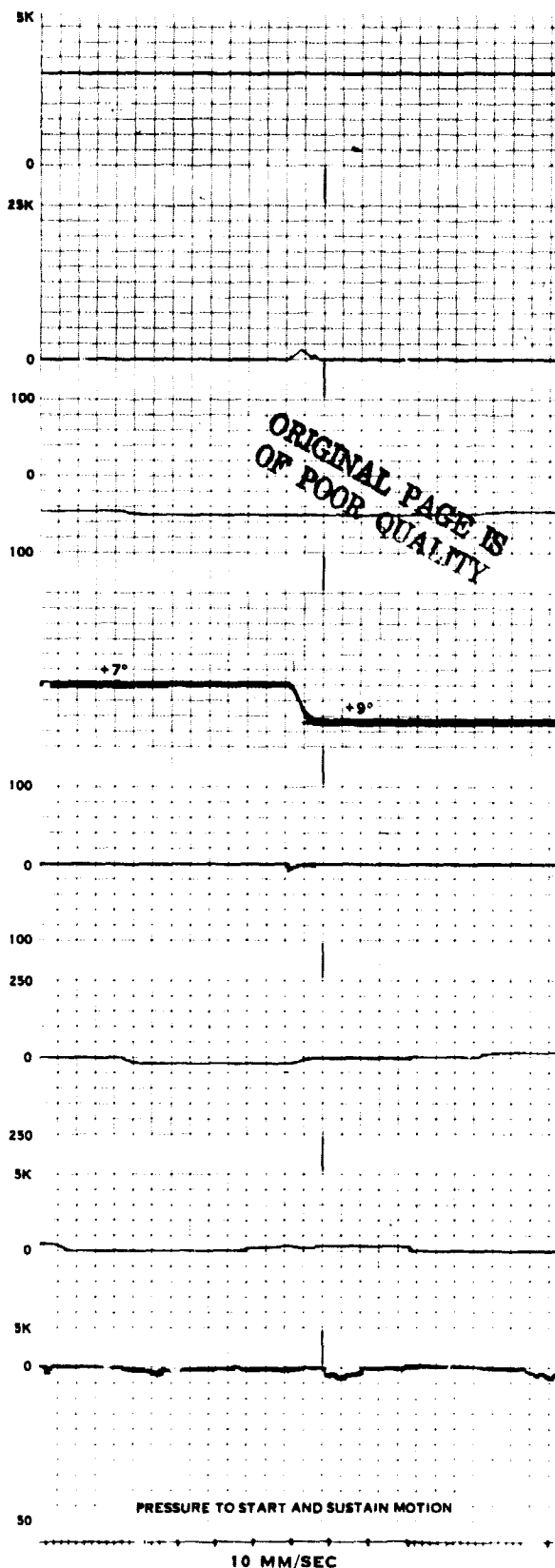
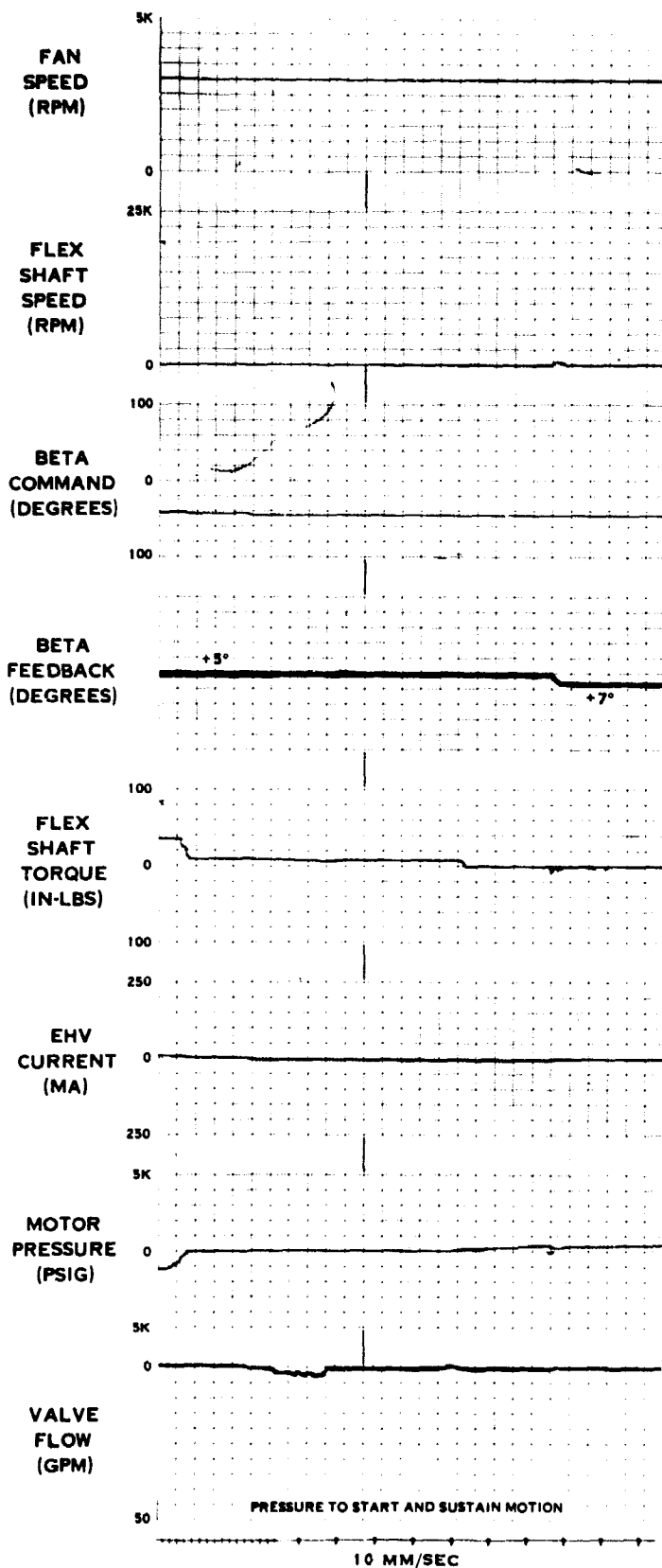
SANBORN RECORDS

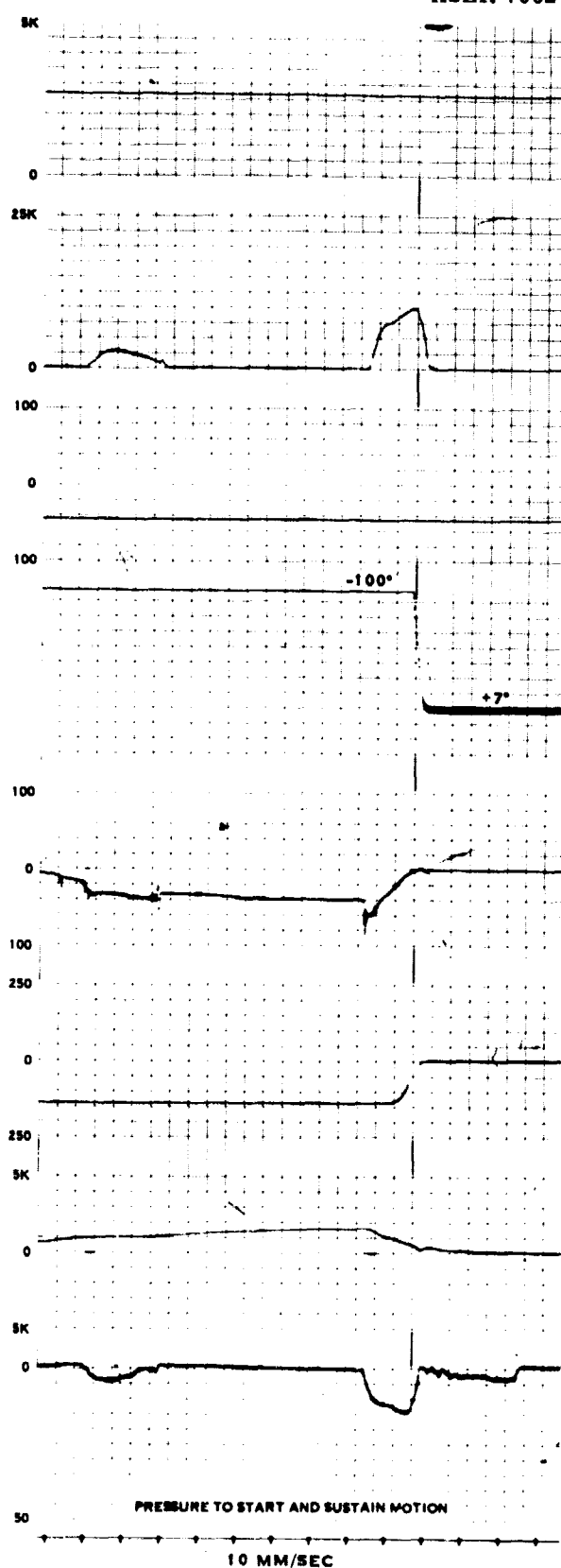
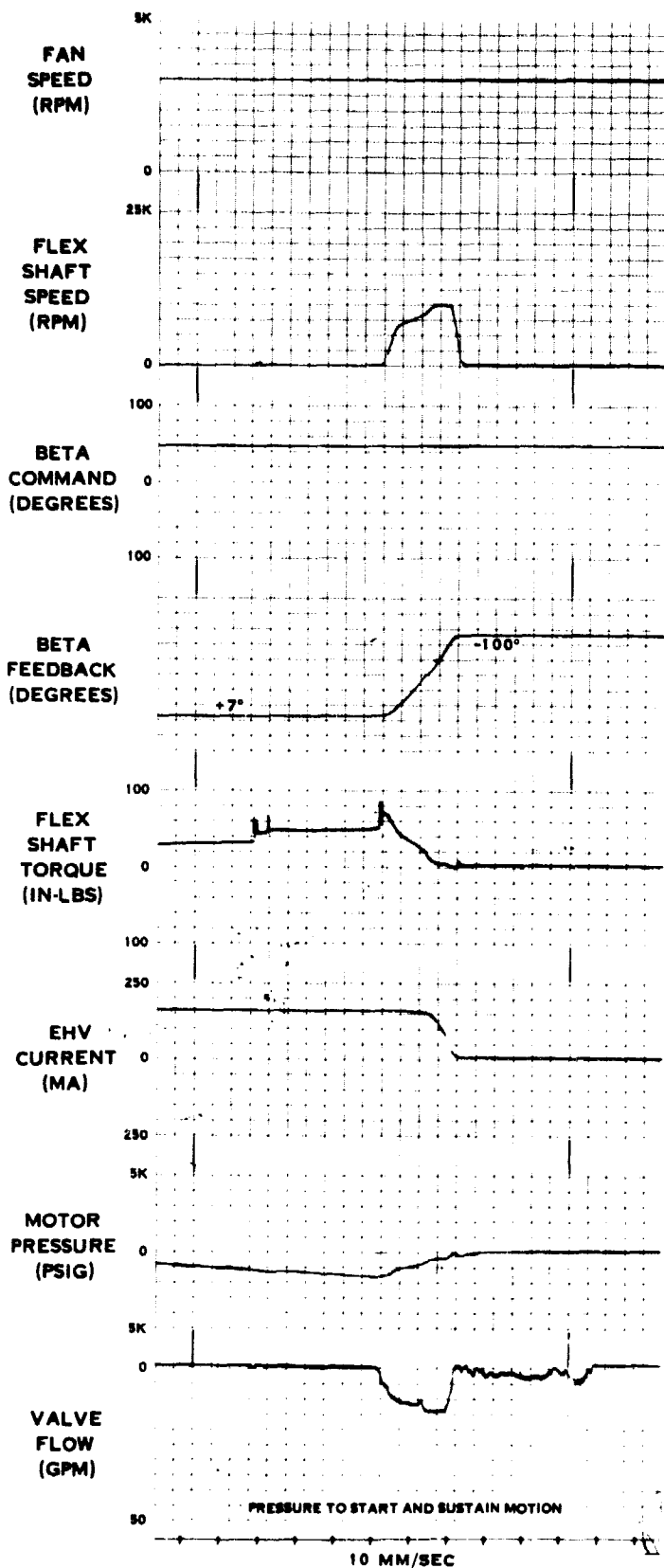


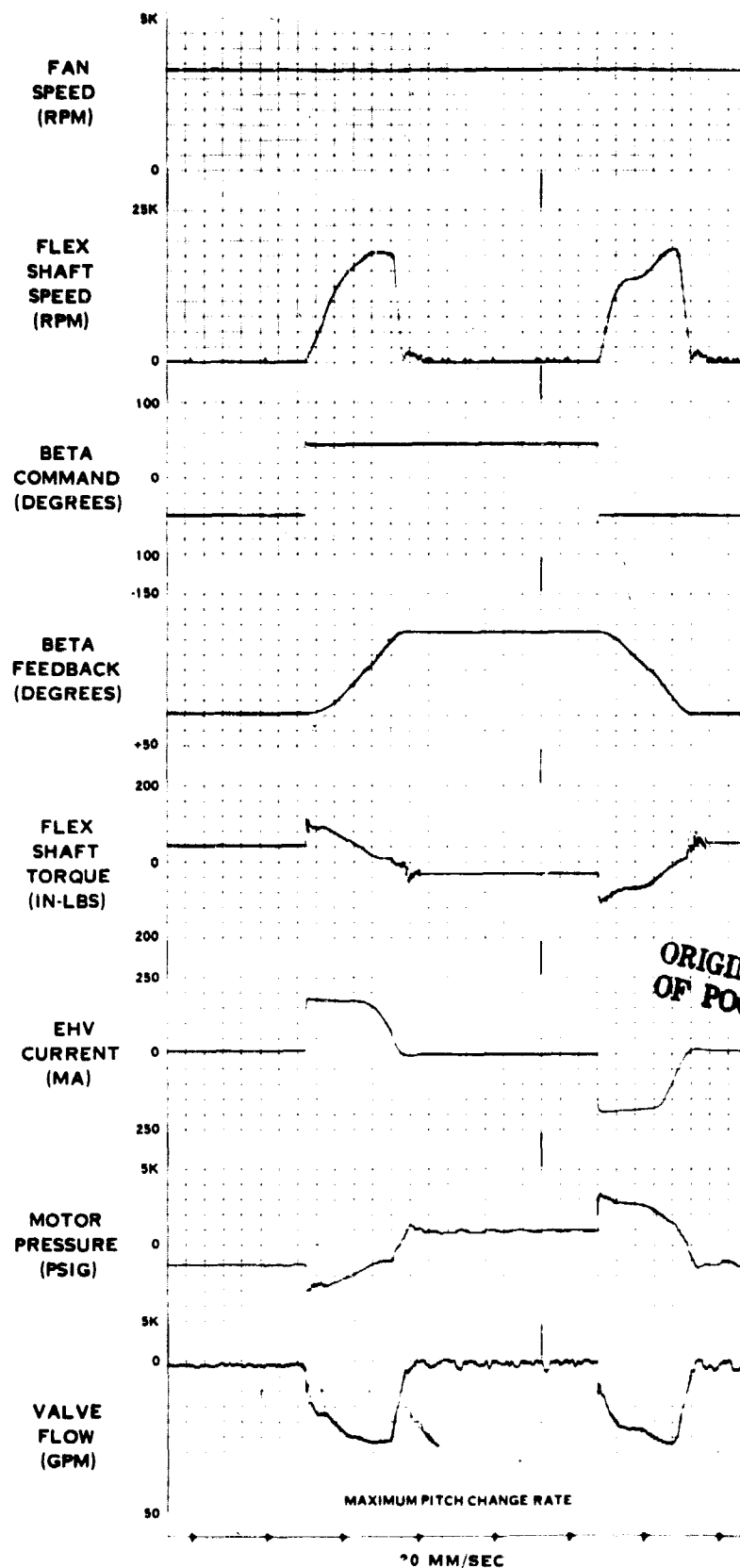












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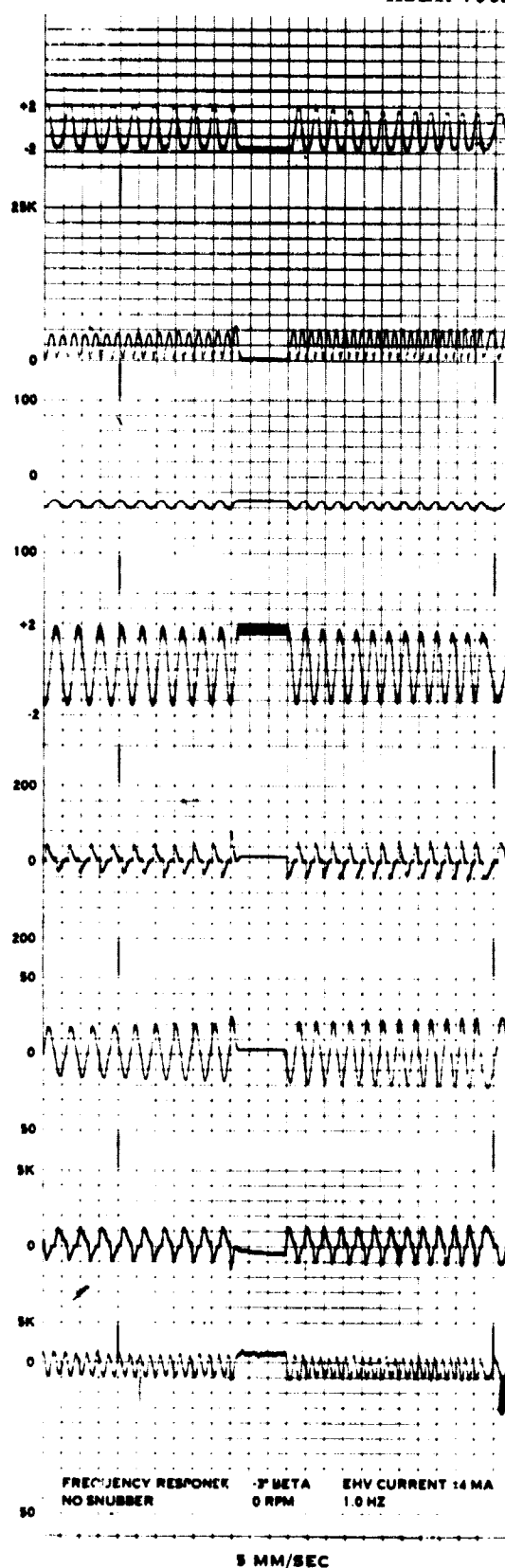
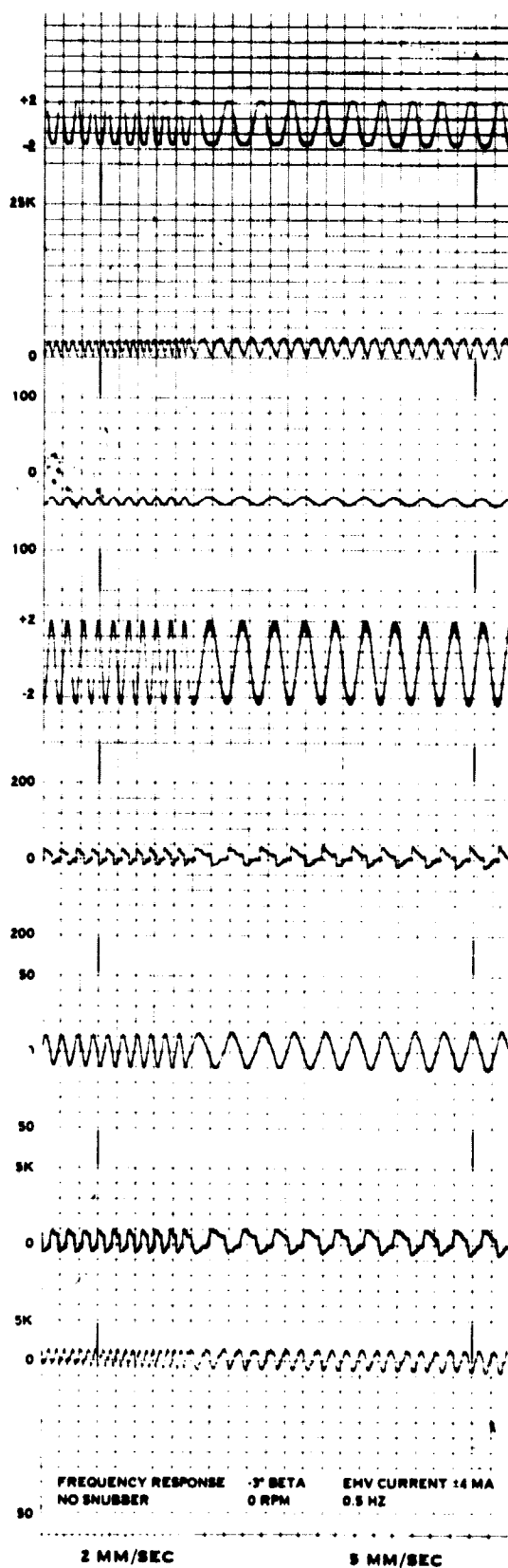
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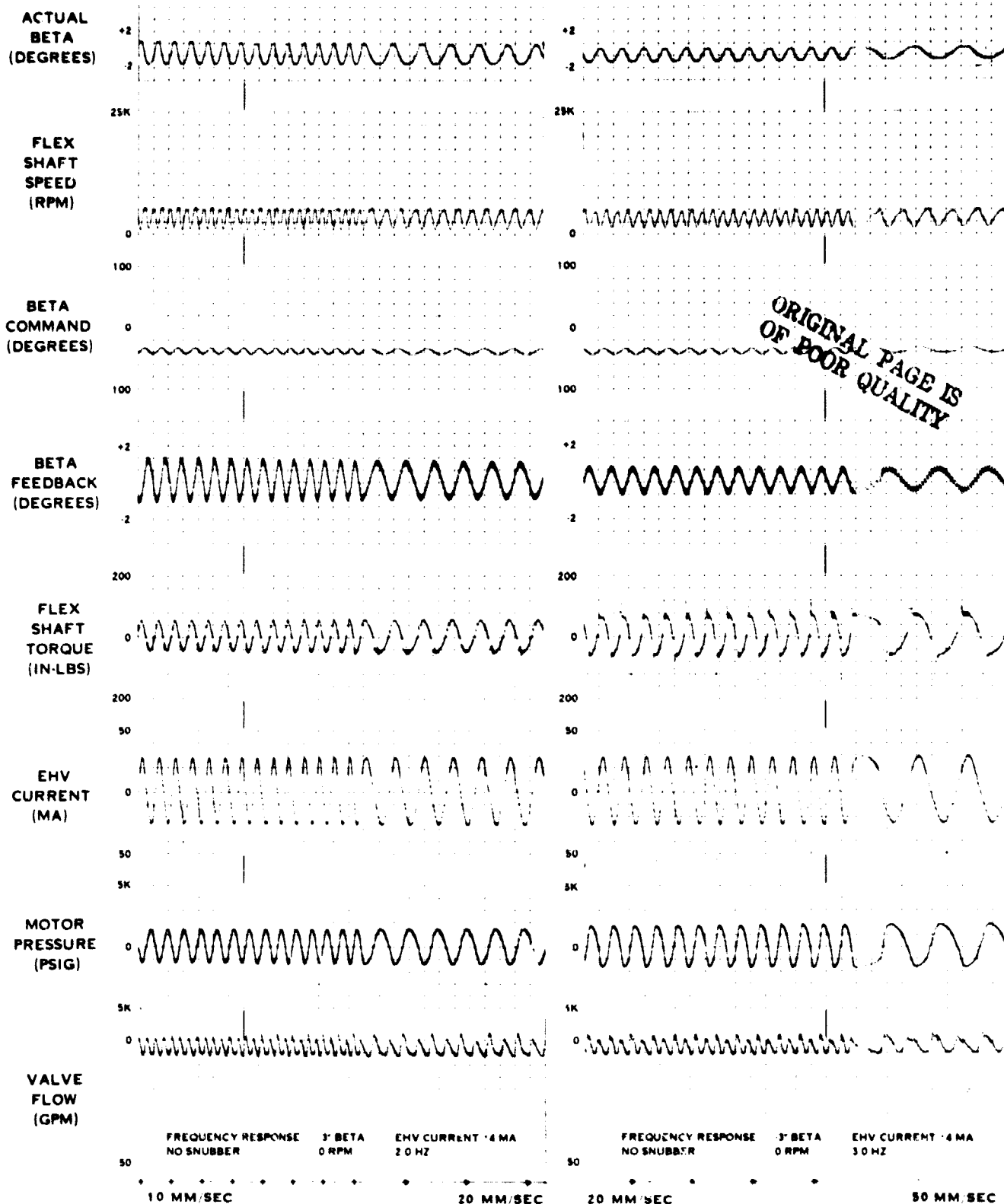
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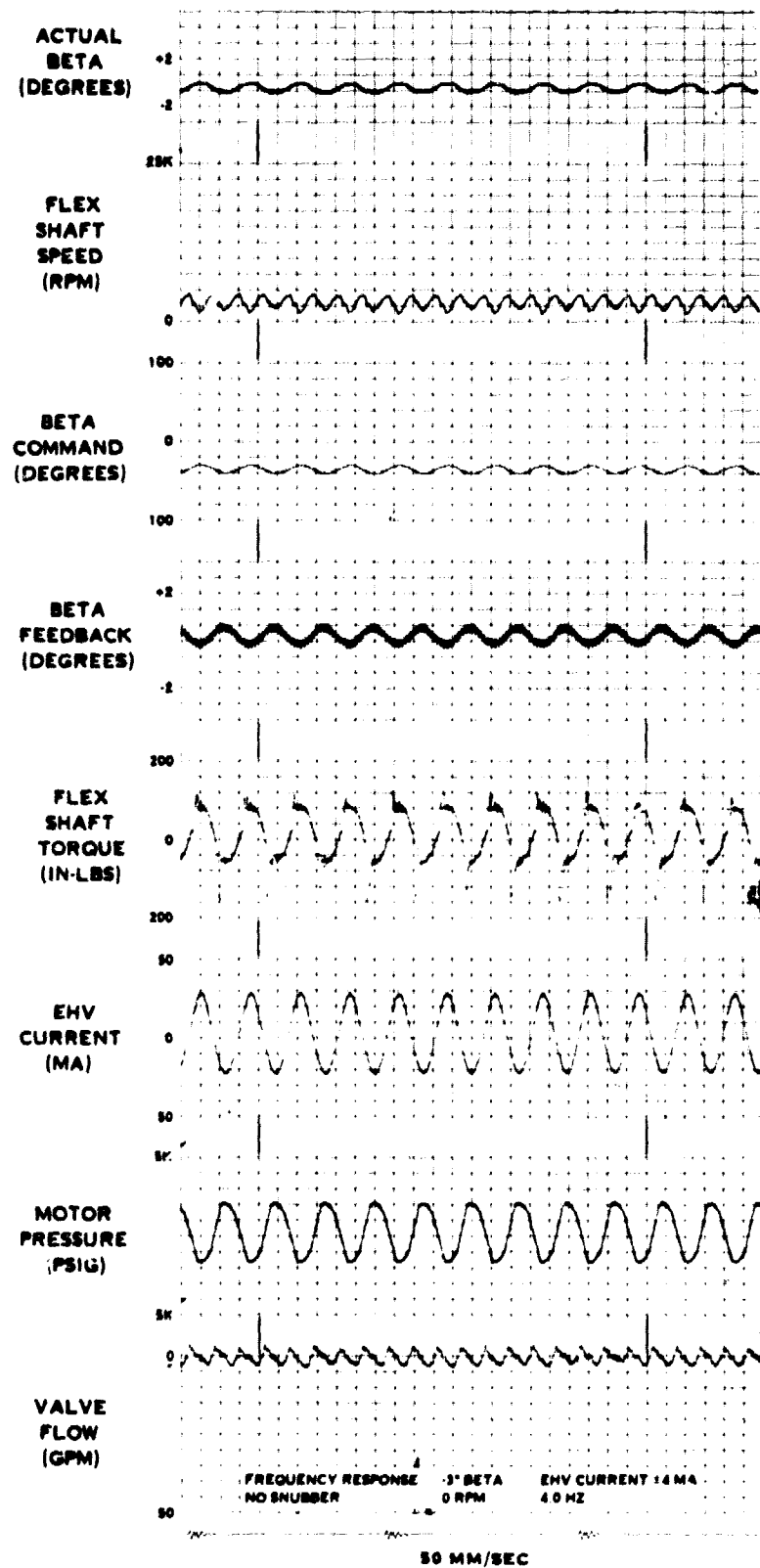
EHV
CURRENT
(MA)

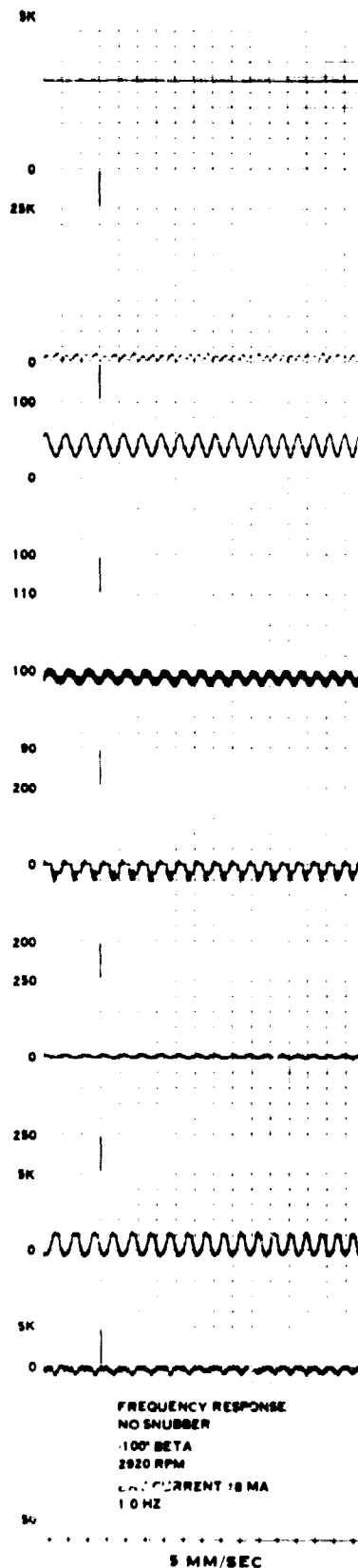
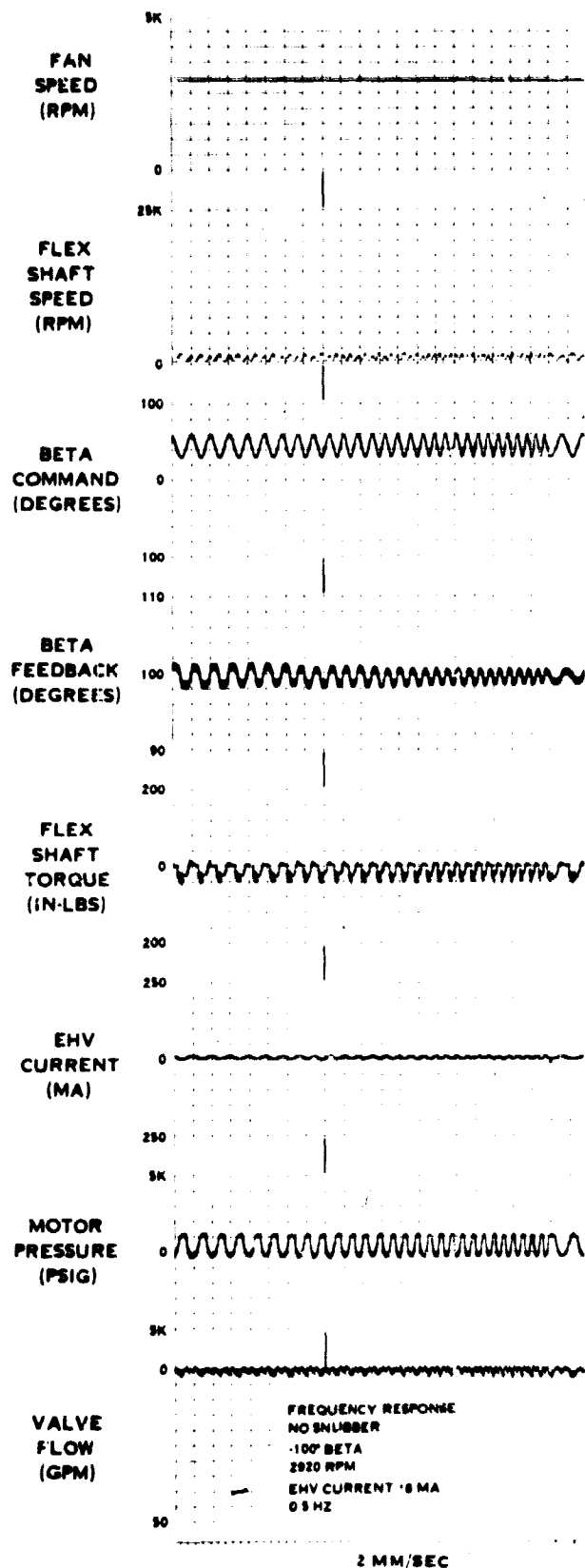
MOTOR
PRESSURE
(PSIG)

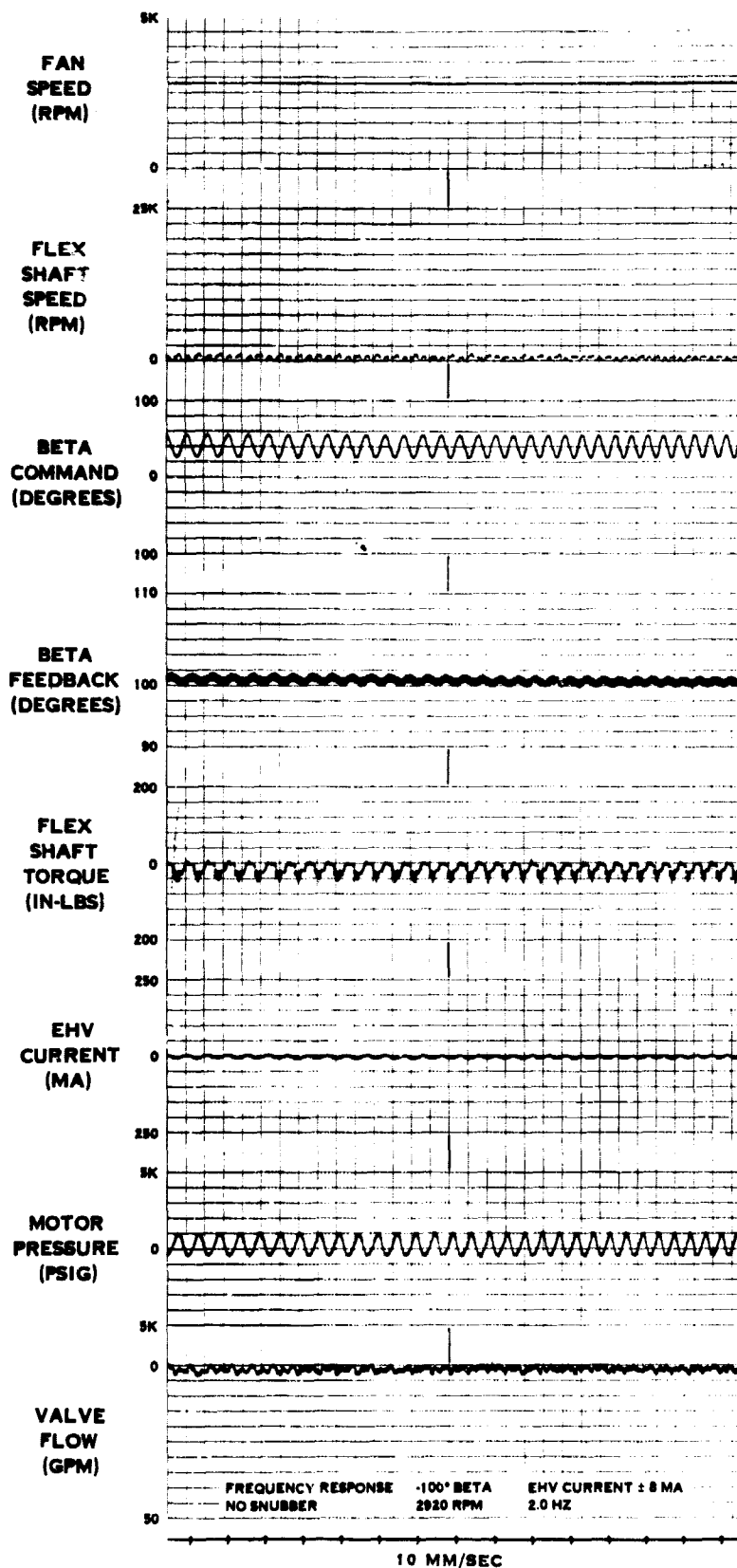
VALVE
FLOW
(GPM)

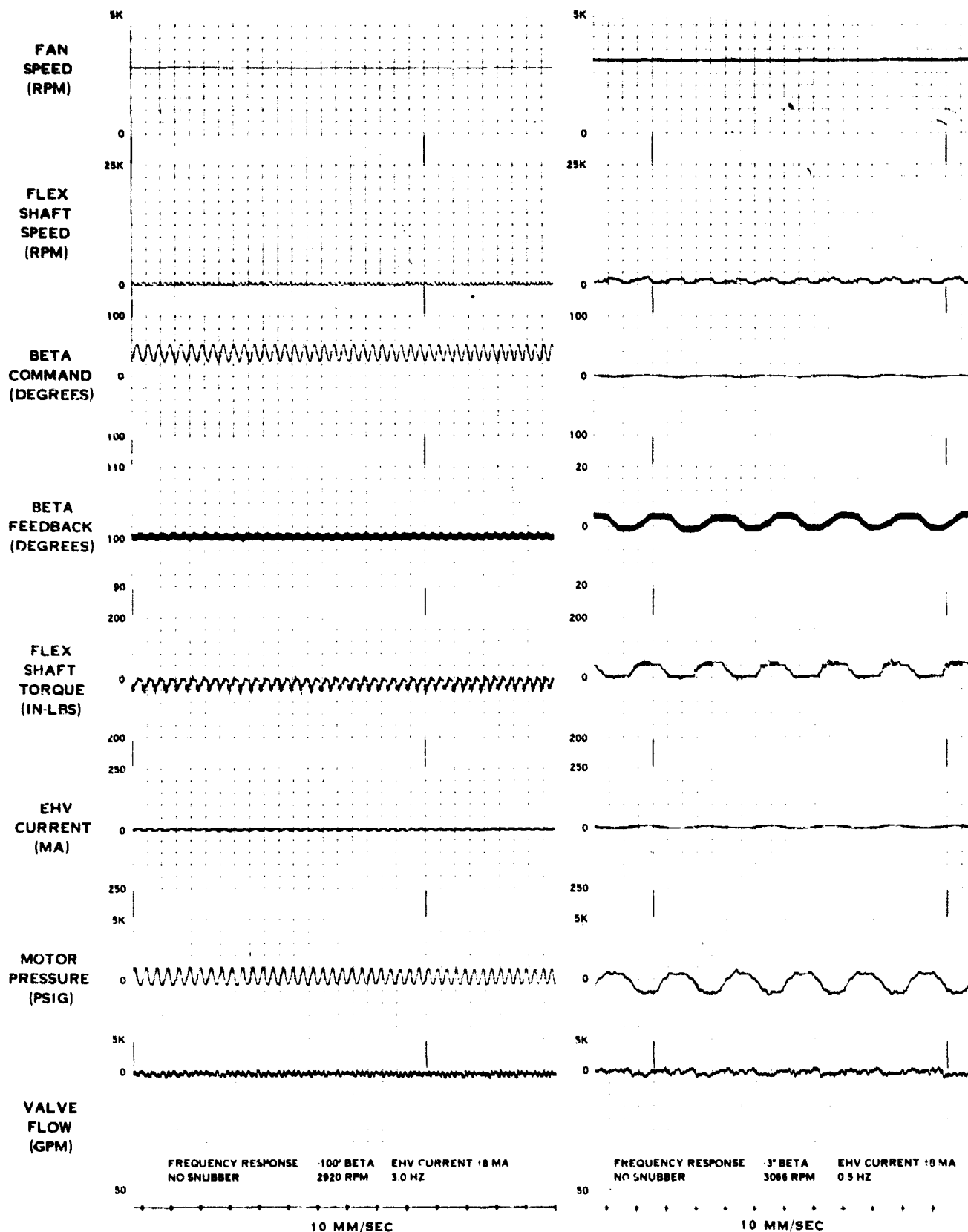


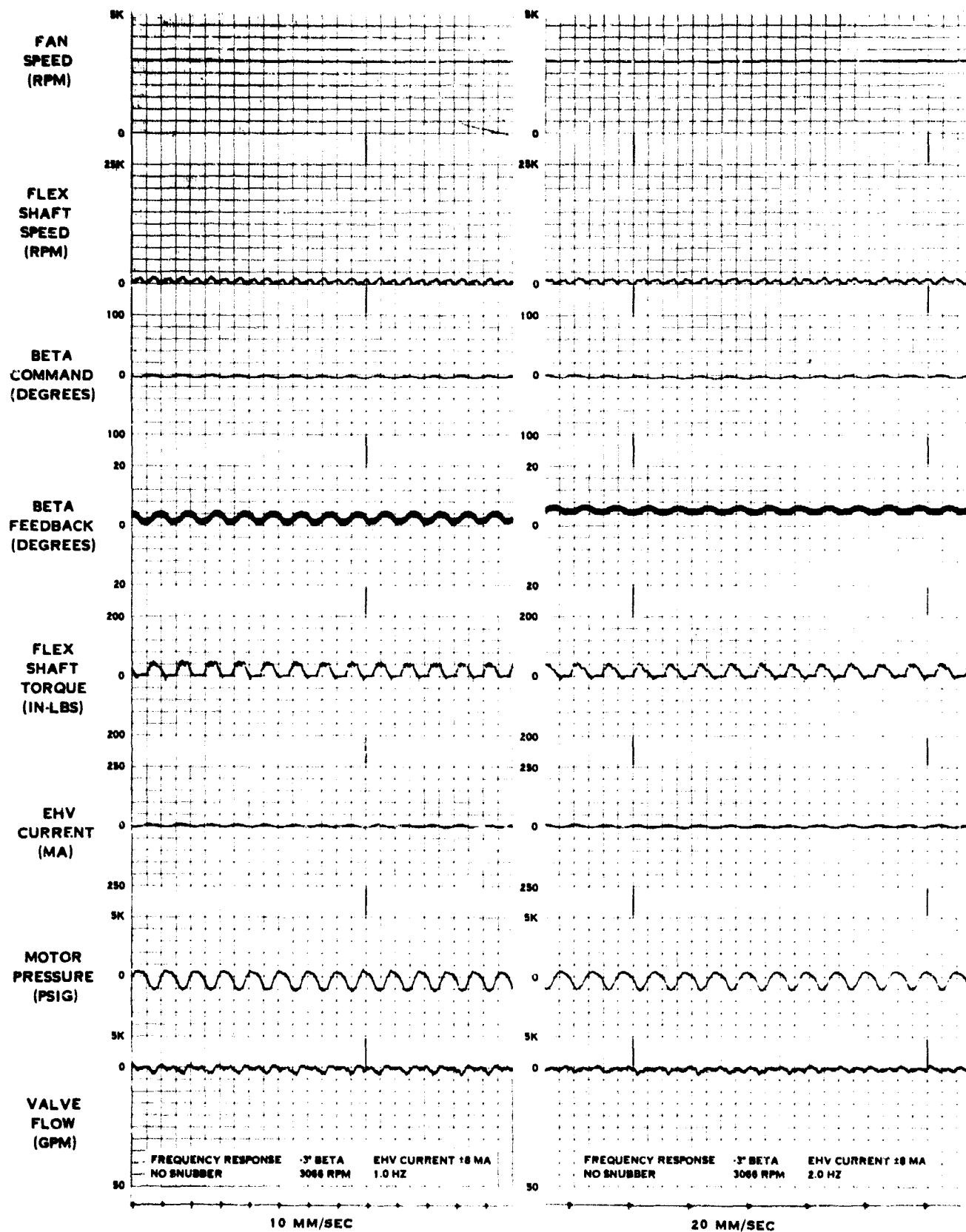


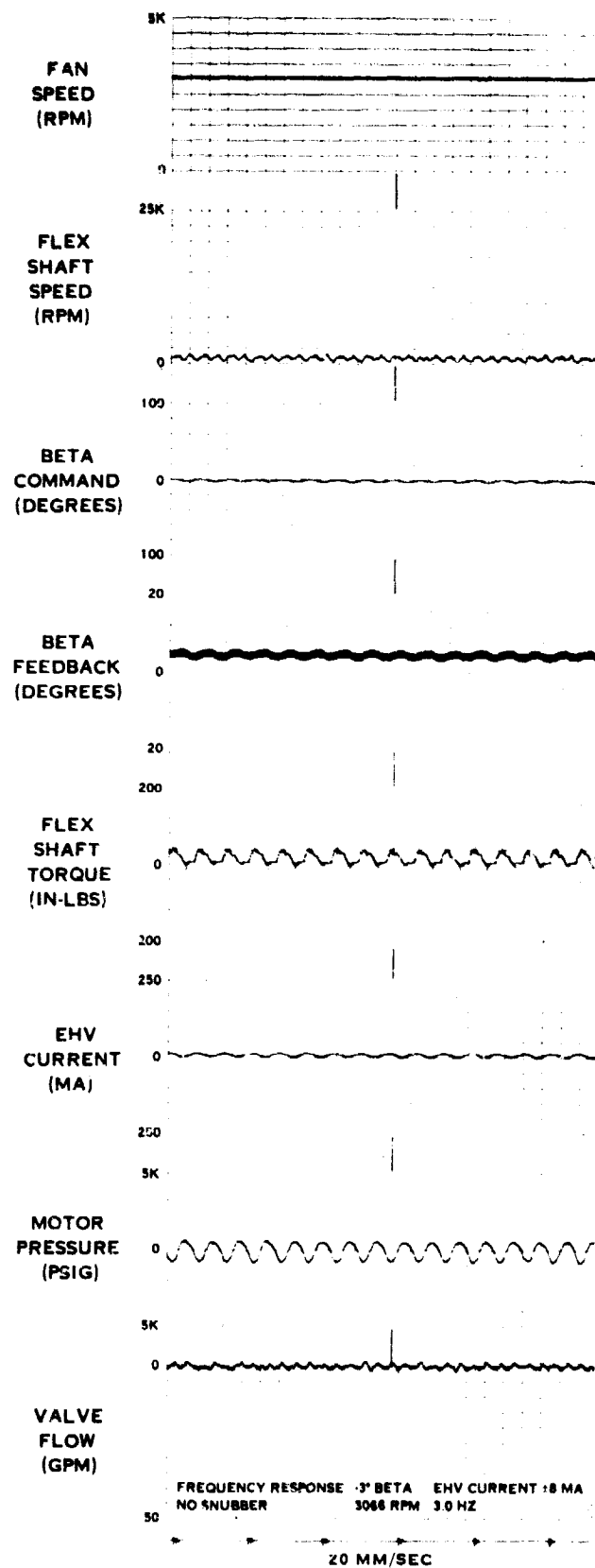


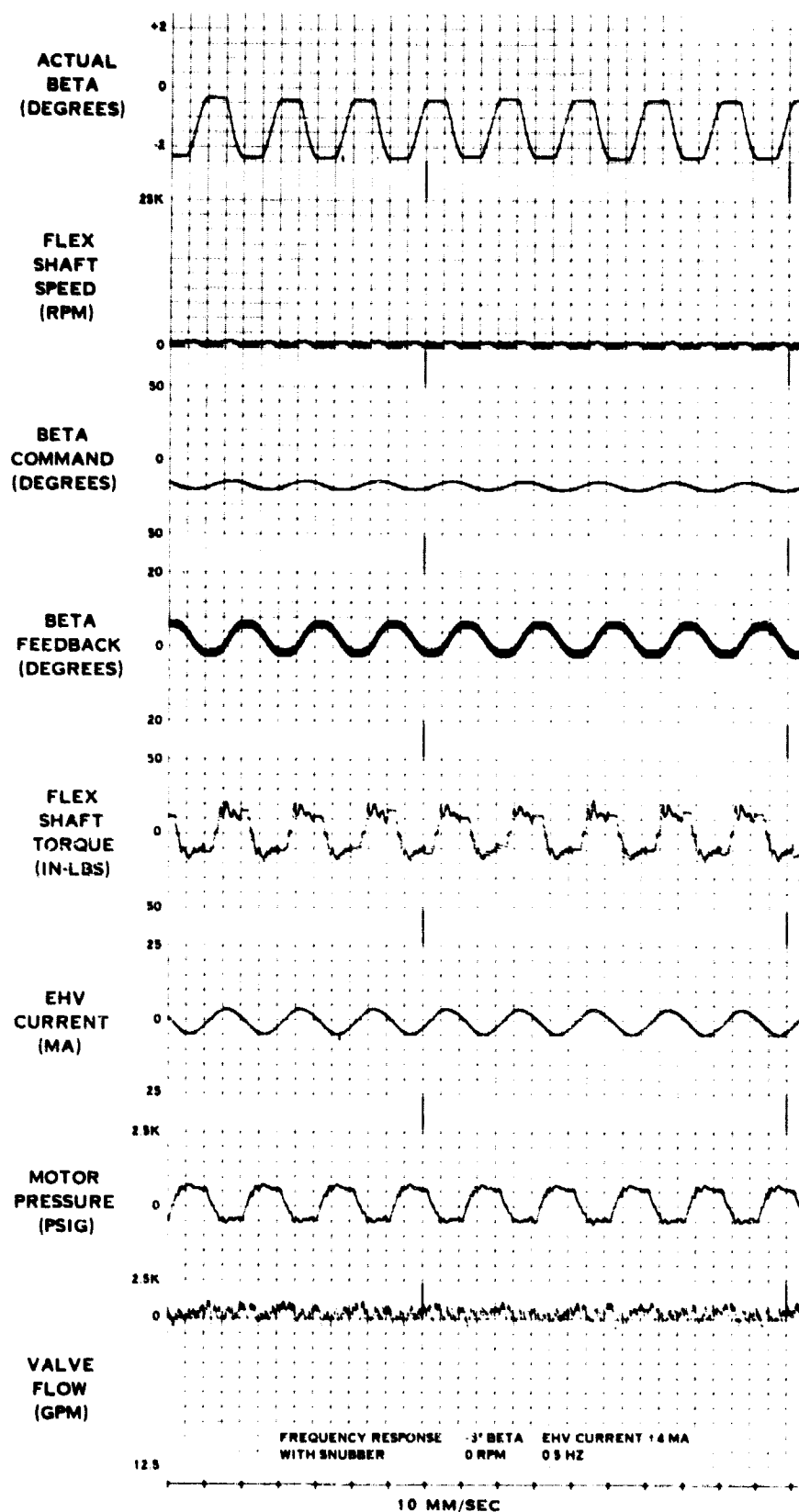


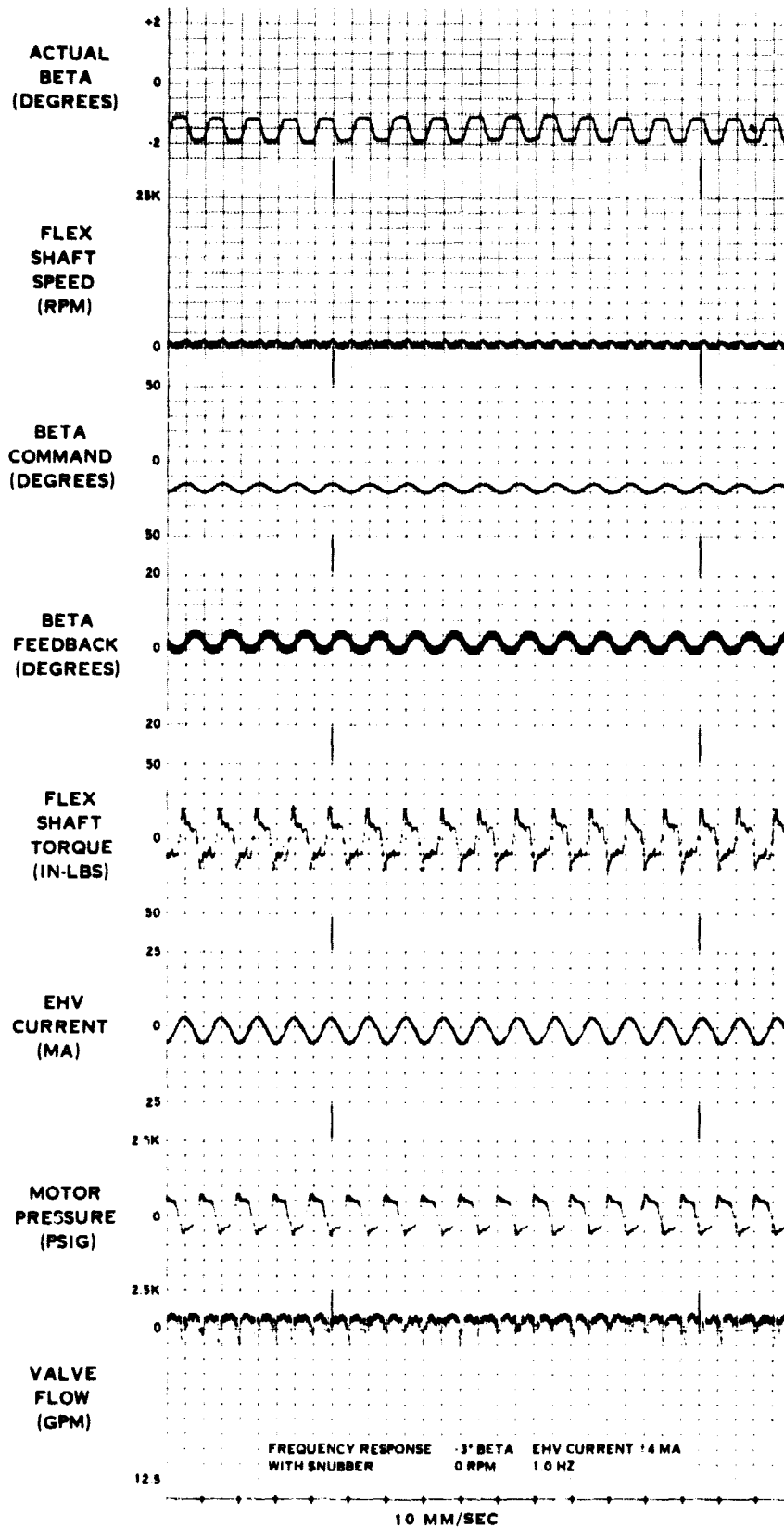


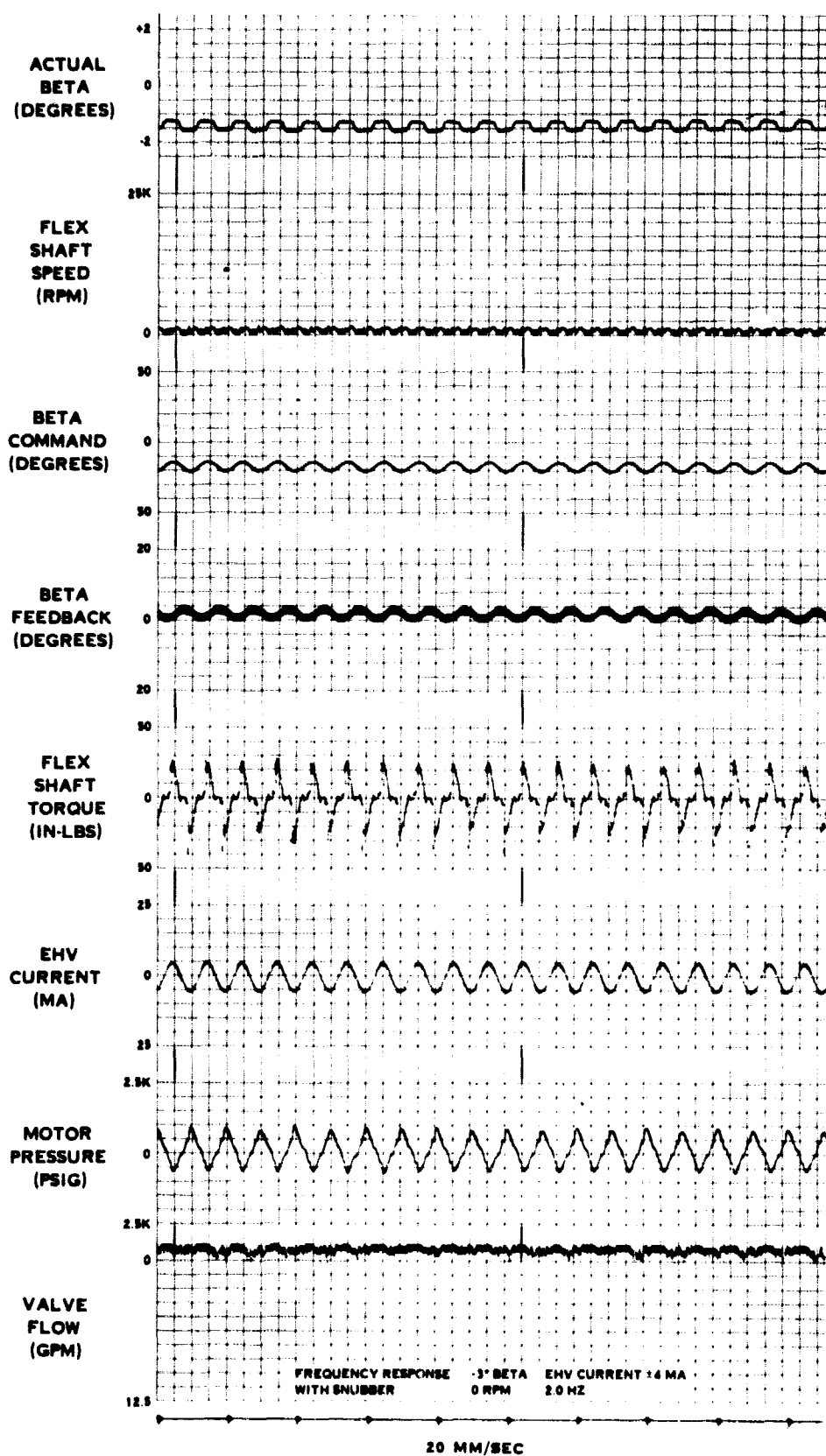


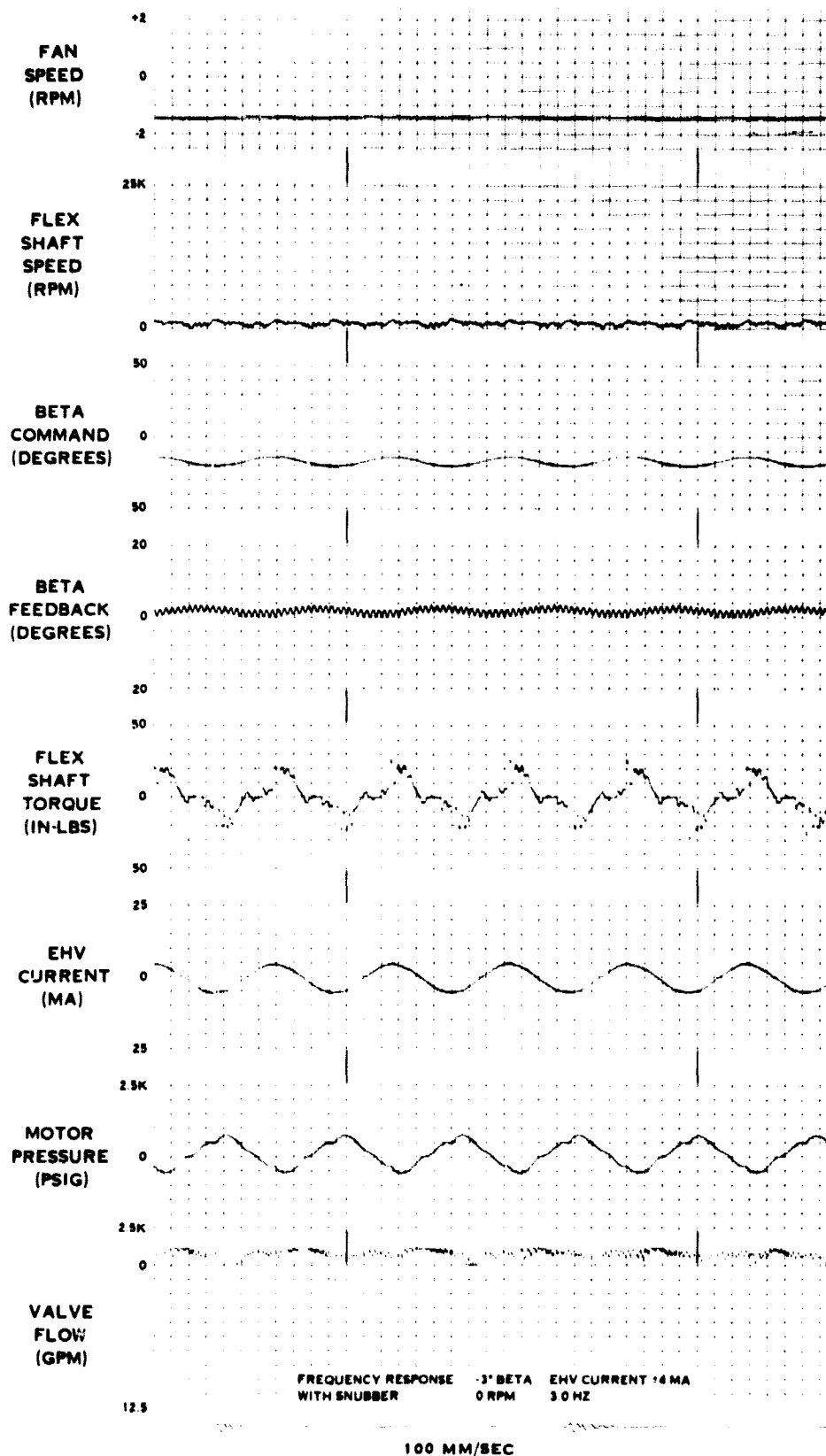


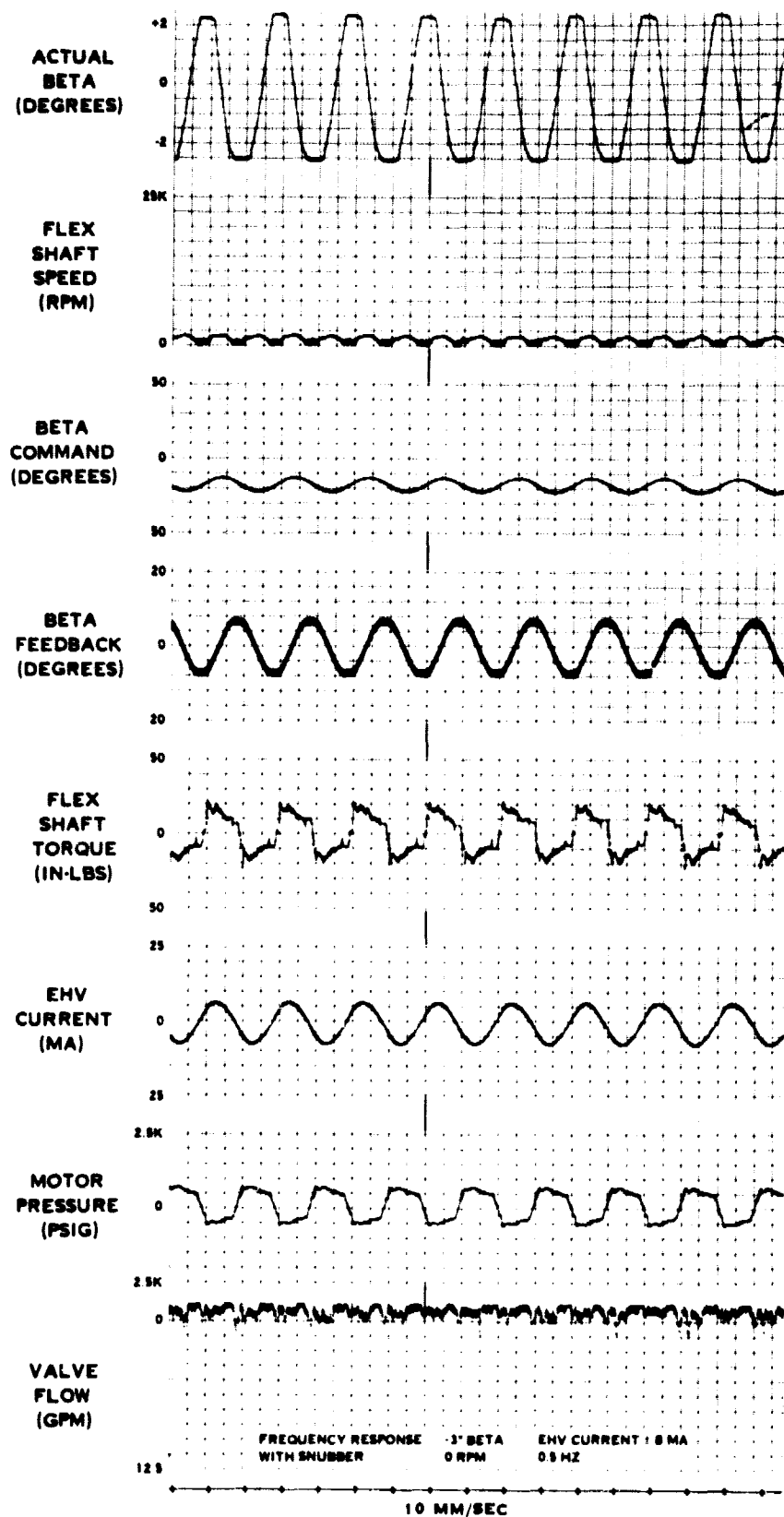


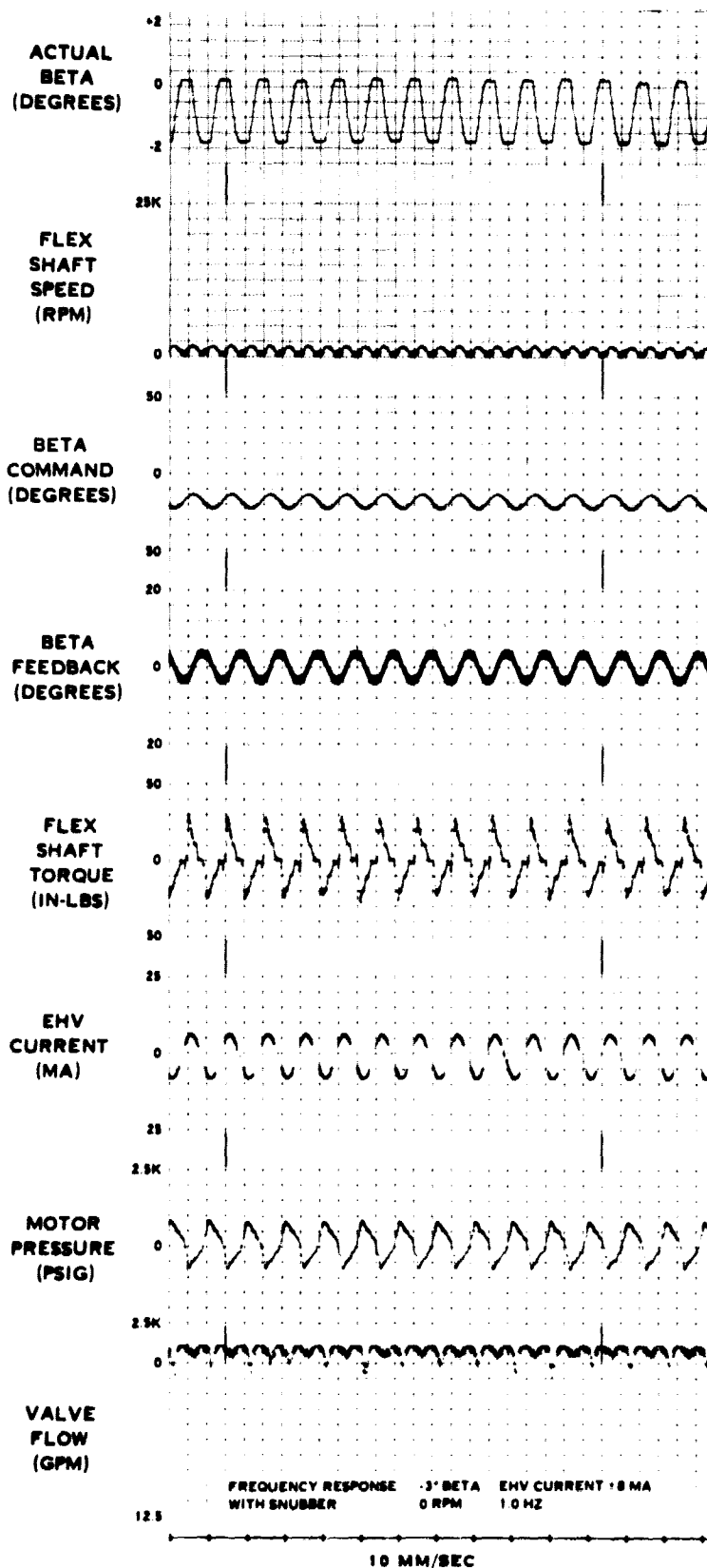


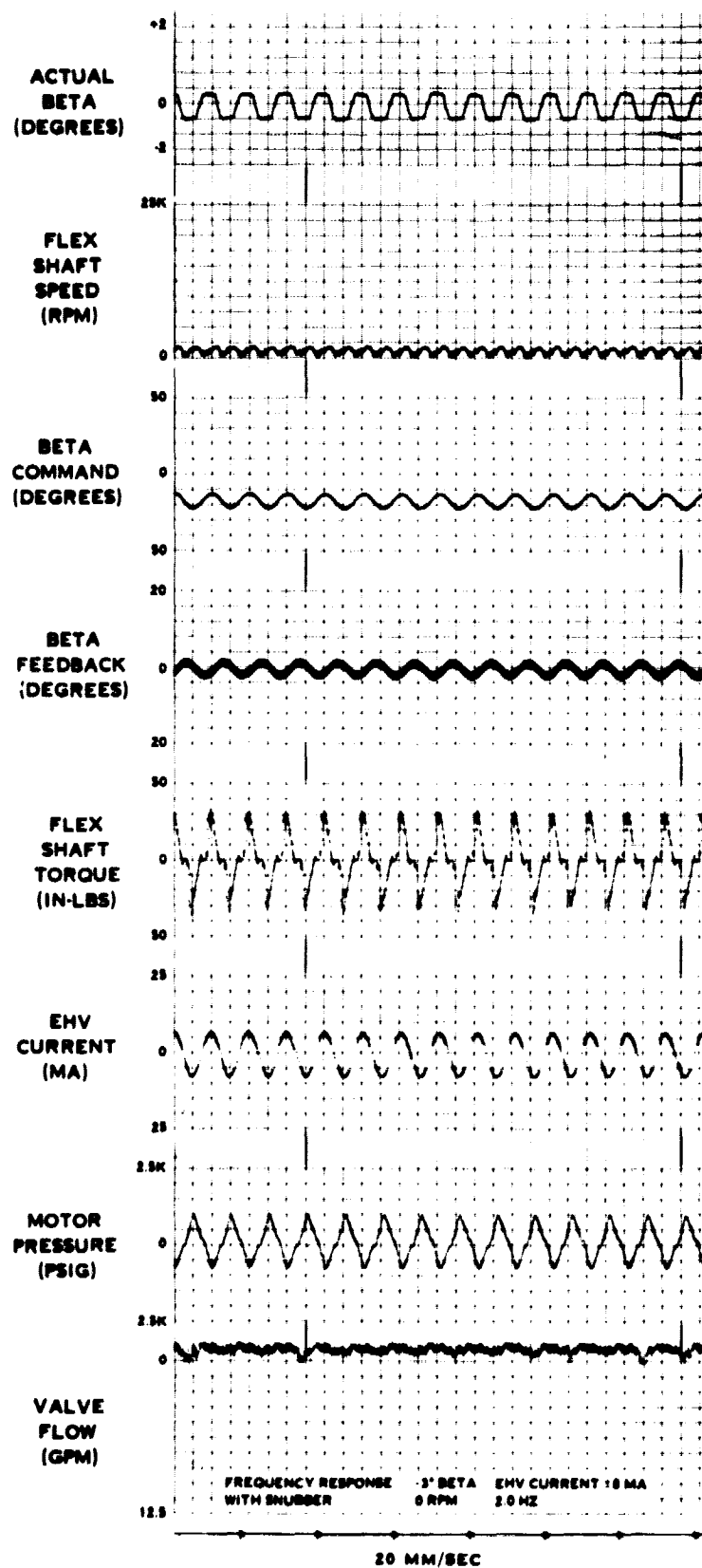


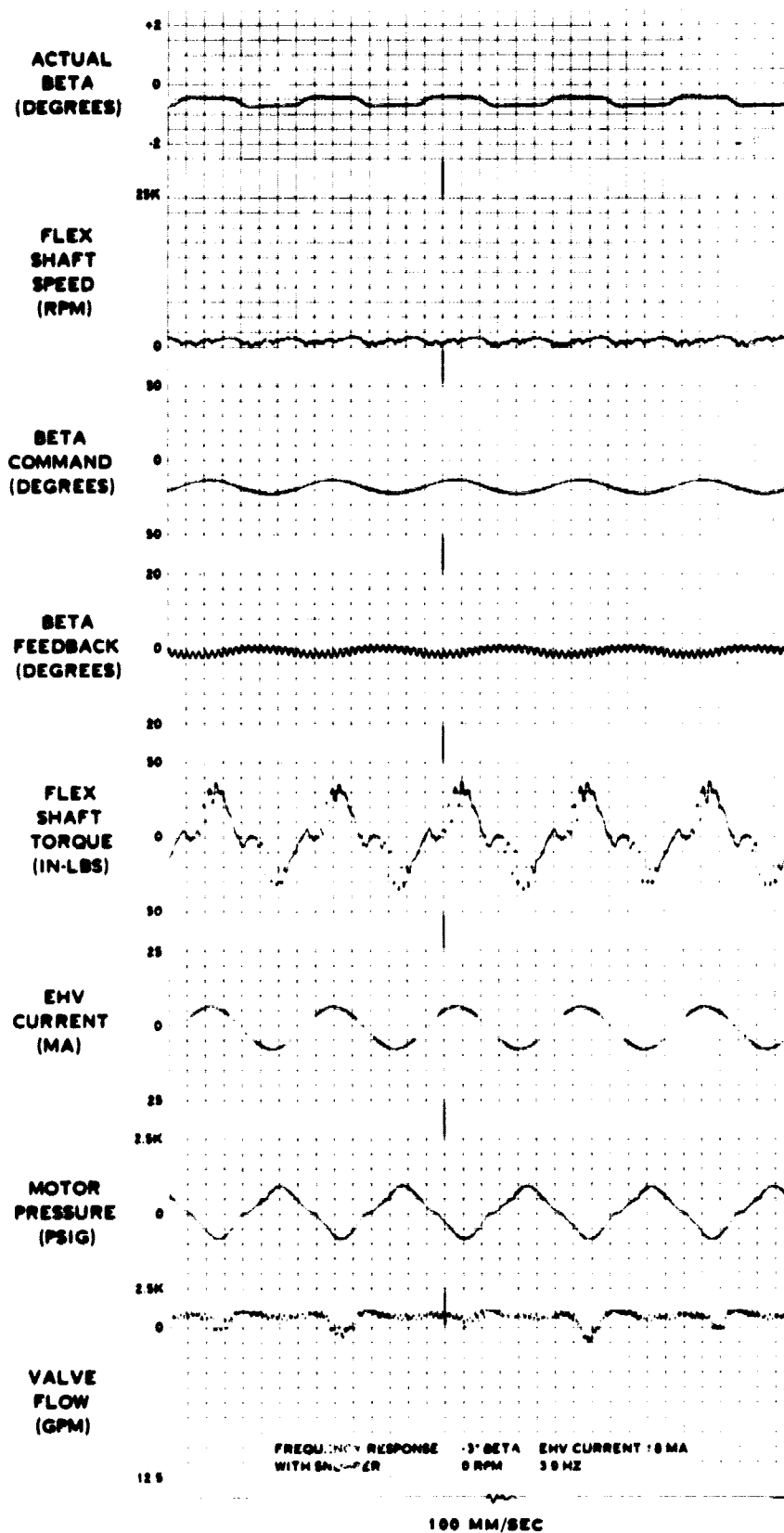


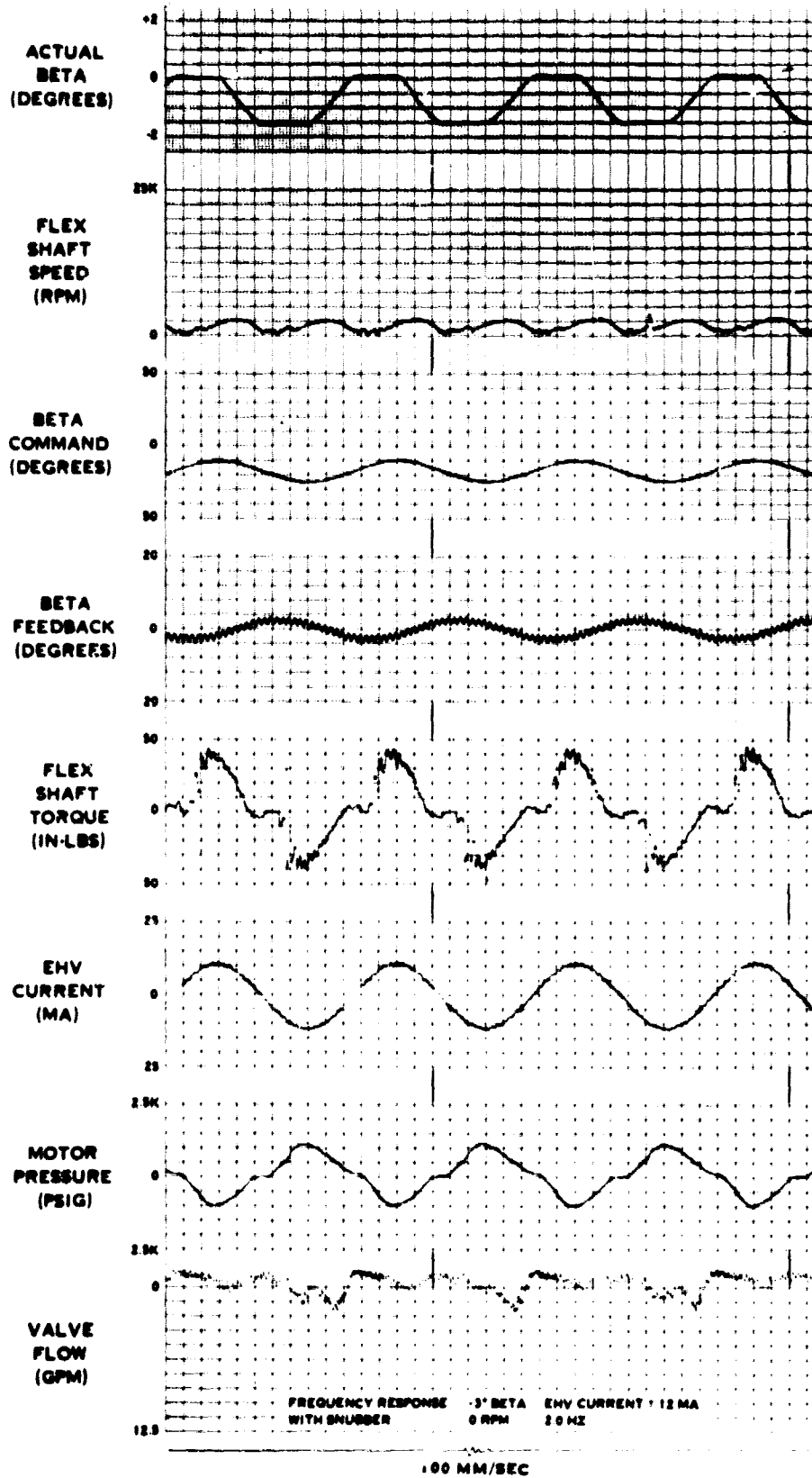


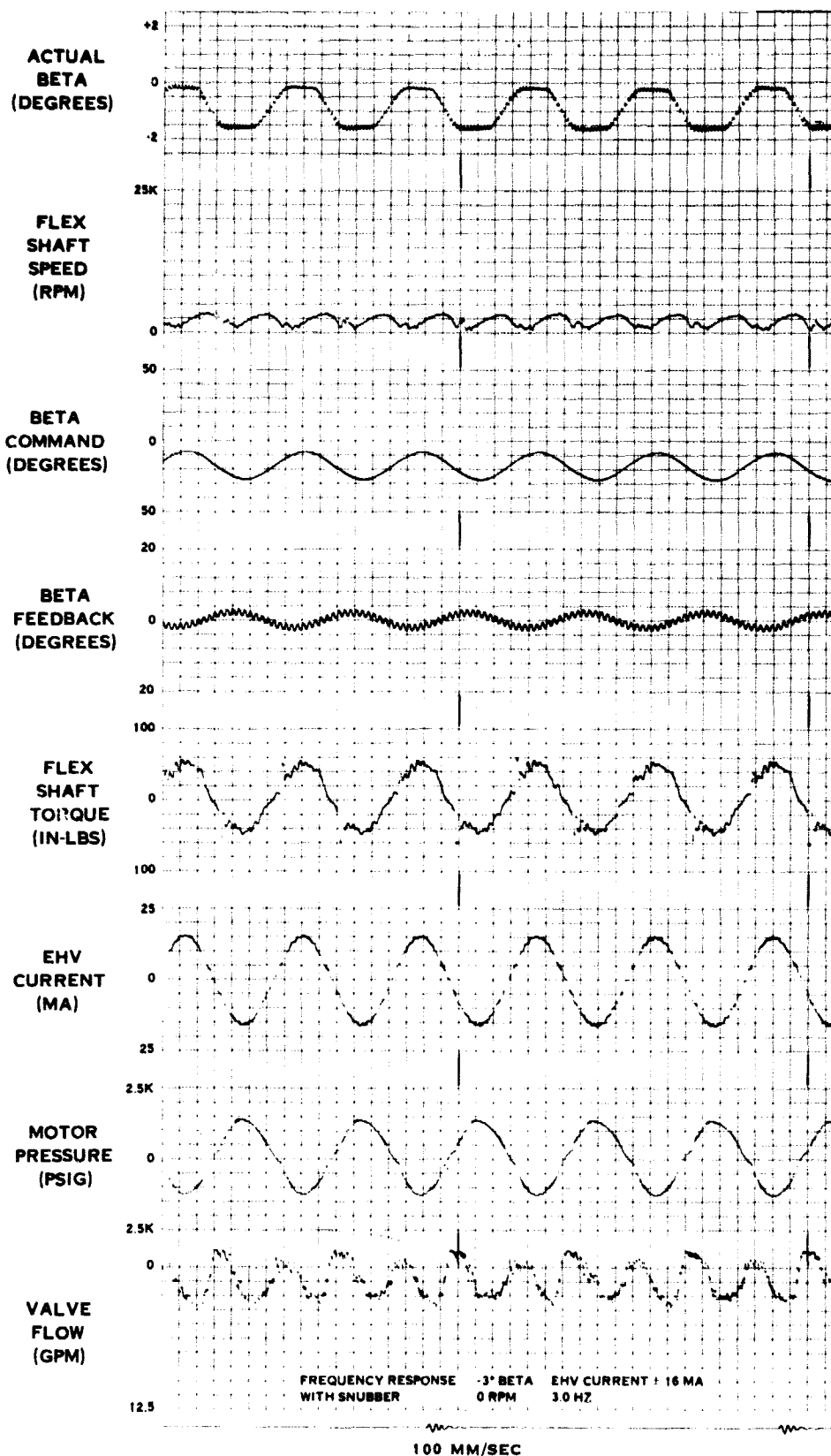


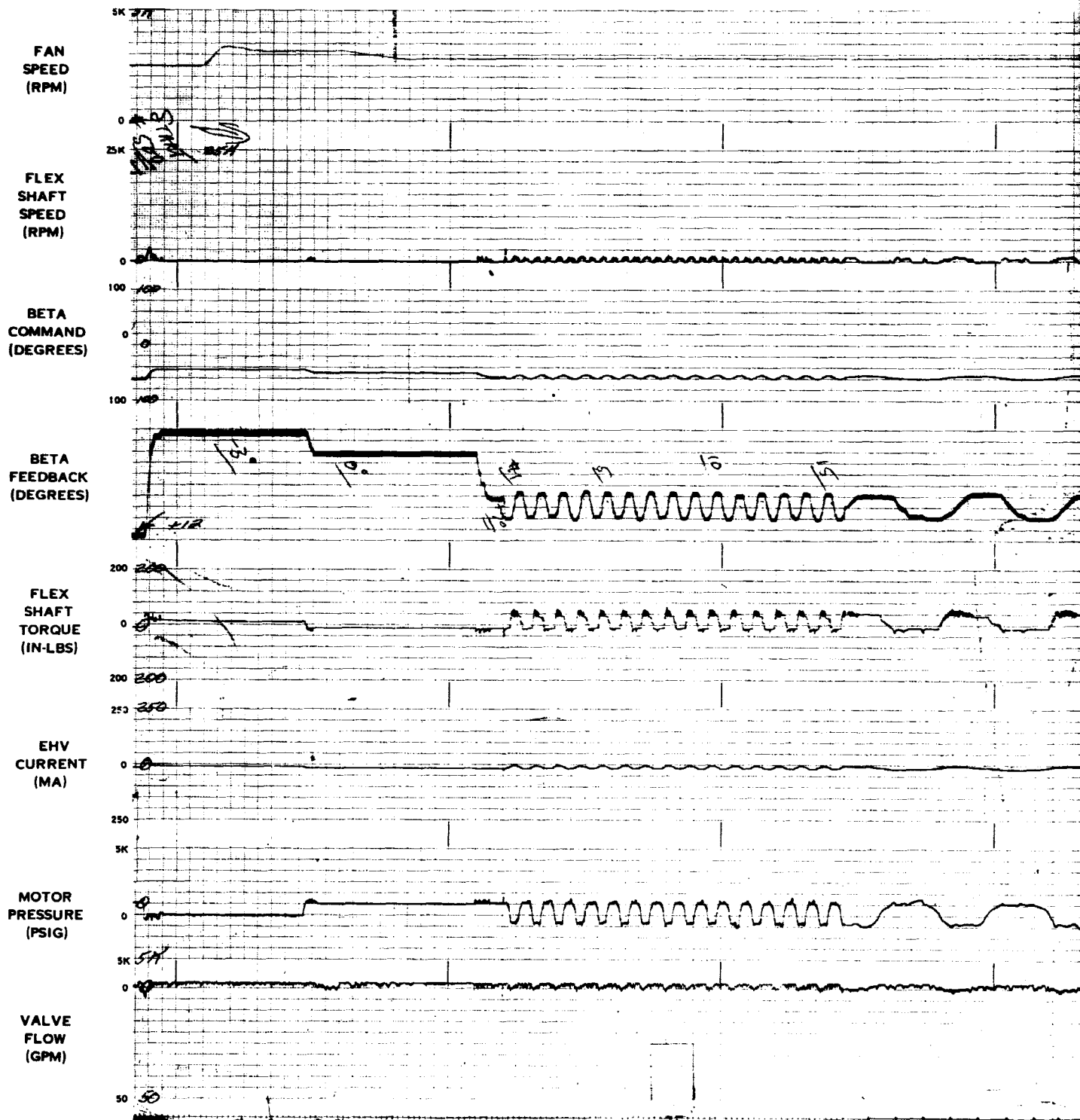








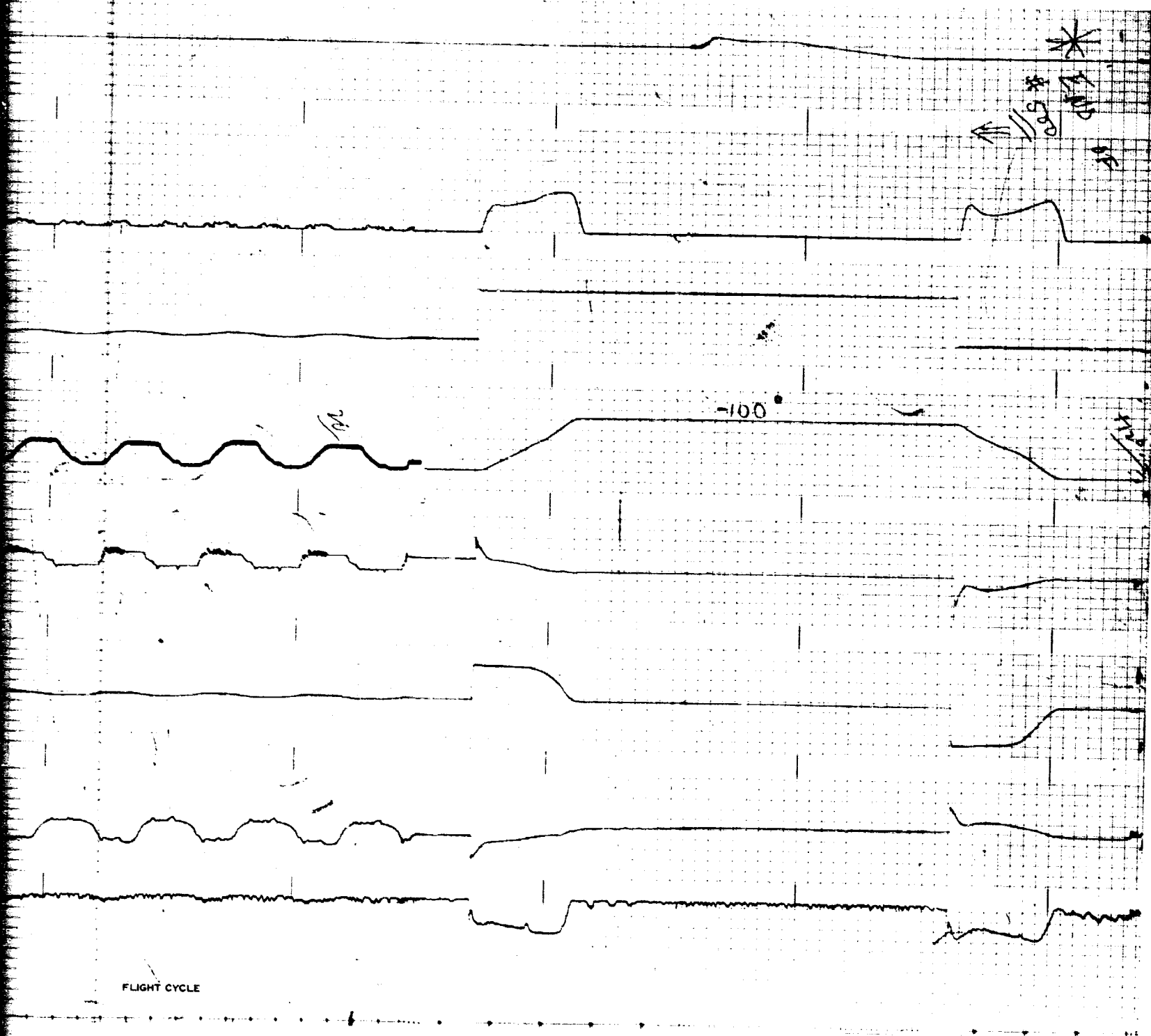




ORIGINAL PAGE 15
OF POOR QUALITY

2 MM/SEC

/ FOLDOUT FRAME



FLIGHT CYCLE

20 MM/SEC

2 MM/SEC

20 MM/SEC

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OF POOR QUALITY

119

2 FOLDOUT FRAME

PAGE 118 INTENTIONALLY BLANK

APPENDIX D

LOG SHEETS

Hamilton Standard
FOR LOCKS, CONNECTICUT • U.S.A.

4107

ON 53

TYPE OF TEST

Q. 2

PLAN OF TEST NO. HS 6671 20, 21, 22

SERIAL NO. 1 PART NO.

DATE _____
ENGINEER _____
OPERATORS _____

1

[illegible]

DR. MADRY.

-123

ENGINEERING LABORATORIES

2

22

1

PLAN OF TEST NO.

SERIAL NO.

ON LIVE

DATE:

ENGINEER

OPERATORS

153

REPORT NO.
HSE 7002

[illegible]

REMARKS:

... NO

Hamilton Standard
DIVISION OF UNITED STATES STEEL COMPANY
3509 LOCKS, CONNECTICUT • U.S.A.

**U
A.**

**LOG OF TEST
ENGINEERING LABORATORIES**

WIG NO. C-27

TYPE OF TEST

W.P.I. NO. 109-002-003A

DATE 10-30-75
ENGINEER A. S. Smith
OPERATORS F. S. Smith

PLAN OF TEST NO.
SERIAL NO.

PART NO.

UNITS →	TIME	RPM	G-Box Accel	VIBRATION VERT HORIZ	REMARKS
	100		20	0 0	
	1000		20	0 0	
	1500		20	0 0	
	2000		20	0 0	
	2500		20	.1 .1	
	3000		20	.2 .1	WITH BELT ADDED
	3000		20	.1 .1	WITHOUT BELT

ORIGINAL PAGE
OF FOUR

REMARKS

LOG OF TEST ENGINEERING LABORATORIES

DATE 11-2-68 ET OF
ENGINEER W. J. [Signature]
OPERATORS

PLAN OF TEST NO. 228 PT-31 10-1-1
SERIAL NO. 1 PART NO. 228 PT-31-1

RIG NO. 7-2
TYPE OF TEST 2-1
W.P.I. NO.

UNITS →

TIME

Set electrical stop

ORIGINAL OF POOR QUALITY

REMARKS:

PAGE NO
127

REPORT NO.
HSER 7002

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WEAVERS

PAGE NO

REPORT NO.

HSER 7002

ORIGINAL PAGE IS

LOG OF TEST ENGINEERING LABORATORIES

DATE 11.2.25
ENGINEER D. J. L. J. L.
OPERATORS T. J. L. J. L.

RIG NO. 6-7

TYPE OF TEST ()

TYPE OF TEST G.E. WETTED DENSITY
W.P.I. NO. 109-C07-402R

Functional Test

PLAN OF TEST NO. 222PT-31 Rev. H
SERIAL NO. _____ PART NO. 763509

PART NO. 763534

[illegible]

REPORT NO.

HSER 7002

REMARKS:

PAGE NO
133

LOG OF TEST ENGINEERING LABORATORIES

DATE 11-26-72 SHEET 3 OF
ENGINEER 1850101
OPERATORS

134

97-908-603-10F B
PLAN OF TEST NO. 222PT-31 Rev A
SERIAL NO. PART NO. 762570

[illegible]

REMARKS

PAGE NO

REPORT NO.
HSER 7002

LOG OF TEST ENGINEERING LABORATORIES

13 REG NO. G-7

DATE 11-28-78 SHEET 5 OF 5
ENGINEER D. L. Smith
OPERATORS D. L. Smith

ENGINEER W. L. Schmitt
OPERATORS J. K. Jones

PLAN OF TEST NO. 222 PJ-51 Rev A
SERIAL NO.

PLAN OF TEST
SERIAL NO.

-E-Office Activities and Travel Cost
105-003-4023

TYPE OF TEST

[illegible]

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JAN 10 1968

REPORT NO
USER 700

PAGE NO

LOG OF TEST ENGINEERING LABORATORIES

SHEET 6 OF 11
DATE 11-28-75
ENGINEER D. Smith
OPERATORS 11/28/75

MG NO.

	TYPE OF TEST
1.	Visual inspection
2.	Hand palpation
3.	Instrumental examination
4.	Microscopic examination
5.	Culture and sensitivity testing
6.	Histopathological examination
7.	Molecular biology techniques
8.	Immunological assays
9.	Radiological imaging
10.	Genetic testing
11.	Pharmacogenetics
12.	Toxicology
13.	Environmental health assessment
14.	Epidemiological studies
15.	Public health surveillance
16.	Vaccine development
17.	Antibiotic resistance monitoring
18.	Drug safety pharmacovigilance
19.	Regulatory affairs
20.	Health economics
21.	Health equity research
22.	Global health initiatives
23.	Digital health technologies
24.	Artificial intelligence in medicine
25.	Nanotechnology applications
26.	Bioinformatics
27.	Systems biology
28.	Personalized medicine
29.	Regenerative medicine
30.	Tissue engineering
31.	Stem cell research
32.	CRISPR-Cas9 gene editing
33.	Synthetic biology
34.	Bioprinting
35.	Organ-on-a-chip technology
36.	Protein engineering
37.	Enzyme replacement therapy
38.	Gene therapy
39.	Cellular immunotherapy
40.	Chimeric antigen receptor (CAR) T-cell therapy
41.	Exosome-based drug delivery
42.	Hydrogel-based tissue scaffolds
43.	3D printing of medical devices
44.	Wearable health sensors
45.	Mobile health applications
46.	Telemedicine services
47.	Virtual reality training simulations
48.	Augmented reality surgical navigation
49.	Robot-assisted minimally invasive surgery
50.	Autonomous medical robots
51.	Smart drug delivery systems
52.	Targeted cancer therapies
53.	Immunomodulators
54.	Anti-inflammatory drugs
55.	Pain management strategies
56.	Anesthesia techniques
57.	Transfusion medicine
58.	Organ transplantation
59.	Xenotransplantation research
60.	Artificial organs
61.	Biomechanical modeling
62.	Computational fluid dynamics
63.	Finite element analysis
64.	Structural optimization
65.	Material science for implants
66.	Corrosion resistance studies
67.	Surface modification techniques
68.	Coatings for biomaterials
69.	Adhesion promotion agents
70.	Biocompatibility testing
71.	In vivo biodegradation studies
72.	Accelerated degradation testing
73.	Leachate characterization
74.	Biological activity assays
75.	Cell viability tests
76.	Apoptosis induction assays
77.	Gene expression profiling
78.	Protein quantification methods
79.	Mass spectrometry
80.	High-resolution mass spectrometry
81.	Liquid chromatography-mass spectrometry (LC-MS)
82.	Gas chromatography-mass spectrometry (GC-MS)
83.	Thin-layer chromatography (TLC)
84.	Size exclusion chromatography (SEC)
85.	Affinity chromatography
86.	Ion exchange chromatography
87.	Reverse-phase HPLC
88.	Normal-phase HPLC
89.	Supercritical fluid chromatography (SFC)
90.	Capillary electrophoresis (CE)
91.	Isotachopherometry
92.	Amperometric detection
93.	Fluorimetric detection
94.	UV-Vis absorption spectroscopy
95.	Infrared (IR) spectroscopy
96.	Raman spectroscopy
97.	Nuclear magnetic resonance (NMR) spectroscopy
98.	Electron spin resonance (ESR) spectroscopy
99.	Atomic force microscopy (AFM)
100.	Scanning electron microscopy (SEM)
101.	Transmission electron microscopy (TEM)
102.	Scanning tunneling microscopy (STM)
103.	Photolithography
104.	Etching processes
105.	Spin coating
106.	Chemical vapor deposition (CVD)
107.	Physical vapor deposition (PVD)
108.	Sputter coating
109.	Evaporation
110.	Langmuir-Blodgett films
111.	Self-assembled monolayers (SAMs)
112.	Block copolymer brushes
113.	Graft copolymers
114.	Star polymers
115.	Hyperbranched polymers
116.	Conjugated polymers
117.	Polymers of intrinsic microporosity (PIMs)
118.	MOFs (Metal-Organic Frameworks)
119.	COFs (Covalent Organic Frameworks)
120.	Zeolites
121.	Clay minerals
122.	Carbon nanotubes
123.	Graphene
124.	Fullerenes
125.	Quantum dots
126.	Nanowires
127.	Nanobubbles
128.	Nanofibers
129.	Nanoparticles
130.	Encapsulation techniques
131.	Emulsions
132.	Microcapsules
133.	Macroencapsulations
134.	Miniemulsions
135.	Nanoemulsions
136.	Exosomes
137.	Liposomes
138.	Polymeric nanoparticles
139.	Inorganic nanoparticles
140.	Hybrid nanoparticles
141.	Core-shell structures
142.	Janus particles
143.	Amphiphilic molecules
144.	Surfactants
145.	Block copolymers
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176.	Surfactants
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178.	Star polymers
179.	Hyperbranched polymers
180.	Conjugated polymers

W.P.I. NO.

[illegible]

SERIAL NO.

PART NO. 100-100

UNITS	TIME	1000	1001	1002	1003	1004	1005	1006	1007	1008	1009	1010	1011	1012	1013	1014	1015	1016	1017	1018	1019	1020	1021	1022	1023	1024	1025	1026	1027	1028	1029	1030	1031	1032	1033	1034	1035	1036	1037	1038	1039	1040	1041	1042	1043	1044	1045	1046	1047	1048	1049	1050	1051	1052	1053	1054	1055	1056	1057	1058	1059	1060	1061	1062	1063	1064	1065	1066	1067	1068	1069	1070	1071	1072	1073	1074	1075	1076	1077	1078	1079	1080	1081	1082	1083	1084	1085	1086	1087	1088	1089	1090	1091	1092	1093	1094	1095	1096	1097	1098	1099	1100	1101	1102	1103	1104	1105	1106	1107	1108	1109	1110	1111	1112	1113	1114	1115	1116	1117	1118	1119	1120	1121	1122	1123	1124	1125	1126	1127	1128	1129	1130	1131	1132	1133	1134	1135	1136	1137	1138	1139	1140	1141	1142	1143	1144	1145	1146	1147	1148	1149	1150	1151	1152	1153	1154	1155	1156	1157	1158	1159	1160	1161	1162	1163	1164	1165	1166	1167	1168	1169	1170	1171	1172	1173	1174	1175	1176	1177	1178	1179	1180	1181	1182	1183	1184	1185	1186	1187	1188	1189	1190	1191	1192	1193	1194	1195	1196	1197	1198	1199	1200	1201	1202	1203	1204	1205	1206	1207	1208	1209	1210	1211	1212	1213	1214	1215	1216	1217	1218	1219	1220	1221	1222	1223	1224	1225	1226	1227	1228	1229	1230	1231	1232	1233	1234	1235	1236	1237	1238	1239	1240	1241	1242	1243	1244	1245	1246	1247	1248	1249	1250	1251	1252	1253	1254	1255	1256	1257	1258	1259	1260	1261	1262	1263	1264	1265	1266	1267	1268	1269	1270	1271	1272	1273	1274	1275	1276	1277	1278	1279	1280	1281	1282	1283	1284	1285	1286	1287	1288	1289	1290	1291	1292	1293	1294	1295	1296	1297	1298	1299	1300	1301	1302	1303	1304	1305	1306	1307	1308	1309	1310	1311	1312	1313	1314	1315	1316	1317	1318	1319	1320	1321	1322	1323	1324	1325	1326	1327	1328	1329	1330	1331	1332	1333	1334	1335	1336	1337	1338	1339	1340	1341	1342	1343	1344	1345	1346	1347	1348	1349	1350	1351	1352	1353	1354	1355	1356	1357	1358	1359	1360	1361	1362	1363	1364	1365	1366	1367	1368	1369	1370	1371	1372	1373	1374	1375	1376	1377	1378	1379	1380	1381	1382	1383	1384	1385	1386	1387	1388	1389	1390	1391	1392	1393	1394	1395	1396	1397	1398	1399	1400	1401	1402	1403	1404	1405	1406	1407	1408	1409	1410	1411	1412	1413	1414	1415	1416	1417	1418	1419	1420	1421	1422	1423	1424	1425	1426	1427	1428	1429	1430	1431	1432	1433	1434	1435	1436	1437	1438	1439	1440	1441	1442	1443	1444	1445	1446	1447	1448	1449	1450	1451	1452	1453	1454	1455	1456	1457	1458	1459	1460	1461	1462	1463	1464	1465	1466	1467	1468	1469	1470	1471	1472	1473	1474	1475	1476	1477	1478	1479	1480	1481	1482	1483	1484	1485	1486	1487	1488	1489	1490	1491	1492	1493	1494	1495	1496	1497	1498	1499	1500	1501	1502	1503	1504	1505	1506	1507	1508	1509	1510	1511	1512	1513	1514	1515	1516	1517	1518	1519	1520	1521	1522	1523	1524	1525	1526	1527	1528	1529	1530	1531	1532	1533	1534	1535	1536	1537	1538	1539	1540	1541	1542	1543	1544	1545	1546	1547	1548	1549	1550	1551	1552	1553	1554	1555	1556	1557	1558	1559	1560	1561	1562	1563	1564	1565	1566	1567	1568	1569	1570	1571	1572	1573	1574	1575	1576	1577	1578	1579	1580	1581	1582	1583	1584	1585	1586	1587	1588	1589	1590	1591	1592	1593	1594	1595	1596	1597	1598	1599	1600	1601	1602	1603	1604	1605	1606	1607	1608	1609	1610	1611	1612	1613	1614	1615	1616	1617	1618	1619	1620	1621	1622	1623	1624	1625	1626	1627	1628	1629	1630	1631	1632	1633	1634	1635	1636	1637	1638	1639	1640	1641	1642	1643	1644	1645	1646	1647	1648	1649	1650	1651	1652	1653	1654	1655	1656	1657	1658	1659	1660	1661	1662	1663	1664	1665	1666	1667	1668	1669	1670	1671	1672	1673	1674	1675	1676	1677	1678	1679	1680	1681	1682	1683	1684	1685	1686	1687	1688	1689	1690	1691	1692	1693	1694	1695	1696	1697	1698	1699	1700	1701	1702	1703	1704	1705	1706	1707	1708	1709	1710	1711	1712	1713	1714	1715	1716	1717	1718	1719	1720	1721	1722	1723	1724	1725	1726	1727	1728	1729	1730	1731	1732	1733	1734	1735	1736	1737	1738	1739	1740	1741	1742	1743	1744	1745	1746	1747	1748	1749	1750	1751	1752	1753	1754	1755	1756	1757	1758	1759	1760	1761	1762	1763	1764	1765	1766	1767	1768	1769	1770	1771	1772	1773	1774	1775	1776	1777	1778	1779	1780	1781	1782	1783	1784	1785	1786	1787	1788	1789	1790	1791	1792	1793	1794	1795	1796	1797	1798	1799	1800	1801	1802	1803	1804	1805	1806	1807	1808	1809	1810	1811	1812	1813	1814	1815	1816	1817	1818	1819	1820	1821	1822	1823	1824	1825	1826	1827	1828	1829	1830	1831	1832	1833	1834	1835	1836	1837	1838	1839	1840	1841	1842	1843	1844	1845	1846	1847	1848	1849	1850	1851	1852	1853	1854	1855	1856	1857	1858	1859	1860	1861	1862	1863	1864	1865	1866	1867	1868	1869	1870	1871	1872	1873	1874	1875	1876	1877	1878	1879	1880	1881	1882	1883	1884	1885	1886	1887	1888	1889	1890	1891	1892	1893	1894	1895	1896	1897	1898	1899	1900	1901	1902	1903	1904	1905	1906	1907	1908	1909	1910	1911	1912	1913	1914	1915	1916	1917	1918	1919	1920	1921	1922	1923	1924	1925	1926	1927	1928	1929	1930	1931	1932	1933	1934	1935	1936	1937	1938	1939	1940	1941	1942	1943	1944	1945	1946	1947	1948	1949	1950	1951	1952	1953	1954	1955	1956	1957	1958	1959	1960	1961	1962	1963	1964	1965	1966	1967	1968	1969	1970	1971	1972	1973	1974	1975	1976	1977	1978	1979	1980	1981	1982	1983	1984	1985	1986	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	1997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REMARKS

PAGE NO.
137

REPORT NO.

HSER 7002

LOG OF TEST ENGINEERING LABORATORIES

DATE 11-1-68 SHEET 1 OF 1
ENGINEER D. J. [Signature]
OPERATORS [Signature]

R/G NO. 1
TYPE OF TEST 100% - 100%
P.I. NO. 100% - 100%
PLAN OF TEST NO. 100% - 100%
SERIAL NO. 100% - 100%

[illegible]

REMARKS:

* Corrected Quiz on Page 9

REPORT NO.
HSER 7002

LOG OF TEST ENGINEERING LABORATORIES

DATE 11-23-78 SHEET 9 OF
ENGINEER D. H. S. J.
OPERATORS J. H. S. J.

PLAN OF TEST NO. 222PT-372 Rev A
SERIAL NO.

140
 FIG. NO. 6-7
 TYPE OF TEST 96.5% Test for Infrared Test
 W.P.I. NO. 96.5-603-10013

[illegible]

REPORT NO.
HSER 7002

PAGE NO

LOG OF TEST ENGINEERING LABORATORIES

DATE 11-23-75
ENGINEER
OPERATORS

RIG NO. 1
TYPE OF TEST
W.P.I. NO.

PLAN OF TEST NO. 22287-313-1
SERIAL NO. PART NO.

[illegible]

REMARKS:

REPORT NO.
HSER 7002

LOG OF TEST ENGINEERING LABORATORIES

DATE 11-22-66 SHEET 12 of 12
ENGINEER S. J. [illegible]
OPERATORS [illegible]

PLAN OF TEST NO. 222PT-31 Rev A

See Act for Functional Test
179-003-1047B

PIC NO 6-7
TYPE OF TEST G-1
W.P.I. NO 1

[illegible]

James A. H. Co. 1900

REPORT NO.
HSER 7002

Hamilton Standard

WINDSOR LOCKS, CONNECTICUT • U.S.A.

U
A.

LOG OF TEST
ENGINEERING LABORATORIES

14

INC. NO.

TYPE OF TEST
W.P.I. NO.

PLAN OF TEST NO.

SERIAL NO.

DATE 11-27-53
ENGINEER D. WEISS
OPERATORS J. KOVACH

UNITS	TIME	3065	3066	3067	3068	3069	3070	3071	3072	3073	3074	3075	3076	3077	3078	3079	3080	3081	3082	3083	3084	3085	3086	3087	3088	3089	3090	3091	3092	3093	3094	3095	3096	3097	3098	3099	3100	3101	3102	3103	3104	3105	3106	3107	3108	3109	3110	3111	3112	3113	3114	3115	3116	3117	3118	3119	3120	3121	3122	3123	3124	3125	3126	3127	3128	3129	3130	3131	3132	3133	3134	3135	3136	3137	3138	3139	3140	3141	3142	3143	3144	3145	3146	3147	3148	3149	3150	3151	3152	3153	3154	3155	3156	3157	3158	3159	3160	3161	3162	3163	3164	3165	3166	3167	3168	3169	3170	3171	3172	3173	3174	3175	3176	3177	3178	3179	3180	3181	3182	3183	3184	3185	3186	3187	3188	3189	3190	3191	3192	3193	3194	3195	3196	3197	3198	3199	3200	3201	3202	3203	3204	3205	3206	3207	3208	3209	3210	3211	3212	3213	3214	3215	3216	3217	3218	3219	3220	3221	3222	3223	3224	3225	3226	3227	3228	3229	3230	3231	3232	3233	3234	3235	3236	3237	3238	3239	3240	3241	3242	3243	3244	3245	3246	3247	3248	3249	3250	3251	3252	3253	3254	3255	3256	3257	3258	3259	3260	3261	3262	3263	3264	3265	3266	3267	3268	3269	3270	3271	3272	3273	3274	3275	3276	3277	3278	3279	3280	3281	3282	3283	3284	3285	3286	3287	3288	3289	3290	3291	3292	3293	3294	3295	3296	3297	3298	3299	3300	3301	3302	3303	3304	3305	3306	3307	3308	3309	3310	3311	3312	3313	3314	3315	3316	3317	3318	3319	3320	3321	3322	3323	3324	3325	3326	3327	3328	3329	3330	3331	3332	3333	3334	3335	3336	3337	3338	3339	3340	3341	3342	3343	3344	3345	3346	3347	3348	3349	3350	3351	3352	3353	3354	3355	3356	3357	3358	3359	3360	3361	3362	3363	3364	3365	3366	3367	3368	3369	3370	3371	3372	3373	3374	3375	3376	3377	3378	3379	3380	3381	3382	3383	3384	3385	3386	3387	3388	3389	3390	3391	3392	3393	3394	3395	3396	3397	3398	3399	3400	3401	3402	3403	3404	3405	3406	3407	3408	3409	3410	3411	3412	3413	3414	3415	3416	3417	3418	3419	3420	3421	3422	3423	3424	3425	3426	3427	3428	3429	3430	3431	3432	3433	3434	3435	3436	3437	3438	3439	3440	3441	3442	3443	3444	3445	3446	3447	3448	3449	3450	3451	3452	3453	3454	3455	3456	3457	3458	3459	3460	3461	3462	3463	3464	3465	3466	3467	3468	3469	3470	3471	3472	3473	3474	3475	3476	3477	3478	3479	3480	3481	3482	3483	3484	3485	3486	3487	3488	3489	3490	3491	3492	3493	3494	3495	3496	3497	3498	3499	3500	3501	3502	3503	3504	3505	3506	3507	3508	3509	3510	3511	3512	3513	3514	3515	3516	3517	3518	3519	3520	3521	3522	3523	3524	3525	3526	3527	3528	3529	3530	3531	3532	3533	3534	3535	3536	3537	3538	3539	3540	3541	3542	3543	3544	3545	3546	3547	3548	3549	3550	3551	3552	3553	3554	3555	3556	3557	3558	3559	3560	3561	3562	3563	3564	3565	3566	3567	3568	3569	3570	3571	3572	3573	3574	3575	3576	3577	3578	3579	3580	3581	3582	3583	3584	3585	3586	3587	3588	3589	3590	3591	3592	3593	3594	3595	3596	3597	3598	3599	3600	3601	3602	3603	3604	3605	3606	3607	3608	3609	3610	3611	3612	3613	3614	3615	3616	3617	3618	3619	3620	3621	3622	3623	3624	3625	3626	3627	3628	3629	3630	3631	3632	3633	3634	3635	3636	3637	3638	3639	3640	3641	3642	3643	3644	3645	3646	3647	3648	3649	3650	3651	3652	3653	3654	3655	3656	3657	3658	3659	3660	3661	3662	3663	3664	3665	3666	3667	3668	3669	3670	3671	3672	3673	3674	3675	3676	3677	3678	3679	3680	3681	3682	3683	3684	3685	3686	3687	3688	3689	3690	3691	3692	3693	3694	3695	3696	3697	3698	3699	3700	3701	3702	3703	3704	3705	3706	3707	3708	3709	3710	3711	3712	3713	3714	3715	3716	3717	3718	3719	3720	3721	3722	3723	3724	3725	3726	3727	3728	3729	3730	3731	3732	3733	3734	3735	3736	3737	3738	3739	3740	3741	3742	3743	3744	3745	3746	3747	3748	3749	3750	3751	3752	3753	3754	3755	3756	3757	3758	3759	3760	3761	3762	3763	3764	3765	3766	3767	3768	3769	3770	3771	3772	3773	3774	3775	3776	3777	3778	3779	3780	3781	3782	3783	3784	3785	3786	3787	3788	3789	3790	3791	3792	3793	3794	3795	3796	3797	3798	3799	3800	3801	3802	3803	3804	3805	3806	3807	3808	3809	3810	3811	3812	3813	3814	3815	3816	3817	3818	3819	3820	3821	3822	3823	3824	3825	3826	3827	3828	3829	3830	3831	3832	3833	3834	3835	3836	3837	3838	3839	3840	3841	3842	3843	3844	3845	3846	3847	3848	3849	3850	3851	3852	3853	3854	3855	3856	3857	3858	3859	3860	3861	3862	3863	3864	3865	3866	3867	3868	3869	3870	3871	3872	3873	3874	3875	3876	3877	3878	3879	3880	3881	3882	3883	3884	3885	3886	3887	3888	3889	3890	3891	3892	3893	3894	3895	3896	3897	3898	3899	3900	3901	3902	3903	3904	3905	3906	3907	3908	3909	3910	3911	3912	3913	3914	3915	3916	3917	3918	3919	3920	3921	3922	3923	3924	3925	3926	3927	3928	3929	3930	3931	3932	3933	3934	3935	3936	3937	3938	3939	3940	3941	3942	3943	3944	3945	3946	3947	3948	3949	3950	3951	3952	3953	3954	3955	3956	3957	3958	3959	3960	3961	3962	3963	3964	3965	3966	3967	3968	3969	3970	3971	3972	3973	3974	3975	3976	3977	3978	3979	3980	3981	3982	3983	3984	3985	3986	3987	3988	3989	3990	3991	3992	3993	3994	3995	3996	3997	3998	3999	4000	4001	4002	4003	4004	4005	4006	4007	4008	4009	4010	4011	4012	4013	4014	4015	4016	4017	4018	4019	4020	4021	4022	4023	4024	4025	4026	4027	4028	4029	4030	4031	4032	4033	4034	4035	4036	4037	4038	4039	4040	4041	4042	4043	4044	4045	4046	4047	4048	4049	4050	4051	4052	4053	4054	4055	4056	4057	4058	4059	4060	4061	4062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LOG OF TEST ENGINEERING LABORATORIES

On 5th

TRP. OF U.S.

W.P.I. NO.

DATE _____

Practical

CRIMINALS

2017/408

222P1-2/100A

11

SERIAL NO.

PART TWO

[illegible]

REMARKS:

PAGE NO
145

REPORT NO.
HSER 7002

LOG OF TEST ENGINEERING LABORATORIES

146
ECG NO.
TYPE OF TEST
W.P.I. NO.

DATE 12/1/62 SHEET 1 OF 1
ENGINEER D. J. Smith
OPERATOR J. C. Smith

W.P.I. NO. _____
DATE OF TEST _____
NAME OF TESTER _____
NAME OF TEST NO. _____

Serial No.

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DEMANDS

PAGE NO

REPORT NO.
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WINDSOR LOCKS, CONNECTICUT • U.S.A.

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LOG OF TEST

ENGINEERING LABORATORIES

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PLAN OF TEST NO.

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2224-1

340

Discarded

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11/18

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100

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DEWARS.

PAGE NO
147

REPORT NO.

HSER 7002

10

100

12-10-68

PART NO. 162570

[illegible]

528VW38

UNIT NO.	TYPE OF TEST	W.P.I. NO.	Serial No.	PLAN OF TEST NO.	PART NO.	OPERATOR
UNITS						
TIME						
1354	4.7	27	178	78	3550/18.5	14.5
1355	4.7	27	178	78	3550/18.5	14.5
1356	4.7	27	178	78	3550/18.5	14.5
1357	4.7	27	178	78	3550/18.5	14.5
1358	4.7	27	178	78	3550/18.5	14.5
1359	4.7	27	178	78	3550/18.5	14.5
1360	4.7	27	178	78	3550/18.5	14.5
1361	4.7	27	178	78	3550/18.5	14.5
1362	4.7	27	178	78	3550/18.5	14.5
1363	4.7	27	178	78	3550/18.5	14.5
1364	4.7	27	178	78	3550/18.5	14.5
1365	4.7	27	178	78	3550/18.5	14.5
1366	4.7	27	178	78	3550/18.5	14.5
1367	4.7	27	178	78	3550/18.5	14.5
1368	4.7	27	178	78	3550/18.5	14.5
1369	4.7	27	178	78	3550/18.5	14.5
1370	4.7	27	178	78	3550/18.5	14.5
1371	4.7	27	178	78	3550/18.5	14.5
1372	4.7	27	178	78	3550/18.5	14.5
1373	4.7	27	178	78	3550/18.5	14.5
1374	4.7	27	178	78	3550/18.5	14.5
1375	4.7	27	178	78	3550/18.5	14.5
1376	4.7	27	178	78	3550/18.5	14.5
1377	4.7	27	178	78	3550/18.5	14.5
1378	4.7	27	178	78	3550/18.5	14.5
1379	4.7	27	178	78	3550/18.5	14.5
1380	4.7	27	178	78	3550/18.5	14.5
1381	4.7	27	178	78	3550/18.5	14.5
1382	4.7	27	178	78	3550/18.5	14.5
1383	4.7	27	178	78	3550/18.5	14.5
1384	4.7	27	178	78	3550/18.5	14.5
1385	4.7	27	178	78	3550/18.5	14.5
1386	4.7	27	178	78	3550/18.5	14.5
1387	4.7	27	178	78	3550/18.5	14.5
1388	4.7	27	178	78	3550/18.5	14.5
1389	4.7	27	178	78	3550/18.5	14.5
1390	4.7	27	178	78	3550/18.5	14.5
1391	4.7	27	178	78	3550/18.5	14.5
1392	4.7	27	178	78	3550/18.5	14.5
1393	4.7	27	178	78	3550/18.5	14.5
1394	4.7	27	178	78	3550/18.5	14.5
1395	4.7	27	178	78	3550/18.5	14.5
1396	4.7	27	178	78	3550/18.5	14.5
1397	4.7	27	178	78	3550/18.5	14.5
1398	4.7	27	178	78	3550/18.5	14.5
1399	4.7	27	178	78	3550/18.5	14.5
1400	4.7	27	178	78	3550/18.5	14.5
1401	4.7	27	178	78	3550/18.5	14.5
1402	4.7	27	178	78	3550/18.5	14.5
1403	4.7	27	178	78	3550/18.5	14.5
1404	4.7	27	178	78	3550/18.5	14.5
1405	4.7	27	178	78	3550/18.5	14.5
1406	4.7	27	178	78	3550/18.5	14.5
1407	4.7	27	178	78	3550/18.5	14.5
1408	4.7	27	178	78	3550/18.5	14.5
1409	4.7	27	178	78	3550/18.5	14.5
1410	4.7	27	178	78	3550/18.5	14.5
1411	4.7	27	178	78	3550/18.5	14.5
1412	4.7	27	178	78	3550/18.5	14.5
1413	4.7	27	178	78	3550/18.5	14.5
1414	4.7	27	178	78	3550/18.5	14.5
1415	4.7	27	178	78	3550/18.5	14.5
1416	4.7	27	178	78	3550/18.5	14.5
1417	4.7	27	178	78	3550/18.5	14.5
1418	4.7	27	178	78	3550/18.5	14.5
1419	4.7	27	178	78	3550/18.5	14.5
1420	4.7	27	178	78	3550/18.5	14.5
1421	4.7	27	178	78	3550/18.5	14.5
1422	4.7	27	178	78	3550/18.5	14.5
1423	4.7	27	178	78	3550/18.5	14.5
1424	4.7	27	178	78	3550/18.5	14.5
1425	4.7	27	178	78	3550/18.5	14.5
1426	4.7	27	178	78	3550/18.5	14.5
1427	4.7	27	178	78	3550/18.5	14.5
1428	4.7	27	178	78	3550/18.5	14.5
1429	4.7	27	178	78	3550/18.5	14.5
1430	4.7	27	178	78	3550/18.5	14.5
1431	4.7	27	178	78	3550/18.5	14.5
1432	4.7	27	178	78	3550/18.5	14.5
1433	4.7	27	178	78	3550/18.5	14.5
1434	4.7	27	178	78	3550/18.5	14.5
1435	4.7	27	178	78	3550/18.5	14.5
1436	4.7	27	178	78	3550/18.5	14.5
1437	4.7	27	178	78	3550/18.5	14.5
1438	4.7	27	178	78	3550/18.5	14.5
1439	4.7	27	178	78	3550/18.5	14.5
1440	4.7	27	178	78	3550/18.5	14.5

MEMBERS.

PAGE NO

LOG OF TEST ENGINEERING LABORATORIES

DATE 12-20-77 SHEET 20 OF 21

DATE 12-1-77
ENGINEER [Signature]
OPERATORS [Signature]

PLAN OF TEST NO. 222 PF-31 QvA

[illegible]

REMARKS

REPORT NO.
HSER 7002

[illegible]

REMARKS:

PAGE NO

REPORT NO.
USER 7002

RIG NO. 156
TYPE OF TEST 156
W.P.I. NO. 156
PLAN OF TEST NO. 156
SERIAL NO. 156
PART NO. 156

UNITS	TIME	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	220	221	222	223	224	225	226	227	228	229	230	231	232	233	234	235	236	237	238	239	240	241	242	243	244	245	246	247	248	249	250	251	252	253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273	274	275	276	277	278	279	280	281	282	283	284	285	286	287	288	289	290	291	292	293	294	295	296	297	298	299	300	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315	316	317	318	319	320	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335	336	337	338	339	340	341	342	343	344	345	346	347	348	349	350	351	352	353	354	355	356	357	358	359	360	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	376	377	378	379	380	381	382	383	384	385	386	387	388	389	390	391	392	393	394	395	396	397	398	399	400	401	402	403	404	405	406	407	408	409	410	411	412	413	414	415	416	417	418	419	420	421	422	423	424	425	426	427	428	429	430	431	432	433	434	435	436	437	438	439	440	441	442	443	444	445	446	447	448	449	450	451	452	453	454	455	456	457	458	459	460	461	462	463	464	465	466	467	468	469	470	471	472	473	474	475	476	477	478	479	480	481	482	483	484	485	486	487	488	489	490	491	492	493	494	495	496	497	498	499	500	501	502	503	504	505	506	507	508	509	510	511	512	513	514	515	516	517	518	519	520	521	522	523	524	525	526	527	528	529	530	531	532	533	534	535	536	537	538	539	540	541	542	543	544	545	546	547	548	549	550	551	552	553	554	555	556	557	558	559	560	561	562	563	564	565	566	567	568	569	570	571	572	573	574	575	576	577	578	579	580	581	582	583	584	585	586	587	588	589	590	591	592	593	594	595	596	597	598	599	600	601	602	603	604	605	606	607	608	609	610	611	612	613	614	615	616	617	618	619	620	621	622	623	624	625	626	627	628	629	630	631	632	633	634	635	636	637	638	639	640	641	642	643	644	645	646	647	648	649	650	651	652	653	654	655	656	657	658	659	660	661	662	663	664	665	666	667	668	669	670	671	672	673	674	675	676	677	678	679	680	681	682	683	684	685	686	687	688	689	690	691	692	693	694	695	696	697	698	699	700	701	702	703	704	705	706	707	708	709	710	711	712	713	714	715	716	717	718	719	720	721	722	723	724	725	726	727	728	729	730	731	732	733	734	735	736	737	738	739	740	741	742	743	744	745	746	747	748	749	750	751	752	753	754	755	756	757	758	759	760	761	762	763	764	765	766	767	768	769	770	771	772	773	774	775	776	777	778	779	780	781	782	783	784	785	786	787	788	789	790	791	792	793	794	795	796	797	798	799	800	801	802	803	804	805	806	807	808	809	810	811	812	813	814	815	816	817	818	819	820	821	822	823	824	825	826	827	828	829	830	831	832	833	834	835	836	837	838	839	840	841	842	843	844	845	846	847	848	849	850	851	852	853	854	855	856	857	858	859	860	861	862	863	864	865	866	867	868	869	870	871	872	873	874	875	876	877	878	879	880	881	882	883	884	885	886	887	888	889	890	891	892	893	894	895	896	897	898	899	900	901	902	903	904	905	906	907	908	909	910	911	912	913	914	915	916	917	918	919	920	921	922	923	924	925	926	927	928	929	930	931	932	933	934	935	936	937	938	939	940	941	942	943	944	945	946	947	948	949	950	951	952	953	954	955	956	957	958	959	960	961	962	963	964	965	966	967	968	969	970	971	972	973	974	975	976	977	978	979	980	981	982	983	984	985	986	987	988	989	990	991	992	993	994	995	996	997	998	999	1000
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REPORT NO.
HSER 7002

REMARKS

PAGE NO.

Hamilton Standard
WINDSOR LOCKS, CONNECTICUT • U.S.A.

LOG OF TEST ENGINEERING LABORATORIES

DATE 12-3-75 SHEET 26 OF 27

FIG NO. 7

TYPE OF TEST Explosive Actometer Func
W.P.I. NO. 109-CD3-4102B

PLAN OF TEST

222 PT-31 Rev. A

PART NO 771053

[illegible]

**LOG OF TEST
ENGINEERING LABORATORIES**

DATE 12-27-74 SHEET 27 OF 28
ENGINEER D. J. ...
OPERATORS

158

REG. NO.	5
TYPE OF TEST	
W.P.I. NO.	

Actuals Functions List

PLAN OF TEST NO. 22207-21 SUB
SERIAL NO. 6039

PART NO.

[illegible]

PAGE NO

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Hamilton Standard WINDSOR LOCKS CONNECTICUT - U.S.A.

LOG OF TEST
ENGINEERING LABORATORIES

FIG. NO. 6-17

TYPE OF TEST

W.P.I. NO.

222-11-31

PLAN OF TEST NO.

222-11-31

REV. A

DATE 12-2-79

ENGINEER D. J. ...

OPERATORS

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REPORT NO.
HSER 7002

HS 1758 4/67

Hamilton Standard
WINDSOR LOCKS, CONNECTICUT • U.S.A.

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DIVISION OF UNITED STATES CUSTOMS

LOG OF TEST
ENGINEERING LABORATORIES

162
TYPE OF TEST
W.P.I. NO.

DATE 12-2-76
ENGINEER
OPERATORS

UNITS	TIME	W.P.I. NO.	PLAN OF TEST NO.	SERIAL NO.	PART NO.	REMARKS
1750	2 54	24 03	4.7	Completed Flight Cycle #158 and started #159		
1755	2 51	24 02	4.7	Completed Flight Cycle #157 and started #160		
1758	2 52	24 10	4.7	3008 205 90 3550 17.5	94° 129° 110° 113°	.1 .2 18.66
1800	3 21	24 12	4.7	Completed Flight Cycle #160 and started #161		
1804	3 08	24 16	4.7	Completed Flight Cycle #161 and started #162		
1806	3 10	24 18	4.7	3408 211 90 3550 17.5	95° 131° 114° 113°	.1 .2 06.92
1810	3 11	24 22	4.7	Completed Flight Cycle #162 and started #163		
1815	3 19	24 27	4.7	Completed Flight Cycle #163 and started #164		
1817	3 21	24 29	4.7	3408 215 90 3550 17.5	94° 136° 116° 114°	.1 .2 03.97
1819	3 23	24 31	4.7	Completed Flight Cycle #164 and started #165		
1824	3 25	24 36	4.7	Completed Flight Cycle #165 and started #166		
1827	3 33	24 41	4.7	2700 218 90 3550 17.5	93° 136° 117° 113°	.1 .3 101.00
1830	3 34	24 42	4.7	Completed Flight Cycle #166 and started #167		
1834	3 33	24 46	4.7	Completed Flight Cycle #167 and started #168		
1836	3 40	24 49	4.7	3408 217 90 3550 17.5	94° 129° 113° 113°	.1 .2 09.25
1841	3 41	24 53		Completed Flight Cycle #168 and started #169		

REPORT NO.
HSER 7002

PAGE NO

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Hamilton Standard
WINDSOR LOCKS, CONNECTICUT • U.S.A.

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LOG OF TEST
ENGINEERING LABORATORIES

PIC NO. **G-7**

TYPE OF TEST
WIPING

DATE OF TEST
10-2-55

PLAN OF TEST NO.
222PT-31

DATE
12-3-55

ENGINEER
W. H. HARRIS

OPERATORS
W. H. HARRIS

TIME	REMARKS	SERIAL NO.	PART NO.	ANGLE	TIME	ANGLE	TIME	ANGLE
15:10 3 41 25 4.7	Completed Flight Cycle #170	3550175	34	131° 115'	1.1	10106		
15:20 3 41 25 4.7	Completed Flight Cycle #170 and started #171	3550175	34	131° 115'	1.1	10106		
15:30 3 41 25 4.7	Completed Flight Cycle #171 and started #172	3550175	34	131° 115'	1.1	10106		
15:40 3 41 25 4.7	Completed Flight Cycle #172 and started #173	3550175	34	131° 115'	1.1	10106		
15:50 3 41 25 4.7	Completed Flight Cycle #173 and started #174	3550175	34	131° 115'	1.1	10106		
16:00 3 41 25 4.7	Completed Flight Cycle #174 and started #175	3550175	34	131° 115'	1.1	10106		
16:10 3 41 25 4.7	Completed Flight Cycle #175 and started #176	3550175	34	131° 115'	1.1	10106		
16:20 3 41 25 4.7	Completed Flight Cycle #176 and started #177	3550175	34	131° 115'	1.1	10106		
16:30 3 41 25 4.7	Completed Flight Cycle #177 and started #178	3550175	34	131° 115'	1.1	10106		
16:40 3 41 25 4.7	Completed Flight Cycle #178 and started #179	3550175	34	131° 115'	1.1	10106		
16:50 3 41 25 4.7	Completed Flight Cycle #179 and started #180	3550175	34	131° 115'	1.1	10106		

REMARKS

215 NO.

TYPE OF YESS

2000

12/15/75

TABLE

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Abstract

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MARKS:

PAGE NO
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HSER 7002

LOG OF TEST ENGINEERING LABORATORIES

DATE 12-10-75, 37 or

FIG NO 6-7

Size of Test

NAME OF TEST C.I. OC VFC ACQUATON
W.P.I. NO. 166-003-A-23

PLAN OF TEST NO.	Endurance Test
	SERIAL NO.

PART NO. 70700

PART NO. 70700

[illegible]

REMARKS:

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REPORT NO
HSER 7002

Hamilton Standard

WINDSOR LOCKS, CONNECTICUT • U.S.A.

DIVISION OF UNITED CARBIDE CORP.

LOG OF TEST

ENGINEERING LABORATORIES

SHEET 35 OF 35

 DATE 12/1/75
 ENGINEER D. J. ...
 OPERATORS J. ...

G-7

 TYPE OF TEST G.E. QCSEE ACTUATOR ENDURANCE TEST
 PLAN OF TEST NO. 222PT-31 Rev. A
 SERIAL NO. 44
 PART NO. 163500

UNITS →	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	deg. Blade Angle
11:30	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
11:45	12	12	12	11	3100	8550	99	3500	12.5	990	1440	1007	95.7	2	1	112°
11:50	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:00	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:05	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:10	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:15	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:20	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:25	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:30	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:35	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:40	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:45	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:50	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
12:55	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
13:00	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°
13:05	12	12	12	11	3100	8550	99	3500	12.5	1020	1440	1007	95.7	2	1	112°

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 HSER 7002

Hamilton Standard
DIVISION OF UNITED AIRCRAFT -
WINDSOR LOCKS, CONNECTICUT • U.S.A.

LOG OF TEST
ENGINEERING LABORATORIES

DATE 12-16-75 SHEET 16 OF 75
ENGINEER D. L. L. L.
OPERATORS L. L. L.

RIG NO. G-7TYPE OF TEST G.E. QCSEE ACTUATOR ENDURANCE TESTW.P.I. NO. 109-CO1-A02-RPLAN OF TEST NO. 222PT-31 Rev. ASERIAL NO. 767500

UNITS →	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deg. Blade Angle
	1100	27	30	11.7	3000	8.5 GPM	99	3500	12.5	11.1	1400	1000	117.2	1	1	100°
	1105	27	30	11.7	3100	8.5 GPM	99	3500	12.5	11.1	1400	1000	117.2	1	1	100°
	1110	27	30	11.7	3100	8.5 GPM	99	3500	12.5	11.1	1400	1000	117.2	1	1	100°
	1115	27	30	11.7	3100	8.5 GPM	99	3500	12.5	11.1	1400	1000	117.2	1	1	100°
	1120	27	30	11.7	3100	8.5 GPM	99	3500	12.5	11.1	1400	1000	117.2	1	1	100°
					COMPLETED 2800	8.5 GPM	99	3500	12.5	11.1	1400	1000	117.2	1	1	100°

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DATE 11-1-72 SHEET 40 OF 40
 ENGINEER W. J. ...
 OPERATORS ...

RIG NO. G-7 PLAN OF TEST NO. 222PT-31 Rev. A PART NO. 767500
 TYPE OF TEST G.E. QCSEE ACTUATOR ENDURANCE TEST SERIAL NO. ...
 W.P.I. NO. 172

TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Dev. Blace Angle
11:00	10:00	11:00	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:05	10:05	11:05	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:10	10:10	11:10	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:15	10:15	11:15	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:20	10:20	11:20	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:25	10:25	11:25	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:30	10:30	11:30	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:35	10:35	11:35	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:40	10:40	11:40	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:45	10:45	11:45	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:50	10:50	11:50	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
11:55	10:55	11:55	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:00	11:00	12:00	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:05	11:05	12:05	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:10	11:10	12:10	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:15	11:15	12:15	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:20	11:20	12:20	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:25	11:25	12:25	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:30	11:30	12:30	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:35	11:35	12:35	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:40	11:40	12:40	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:45	11:45	12:45	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:50	11:50	12:50	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
12:55	11:55	12:55	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1
13:00	12:00	13:00	1.7	3700	0.80	99	3450	18	105.2	105.2	105.2	105.2	1	1	1

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U.A.

LOG OF TEST
ENGINEERING LABORATORIES

RIG NO. G-7

TYPE OF TEST
W.P.I. NO.

G.E. QCSEE ACTUATOR ENDURANCE TEST

PLAN OF TEST NO. 222PT-31

Rev. A

SERIAL NO.

PART NO. 767500

DATE 12/15/87
ENGINEER J. J. J. J.
OPERATORS J. J. J. J.

UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deg. Blade Angle
	21:50	11:50	30:50		3408	.85	99	3450	18	104	126.5	100.5	101.3	.1	.1	700
	21:51	11:51	30:51	4.7	3408	.85	99	3450	18	115	125.5	100.9	108	.1	.1	700
	21:56	11:56	30:56	4.1	2400	.85	99	3450	18	97.4	135.5	102.2	109.7	.1	.1	700
	21:57	11:57	30:57	4.7	2700	.85	99	3450	18	100.7	136.5	108.5	110.3	.1	.1	700
	21:58	11:58	30:58	4.7	2700	.85	99	3450	18	102.4	141.6	108.1	109.3	.1	.1	700
	21:59	11:59	30:59	4.7	3408	.85	99	3450	18	102.6	143.0	109.1	109.1	.1	.1	700
	22:00	12:00	31:00	4.7	3408	.85	99	3450	18	112.0	143.0	109.8	111.1	.1	.1	700
	22:01	12:01	31:01	4.1	3408	.85	99	3450	18	100.7	135.7	110.5	111.6	.1	.1	700
	22:02	12:02	31:02	4.7	3408	.85	99	3450	18	101.6	145.4	110.4	111.1	.1	.1	700
	22:03	12:03	31:03	4.7	3408	.85	99	3450	18	101.6	144.7	110.7	111.8	.1	.1	700
	22:04	12:04	31:04	4.7	3408	.85	99	3450	18	101.6	140.7	110.3	112.2	.1	.1	700
	22:05	12:05	31:05	4.7	2700	.85	99	3450	18	98.4	132.2	113.0	113.0	.1	.1	700
	22:06	12:06	31:06	4.7	2700	.85	99	3450	18	97.4	133.6	111.6	112.5	.1	.1	700
	22:07	12:07	31:07	4.7	2700	.85	99	3450	18	98.4	132.2	113.0	113.0	.1	.1	700
	22:08	12:08	31:08	4.7	2700	.85	99	3450	18	97.4	133.6	111.6	112.5	.1	.1	700
	22:09	12:09	31:09	4.7	2700	.85	99	3450	18	98.4	132.2	113.0	113.0	.1	.1	700
	22:10	12:10	31:10	4.7	2700	.85	99	3450	18	101.6	142.8	111.1	111.5	.1	.1	700

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LOG OF TEST

ENGINEERING LABORATORIES

LOG NO. G-7

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TYPE OF TEST G.E. QCSEE ACTUATOR ENDURANCE TEST

PLAN OF TEST NO. 222PT-31

Rev. A

DATE 12-1-72

ENGINEER D. J. ...

OPERATORS ...

PART NO. 767500

TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deg. Blade Angle
2:18	12:30	24	4.7	3068	.85	99	245	245	112.3	145.0	111.3	110.5	.1	.1	-3
2:22	12:31	28	4.7	3068	.85	99	245	245	111.6	145.0	111.6	111.5	.1	.1	-
2:26	12:32	32	4.7	3068	.85	99	245	245	111.9	145.0	111.5	112.3	.1	.1	-
2:30	12:33	36	4.7	3068	.85	99	245	245	111.7	145.6	111.9	112.2	.1	.1	7
2:34	12:34	40	4.7	3068	.85	99	245	245	110.6	145.0	111.7	112.5	.1	.1	100
2:38	12:35	44	4.7	3068	.85	99	245	245	100.1	140.5	111.2	112.0	.1	.1	120
2:42	12:36	48	4.7	2700	.85	99	245	245	111.6	140.5	111.5	112.5	.1	.1	100
2:46	12:37	52	4.7	2700	.85	99	245	245	98.6	129.5	111.6	112.3	.1	.1	7
2:50	12:38	56	4.7	2700	.85	99	245	245	98.2	141.2	111.7	112.2	.1	.1	12
2:54	12:39	60	4.7	2700	.85	99	245	245	101.2	148.7	111.2	110.5	.1	.1	3
2:58	12:40	64	4.7	3068	.85	99	245	245	100.2	148.7	111.6	110.0	.1	.1	0
3:02	12:41	68	4.7	3068	.85	99	245	245	99.7	141.6	111.7	111.3	.1	.1	0
3:06	12:42	72	4.7	3068	.85	99	245	245	99.1	131.2	111.3	110.7	.1	.1	7
3:10	12:43	76	4.7	3068	.85	99	245	245	100.5	142.8	111.7	112.0	.1	.1	100
3:14	12:44	80	4.7	3068	.85	99	245	245	99.9	140.8	109.8	110.7	.1	.1	100

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LOG OF TEST
ENGINEERING LABORATORIES

DATE 1-17-50 SHEET 41 OF 41
ENGINEER W. J. H. H.
OPERATORS W. J. H. H.

RIG NO. G-7 PLAN OF TEST NO. 222PT-31 REV. A PART NO. 227550
W.P.I. NO. 176 SERIAL NO. 176

TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	Lube Oil	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Den. Blace Horiz. Ang.
8:20	14	14	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
8:30	15	15	4.7	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
8:40	16	16	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
8:50	17	17	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
9:00	18	18	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
9:10	19	19	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
9:20	20	20	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
9:30	21	21	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
9:40	22	22	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
9:50	23	23	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
10:00	24	24	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
10:10	25	25	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
10:20	26	26	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
10:30	27	27	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
10:40	28	28	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
10:50	29	29	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
11:00	30	30	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
11:10	31	31	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
11:20	32	32	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
11:30	33	33	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
11:40	34	34	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
11:50	35	35	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
12:00	36	36	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
12:10	37	37	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
12:20	38	38	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
12:30	39	39	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
12:40	40	40	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
12:50	41	41	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0
1:00	42	42	4.1	2100	2.00	1.00	1.00	1.00	1.00	100.5	100.5	100.5	100.5	1.0	1.0	1.0

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LOG OF TEST

ENGINEERING LABORATORIES

DATE 12-11-72 SHEET 42 OF 42
 ENGINEER J. J. J.
 OPERATORS L. J. J.

TEST NO. G-7 PLAN OF TEST NO. 222PT-31 Rev. A
 W.P.I. NO. 1 SERIAL NO. 767500

TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	Lube Oil	PSIG	PSIG	PSIG	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Blade Angle
11:11	11	11	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:12	12	12	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:13	13	13	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:14	14	14	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:15	15	15	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:16	16	16	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:17	17	17	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:18	18	18	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:19	19	19	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:20	20	20	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:21	21	21	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:22	22	22	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:23	23	23	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:24	24	24	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:25	25	25	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:26	26	26	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:27	27	27	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:28	28	28	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:29	29	29	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:30	30	30	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:31	31	31	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:32	32	32	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:33	33	33	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:34	34	34	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:35	35	35	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:36	36	36	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:37	37	37	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:38	38	38	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:39	39	39	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:40	40	40	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:41	41	41	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:42	42	42	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:43	43	43	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:44	44	44	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:45	45	45	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:46	46	46	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:47	47	47	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:48	48	48	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:49	49	49	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:50	50	50	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:51	51	51	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:52	52	52	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:53	53	53	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:54	54	54	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:55	55	55	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:56	56	56	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:57	57	57	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:58	58	58	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
11:59	59	59	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111
12:00	60	60	1.7	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111	1111

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HSER 7002

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DIVISION OF UNITED AIRCRAFT CORPORATION

LOG OF TEST

ENGINEERING LABORATORIES

FIG. NO. G-7

DATE

ENGINEER

SHEET 11 OF

TYPE OF TEST

G.E. CSEEE ACTUATOR ENDURANCE TEST

PLAN OF TEST NO.

222PT-31

Rev. A

OPERATORS

W.P.I. NO.

SERIAL NO.

PART NO. 767500

UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Dej. Blade Angle
	20.0	11.11	38.11	4.7	3408	177	29	2450	11.5	111°	111°	73°	74°	1	2	12°
	40.40	11.23	38.24													
	20.45	11.23	38.24	4.7	3400	174	29	2450	11.5	114°	115°	73°	75°	2	2	12°
	40.48	11.23	38.24	4.7	3408	172	29	2450	11.5	118°	115°	74°	73°	1	2	12°
	21.00	11.11	38.11	4.7	3408	177	29	2450	11.5	121°	122°	74°	74°	1	2	12°
	41.10	11.21	38.24	4.7	3408	178	29	2450	11.5	114°	114°	73°	74°	1	2	12°
	21.10	11.21	38.24	4.7	3400	176	29	2450	11.5	113°	112°	72°	72°	2	2	12°

REMARKS

PAGE NO.

REPORT NO.
HSER 7002

G-7

TYPE OF TEST

G.E. UCSEE ACTUATOR ENDURANCE TEST

PLAN OF TEST NO.

222PT-31

Rev. A

PART NO. 767510

SERIAL NO.

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U
A.LOG OF TEST
ENGINEERING LABORATORIES

G-7

120

TYPE OF TEST

G.E. COSEE ACTUATOR ENDURANCE TEST

W.P.I. NO.

112 102-11-213

PLAN OF TEST NO.

222PT-31

REV. A

ENGINEER

DATE

SHEET 12 OF 13

OPERATORS

PART NO. 767500

SERIAL NO.

TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 LHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deg. Blade Angle
11:21	11:21	46:14	47	3000	110	3400	3400	3400	110	128	90	90	1.1	1.2	120
11:22	11:22	46:14	47	3000	110	3400	3400	3400	110	128	90	90	1.1	1.2	120
11:23	11:23	46:14	47	3000	110	3400	3400	3400	110	128	90	90	1.1	1.2	120
11:24	11:24	46:14	47	3000	110	3400	3400	3400	110	128	90	90	1.1	1.2	120
11:25	11:25	46:14	47	3000	110	3400	3400	3400	110	128	90	90	1.1	1.2	120
11:26	11:26	46:14	47	3000	110	3400	3400	3400	110	128	90	90	1.1	1.2	120
11:27	11:27	46:14	47	3000	110	3400	3400	3400	110	128	90	90	1.1	1.2	120
11:28	11:28	46:14	47	3000	110	3400	3400	3400	110	128	90	90	1.1	1.2	120
11:29	11:29	46:14	47	3000	110	3400	3400	3400	110	128	90	90	1.1	1.2	120
11:30	11:30	46:14	47	3000	110	3400	3400	3400	110	128	90	90	1.1	1.2	120
11:31	11:31	46:14	47	3000	110	3400	3400	3400	110	128	90	90	1.1	1.2	120

REMARKS

PAGE NO

REPORT NO.

HSER 7032

LOG OF TEST
 ENGINEERING LABORATORIES

SHEET 22 OF 25
 DATE 12-15-55
 ENGINEER J. J. J. J.
 OPERATORS J. J. J. J.

RIG NO. 182
 TYPE OF TEST G-7
 W.P.I. NO. 100003-4000
 PLAN OF TEST NO. 222PT-31
 REV. A
 PART NO. 762500

UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deg. Blade Angle
	10:17	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:18	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:19	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:20	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:21	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:22	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:23	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:24	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:25	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:26	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:27	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:28	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:29	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:30	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:31	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:32	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:33	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:34	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:35	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:36	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:37	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:38	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:39	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:40	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:41	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:42	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:43	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:44	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:45	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:46	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:47	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:48	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:49	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:50	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:51	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:52	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:53	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:54	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:55	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:56	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:57	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:58	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	10:59	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	11:00	11	11	11.7	2700	1.85	99	3450	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5

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 REMARKS
 PAGE NO.

RIG NO. G-7		G. E. QCSEE ACTUATOR ENDURANCE TEST		PLAN OF TEST NO. 222PT-31		Rev. A		PART NO. 762500		ENGINEER OPERATORS						
TYPE OF TEST		W.P.I. NO.		SERIAL NO.												
UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	G/B Oil	Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Ho-iz.	Deg. Blade Angle
	1	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	2	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	3	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	4	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	5	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	6	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	7	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	8	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	9	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	10	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	11	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	12	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	13	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	14	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	15	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	16	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	17	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	18	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	19	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	20	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	21	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	22	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	23	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	24	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	25	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	26	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	27	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	28	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	29	12	4.7	4.7	100	8.4	9.9	11.2	10.0							
	30	12	4.7													

REMARKS:

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LOG OF TEST

ENGINEERING LABORATORIES

DATE 10/1/71 SHEET 1 OF 1
ENGINEER 10/1/71
OPERATORS 10/1/71

RIG NO. G-7

TYPE OF TEST G.E. QCSEE ACTUATOR ENDURANCE TEST

PLAN OF TEST NO. 222PT-31

Rev. A

W.P.I. NO. 10/1/71

SERIAL NO. 10/1/71

PART NO. 767500

UNITS →	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deg. Blade Angle
				10.7												
				11.1												
				11.2												
				11.3												
				11.4												
				11.5												
				11.6												
				11.7												
				11.8												
				11.9												
				12.0												
				12.1												
				12.2												
				12.3												
				12.4												
				12.5												
				12.6												
				12.7												
				12.8												
				12.9												
				13.0												
				13.1												
				13.2												
				13.3												
				13.4												
				13.5												
				13.6												
				13.7												
				13.8												
				13.9												
				14.0												
				14.1												
				14.2												
				14.3												
				14.4												
				14.5												
				14.6												
				14.7												
				14.8												
				14.9												
				15.0												
				15.1												
				15.2												
				15.3												
				15.4												
				15.5												
				15.6												
				15.7												
				15.8												
				15.9												
				16.0												
				16.1												
				16.2												
				16.3												
				16.4												
				16.5												
				16.6												
				16.7												
				16.8												
				16.9												
				17.0												
				17.1												
				17.2												
				17.3												
				17.4												
				17.5												
				17.6												
				17.7												
				17.8												
				17.9												
				18.0												
				18.1												
				18.2												
				18.3												
				18.4												
				18.5												
				18.6												
				18.7												
				18.8												
				18.9												
				19.0												
				19.1												
				19.2												
				19.3												
				19.4												
				19.5												
				19.6												
				19.7												
				19.8												
				19.9												
				20.0												

REMARKS:

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DIVISION OF UNITED AIRCRAFT CORPORATION
MIDDLETOWN, CONNECTICUT - U.S.A.U
A.LOG OF TEST
ENGINEERING LABORATORIESDATE 12-11-77
ENGINEER J. J. J. J.
OPERATORS J. J. J. J.

FIG. NO. G-7

TYPE OF TEST G.E. QCSEE ACTUATOR ENDURANCE TEST

W.P.I. NO. 112-51-112

PLAN OF TEST NO. 222PT-31

Rev. A

SERIAL NO.

PART NO. 762500

UNITS →	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deq. Blade Angle
	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12	11:12
	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13	11:13
	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14	11:14
	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15	11:15
	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16	11:16
	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17	11:17
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WINDSOR LOCKS, CONNECTICUT • U.S.A.

LOG OF TEST

ENGINEERING LABORATORIES

U
A.

HS 1758 4/67

REG. NO. G-7

TYPE OF TEST G.E. QCSEE ACTUATOR ENDURANCE TEST

W.P.I. NO. 777 103-403 B

PLAN OF TEST NO. 222PT-31

REV. A

DATE 12-15-75

ENGINEER D. H. HUNT

OPERATORS S. HUNT

PART NO. 767500

UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deq. Blade Angle
1110	24	41	45	4.7	3068	.85	99	3500	18	122	96	55	59	.1	.1	8.5
1125	24	41	45													
1140	24	41	45													
1155	24	41	45													
1450	24	41	45	4.7	3068	.85	99	3500	18	122	96	55	59	.1	.1	12
2000	25	41	45	4.7	3068	.85	99	3500	18	122	96	55	59	.1	.1	3
2010	25	41	46	4.7	3068	.85	99	3500	18	122	96	55	59	.1	.1	100
2020	25	41	46	4.7	3068	.85	99	3500	18	122	96	55	59	.1	.1	3

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DIVISION OF UNITED TECHNOLOGIES CORPORATION
HARTFORD, CONNECTICUT • U.S.A.

LOG OF TEST

ENGINEERING LABORATORIES

DATE 12-19-73
ENGINEER J. H. HUNT
OPERATORS J. H. HUNT

P.S. NO. G-7

TYPE OF TEST G.E. GCSEE ACTUATOR ENDURANCE TEST

W.P.I. NO. 100-712-6

PLAN OF TEST NO. 222PT-31

Rev. A

SERIAL NO.

PART NO. 767500

UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Den. Blade Angle
1135	26	11	11	4.1	3060	.85	99	3500	END Cycle #161	97	135	51	75	.1	.1	3
1145	26	11	11	4.1	3060	.85	99	3500	END Cycle #162							
1155	26	11	11	4.1	3060	.85	99	3500	END Cycle #163							
1205	26	11	11	4.1	3060	.85	99	3500	END Cycle #164							
1215	26	11	11	4.1	3060	.85	99	3500	END Cycle #165	109	104	54	57	.1	.1	12
1225	26	11	11	4.1	3060	.85	99	3500	END Cycle #166							
1235	26	11	11	4.1	3060	.85	99	3500	END Cycle #167	104	133	80	74	.1	.1	6
1245	26	11	11	4.1	3060	.85	99	3500	END Cycle #168							
1255	26	11	11	4.1	3060	.85	99	3500	END Cycle #169							
1305	26	11	11	4.1	3060	.85	99	3500	END Cycle #170	100	132	77	75	.1	.1	3
1315	26	11	11	4.1	3060	.85	99	3500	END Cycle #171							
1325	26	11	11	4.1	3060	.85	99	3500	END Cycle #172							
1335	26	11	11	4.1	3060	.85	99	3500	END Cycle #173	119	121	78	75	.1	.1	11
1345	26	11	11	4.1	3060	.85	99	3500	END Cycle #174							
1355	26	11	11	4.1	3060	.85	99	3500	END Cycle #175							

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ENGINEERING LABORATORIES

U.S. NO. G-7

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DATE 12-14-75
ENGINEER D. N. L. C. O.
OPERATORS S. H. H. O.

TYPE OF TEST G.E. QCSEE ACTUATOR ENDURANCE TEST
W.P.I. NO. 117-003-ADD 13
PLAN OF TEST NO. 222PT-31 Rev. A
SERIAL NO. PART NO. 767500

UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deq. Blade Angle
2235	21	18	20	4.7	3408	.85	99	3500	END CYCLE #176	101	123	78	74	.1	.1	700
2205	21	18	30	4.7	3068	.85	99	3500	END CYCLE #178	99	135	78	75	.1	.1	700
2220	28	18	15	4.7	2700	.85	99	3500	END CYCLE #182	99	124	78	75	.1	.1	700
2230	28	17	05	4.7	3408	.85	99	3500	END CYCLE #185	101	137	76	74	.1	.1	700

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Hamilton Standard
WINDSOR LOCKS, CONNECTICUT - U.S.A.

U.S. DEPARTMENT OF DEFENSE
A.

LOG OF TEST
ENGINEERING LABORATORIES

RIG NO. G-7

NO. OF TEST 1
W.P.J. NO. 11

G.E. QCSEE ACTUATOR ENDURANCE TEST

PLAN OF TEST NO. 222PT-31

REV. A

SERIAL NO. 767500

DATE 1-2-73

ENGINEER

OPERATORS

UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deg. Blade Angle
10	50	11	50	11.7	3408	8.550	11	34.0	17.5	100	100	100	114	1	1	100
11	00	12	50	11.7												
11	10	13	50	11.7												
11	20	14	50	11.7												
11	30	15	50	11.7												
11	40	16	50	11.7												
11	50	17	50	11.7												
11	00	18	50	11.7												
11	10	19	50	11.7												
11	20	20	50	11.7												
11	30	21	50	11.7												
11	40	22	50	11.7												
11	50	23	50	11.7												
11	00	24	50	11.7												
11	10	25	50	11.7												
11	20	26	50	11.7												
11	30	27	50	11.7												
11	40	28	50	11.7												
11	50	29	50	11.7												
11	00	30	50	11.7												
11	10	31	50	11.7												
11	20	32	50	11.7												
11	30	33	50	11.7												
11	40	34	50	11.7												
11	50	35	50	11.7												
11	00	36	50	11.7												
11	10	37	50	11.7												
11	20	38	50	11.7												
11	30	39	50	11.7												
11	40	40	50	11.7												
11	50	41	50	11.7												
11	00	42	50	11.7												
11	10	43	50	11.7												
11	20	44	50	11.7												
11	30	45	50	11.7												
11	40	46	50	11.7												
11	50	47	50	11.7												
11	00	48	50	11.7												
11	10	49	50	11.7												
11	20	50	50	11.7												
11	30	51	50	11.7												
11	40	52	50	11.7												
11	50	53	50	11.7												
11	00	54	50	11.7												
11	10	55	50	11.7												
11	20	56	50	11.7												
11	30	57	50	11.7												
11	40	58	50	11.7												
11	50	59	50	11.7												
11	00	60	50	11.7												
11	10	61	50	11.7												
11	20	62	50	11.7												
11	30	63	50	11.7												
11	40	64	50	11.7												
11	50	65	50	11.7												
11	00	66	50	11.7												
11	10	67	50	11.7												
11	20	68	50	11.7												
11	30	69	50	11.7												
11	40	70	50	11.7												
11	50	71	50	11.7												
11	00	72	50	11.7												
11	10	73	50	11.7												
11	20	74	50	11.7												
11	30	75	50	11.7												
11	40	76	50	11.7												
11	50	77	50	11.7												
11	00	78	50	11.7												
11	10	79	50	11.7												
11	20	80	50	11.7												
11	30	81	50	11.7												
11	40	82	50	11.7												
11	50	83	50	11.7												
11	00	84	50	11.7												
11	10	85	50	11.7												
11	20	86	50	11.7												
11	30	87	50	11.7												
11	40	88	50	11.7												
11	50	89	50	11.7												
11	00	90	50	11.7												
11	10	91	50	11.7												
11	20	92	50	11.7												
11	30	93	50	11.7												
11	40	94	50	11.7												
11	50	95	50	11.7												
11	00	96	50	11.7												
11	10	97	50	11.7												
11	20	98	50	11.7												
11	30	99	50	11.7												
11	40	100	50	11.7												

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U. S. A.

LOG OF TEST
ENGINEERING LABORATORIES

RIG NO. C-100

TYPE OF TEST Pressure vs Flow

W.P.I. NO. 10

PLAN OF TEST NO. 100

SERIAL NO. _____

PART NO. _____

DATE 1-11-68 OF
ENGINEER D. J. [illegible]
OPERATORS [illegible]

UNITS →	TIME	INLET PRESS	FLOW GPM	OF GPM PERMIN
	10	9	80	
	20	18	110	
	30	18	135	
	40	21.75	129	
	50	24.25	132	
	60	26.75	133	
	70	29	134	
	80	31	134	

ORIGINAL PAID
OF POOR QUALITY

REMARKS MIL-L-78086

REPORT NO.
HSER 7002

TYPE OF TEST

PLAN OF TEST NO. _____
SERIAL NO. _____

PART NO. 021310

REPORT NO.
HSER 7002

[illegible]

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/INDSOR LOCKS, CONNECTICUT • U.S.A.U
A.LOG OF TEST
ENGINEERING LABORATORIES

SHEET 2 OF 2

RIG NO. G-7

G-7

TYPE OF TEST

G.E. QCSEE ACTUATOR ENDURANCE TEST

W.P.I. NO.

11-11-67-112-34

PLAN OF TEST NO.

222PT-3B

Rev. A

SERIAL NO.

PART NO. 767500

DATE

ENGINEER

OPERATORS

UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	Cycles	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deg. Blade Angle
1	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
2	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
3	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
4	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
5	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
6	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
7	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
8	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
9	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
10	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
11	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
12	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
13	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
14	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
15	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
16	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
17	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
18	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
19	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
20	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
21	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
22	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
23	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
24	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
25	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
26	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
27	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
28	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
29	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
30	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
31	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
32	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
33	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
34	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
35	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
36	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
37	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
38	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
39	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
40	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
41	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
42	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
43	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
44	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
45	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
46	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
47	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
48	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
49	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18
50	27 45	50	35	3.6	3100	18	18	18	18	18	18	18	18	18	18	18	18

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REPORT NO.

HSER 7002

REG. NO. G-7

TYPE OF TEST G.E. QCSEE ACTUATOR ENDURANCE TEST

W.P.I. NO. 11-1-74

PLAN OF TEST NO. 222PT-38

SERIAL NO. 11-1-74

PART NO. 763500

UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/D Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deq. Blade Angle
1130	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1140	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1150	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1200	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1210	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1220	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1230	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1240	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1250	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1300	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1310	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1320	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1330	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1340	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1350	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1360	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1370	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1380	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1390	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1400	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1410	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1420	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1430	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1440	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1450	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1460	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1470	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1480	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1490	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2
1500	341	54	10	3.6	3000	500	78	3400	18	1000	1350	100	1200	1	1.2	1.2

HSER 7002

PAGE NO.

Hamilton Standard
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Hamilton Standard
WINDSOR LOCKS, CONNECTICUT • U.S.A.

LOG OF TEST ENGINEERING LABORATORIES

PIC NO. **G-7**

11-75

TYPE OF TEST

G.E. QCSEE ACTUATOR ENDURANCE TEST

222PT-38

PLAN OF TEST NO.

W.P.I. NO.

161-000-1074

SERIAL NO. _____
 FILE NO. _____

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WINDSOR LOCKS, CONNECTICUT • U.S.A.

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LOG OF TEST ENGINEERING LABORATORIES

SHEET 5 OF 1308

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RIG NO. **G-7**

TYPE OF TEST

EE OCSEE ACTUATOR ENDURANCE TEST

222PT-38

PLAN OF TEST NO.

PLAN OF TEST

W.P.L. NO.

11-66-403A

PART TWO

763500

UNITS	TIME	Test Time	Total Time	Para.	Rig R.P.M.	Lube Flow	PSIG Lube Oil	PSIG EHV Supply	PSIG G/B Oil	#1 Clutch	#3 EHV Supply	#4 Lube Oil	#5 Shroud Temp.	MILS Vib. Vert.	MILS Vib. Horiz.	Deq. Blade Angle
13	10	10	10	10	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
14	11	11	11	11	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
15	12	12	12	12	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
16	13	13	13	13	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
17	14	14	14	14	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
18	15	15	15	15	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
19	16	16	16	16	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
20	17	17	17	17	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
21	18	18	18	18	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
22	19	19	19	19	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
23	20	20	20	20	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
24	21	21	21	21	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
25	22	22	22	22	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
26	23	23	23	23	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
27	24	24	24	24	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
28	25	25	25	25	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
29	26	26	26	26	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
30	27	27	27	27	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
31	28	28	28	28	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
32	29	29	29	29	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
33	30	30	30	30	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
34	31	31	31	31	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
35	32	32	32	32	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
36	33	33	33	33	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
37	34	34	34	34	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
38	35	35	35	35	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
39	36	36	36	36	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
40	37	37	37	37	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
41	38	38	38	38	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
42	39	39	39	39	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
43	40	40	40	40	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
44	41	41	41	41	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
45	42	42	42	42	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
46	43	43	43	43	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
47	44	44	44	44	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
48	45	45	45	45	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
49	46	46	46	46	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
50	47	47	47	47	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
51	48	48	48	48	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
52	49	49	49	49	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
53	50	50	50	50	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
54	51	51	51	51	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
55	52	52	52	52	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
56	53	53	53	53	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
57	54	54	54	54	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
58	55	55	55	55	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
59	56	56	56	56	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
60	57	57	57	57	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
61	58	58	58	58	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
62	59	59	59	59	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
63	60	60	60	60	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
64	61	61	61	61	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
65	62	62	62	62	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
66	63	63	63	63	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
67	64	64	64	64	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
68	65	65	65	65	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
69	66	66	66	66	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
70	67	67	67	67	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
71	68	68	68	68	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
72	69	69	69	69	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
73	70	70	70	70	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
74	71	71	71	71	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
75	72	72	72	72	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
76	73	73	73	73	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
77	74	74	74	74	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
78	75	75	75	75	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
79	76	76	76	76	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
80	77	77	77	77	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
81	78	78	78	78	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
82	79	79	79	79	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
83	80	80	80	80	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
84	81	81	81	81	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
85	82	82	82	82	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
86	83	83	83	83	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
87	84	84	84	84	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
88	85	85	85	85	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
89	86	86	86	86	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
90	87	87	87	87	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
91	88	88	88	88	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
92	89	89	89	89	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
93	90	90	90	90	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
94	91	91	91	91	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
95	92	92	92	92	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
96	93	93	93	93	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
97	94	94	94	94	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
98	95	95	95	95	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
99	96	96	96	96	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
100	97	97	97	97	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
101	98	98	98	98	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
102	99	99	99	99	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
103	100	100	100	100	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
104	101	101	101	101	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
105	102	102	102	102	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1		
106	103	103	103	103	3000	0.5 GPM	25	3400	18	1000	1000	1.0	1000	.1	</	

QUESTIONS

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LOG OF TEST ENGINEERING LABORATORIES

05:39

TYPE OF TEST

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PLAN OF TEST NO.

SERIAL NO.

PART NO.

DATE _____

ENGINEER

OPERATORS

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REPORT NO.
HSER 7002

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APPENDIX E

TEST CHRONOLOGY

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TEST CHRONOLOGY

11-4-75	Started installation of actuator on rig.
11-5-75 & 11-6-75	Continued installation of actuator on rig.
11-7-75	Checked torque required to change pitch at wave generator. Appears high.
11-8-75	Removed actuator from disc. Retorqued blade retaining nuts to approximately equal twisting torques for each blade. Reinstalled actuator. Torque at wave generator now \approx 150 inch pounds. Continued assembly.
11-10-75	Completed installation. Ran LVDT calibrations and lubrication flow check. Found flex shaft leaks.
11-11-75	Sealed up leaks in flex shaft. Started running travel limit switch tests. After several stops, actuator would not move. Partial disassembly revealed no back output shaft fractured.
11-12-75 thru 11-19-75	Removed actuator from rig for inspection, and reinstalled on rig with repaired (welded) no back output shaft. Torque at wave generator to change pitch 140 inch pounds and at manual input \approx 45 inch pounds.
11-20-75	Attempts to run stopped by oil leaks at rig drive flange and water leaks at rig clutch. Removed actuator and disc from rig. Reworked oil drain holes in rig drive flange, and revised drive flange seal and clutch cooling water plumbing.

TEST CHRONOLOGY (continued)

11-21-75	Reinstalled disc and actuator. Oil leaks o.k., but clutch cooling water marginal. Could not get fan speed above 2750 rpm with blade angle as circuit breakers trip.
11-22-75	Exploring rig power problem.
11-24-75 thru 11-26-75	Fabricated shroud to enclose blades. Check run shows power problem solved.
11-28-75	Ran performance tests and 15 flight cycles with reduced pitch change rate.
11-29-75	Ran 31 flight cycles (total 46) and max pitch change rate tests.
12-1-75	Started disassembly for inspection. Found no-back output shaft fractured.
12-2-75 thru 12-5-75	Continued inspection and reassembly with new output shaft. Hydraulic motor bevel gear mesh pattern high. Reshimmed closer into mesh. Trunnion roller pattern on cam is high on one side of track, low on other. Torque to change pitch at manual input <u>40</u> inch pounds.
12-6-75	Ran 14 flight cycles (total 60). Inspected no-back hardware, o.k.
12-8-75	Ran 71 flight cycles (total 131).
12-9-75	Ran 24 flight cycles (total 155). Inspected no-back hardware, o.k..
212	Ran 33 flight cycles (total 188).

TEST CHRONOLOGY (continued)

12-10-75	Ran 52 flight cycles (total 240). Torque to change pitch at manual input now 35-40 inch pounds.
12-15-75	Ran part of frequency response testing and 60 flight cycles (total 300).
12-16-75	Inspected no-back hardware, o.k. Reworked no-back output shaft to reduce stress concentrations and shot peened it in web area.
12-17-75	Reassembled and ran 70 flight cycles (total 370).
12-18-75	Ran 115 flight cycles (total 485).
12-19-75	Ran 20 flight cycles (total 505). Disassembled no-back for inspection. Output shaft fractured in one web.
12-29-75	Reassembled and ran rotating frequency response test.
12-30-75	Ran positioning accuracy and minimum blade angle change tests.
12-31-75	Re-ran travel limit switch, performance, positioning accuracy, and static frequency response tests.
1-2-76 thru 1-7-76	Complete disassembly and inspection including magnaflux and zygo. Hydraulic motor bevel gear mesh showed pitting and scoring. One hydraulic motor damaged during disassembly. No-back output shaft was fractured. All other magnaflux and zygo o.k.

TEST CHRONOLOGY (continued)

1-8-76 thru 1-12-76	Reassembled beta regulator with one new motor, new bevel gear set, and reworked feedback shaft to provide positive bevel gear mesh lubrication.
1-13-76	Reassembled differential gear train. Beta regulator at inspection for installation dimension check.
1-14-76	Ran lubrication flow versus pressure test on beta regulator.
1-15-76	Beta regulator to shipping. Reassembled no-back with new spring and new output shaft.
1-16-76	Fitting spring to drum.
1-19-76	Started actuator installation in rig. Rear housing fractured during assembly.
1-20-76 thru 1-30-76	Repair of rear housing. Ran static deflection tests on snubber.
2-2-76 thru	Reassembly on rig. Actuator has new no-back spring and output shaft, new flex shaft, and snubber. New flex shaft has slight leak.
2-5-76	Ran an LVDT calibration and maximum pitch change rate testing. Inspected no-back hardware, o.k.

TEST CHRONOLOGY) (continued)

2-6-76	Reassembled actuator and attempted to run flight cycles. Had trouble with controller and pumps which supply pitch change fluid. Ran 3 flight cycles.
2-7-76	Ran 12 flight cycles (total 15). Had trouble with pitch change fluid pumps.
2-9-76	Installed an accumulator in the pitch change fluid supply system.
2-10-76	Ran 45 flight cycles (total 60).
2-11-76	Attempted to run static frequency response test. No response at ± 4 ma input to servo valve.
2-12-76	Disassembled regulator. Found one hydraulic motor (new one) has heavy wear on housing at drive gear face. Dimensional checks show nothing. Started rework necessary to obtain new motor.
2-13-76	Reassembled regulator and ran travel limit switch tests.
2-14-76	Installed new motor in regulator. Actuator responds to ± 4 ma inputs to servo valve. Ran blade angle accuracy and performance tests.
2-16-76	Ran static frequency response test. Started disassembly.
2-17-76	Hardware inspection revealed that flex shaft had been overtorqued. All other hardware o.k.

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**APPENDIX F
REFERENCES**

REFERENCE LIST

HSPC 74A14	QCSEE Variable Pitch Fan System Proposal
SP 08A74	QCSEE Variable Pitch Fan Pitch Change System
NASA CR-134852	Hamilton Standard Cam/Harmonic Drive Variable Pitch Fan Actuation System Detail Design Report
NASA CR-134873	QCSEE Ball Spline Pitch Change Mechanism Design Report